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RESULTS ON LOCATION AND SCALE PARAMETER ESTIMATION WITH APPLICATION TO THE EXTREME-VALUE DISTRIBUTION

NANCY R. MANN
ROCKETDYNE, A DIVISION OF NORTH AMERICAN
AVIATION, INC.
CANOGA PARK, CALIFORNIA

Contract No. AF 33(615)-2818

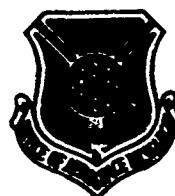
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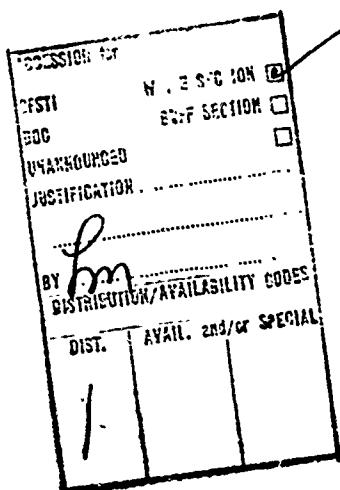


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AEROSPACE RESEARCH LABORATORIES
OFFICE OF AEROSPACE RESEARCH
UNITED STATES AIR FORCE
WRIGHT-PATTERSON AIR FORCE BASE, OHIO

FOREWORD

The major portion of the work summarized in this interim technical report was sponsored by the Aerospace Research Laboratories, Office of Aerospace Research, United States Air Force, Wright-Patterson Air Force Base, Ohio under Contract AF33(615)-2818. Work on this contract, technically monitored by Dr. H. L. Harter, is documented under Project 7071, Research in Applied Mathematics. The tables for obtaining the best linear invariant estimates of parameters of the extreme-value distribution which appear in Appendix C were calculated under the auspices of the Reliability Subdivision of the Liquid Rocket Division at Rocketdyne, with the support of Contract NAS 8-19 (J2 Engine System Development). The initial work on the tables appearing in Appendix D was also performed under the NAS contract.

ABSTRACT

This report gives results concerning estimation of location and scale parameters.

Most of the work pertains to the first extreme-value distribution of smallest values, the distribution of the natural logarithms of failure times having the two-parameter Weibull distribution. Experimental designs are derived, under the assumption that log failure times are polynomial functions of the reciprocal of stress level and have the extreme-value distribution, for over-stress life tests.

These designs yield least-squares curves with minimum variance at a specified (nominal) stress level below the levels at which the life test is conducted.

An estimate of the extreme-value location parameter u associated with the nominal stress level and the relationship between u and stress level can be obtained from the least-squares curve. Other extreme-value results apply to a life test conducted at a single fixed stress level.

Interval estimators (confidence bounds) are derived for the extreme-value scale parameter b and for any location parameter of the form $x_R = u + b \log \log(1/R)$ where R is specified (the 100(1-R)percent point of the distribution). The bounds for b and x_R are, respectively, based on two and three of the first n extreme-value order statistics, $x_1 \leq x_2 \leq \dots \leq x_m$, and are of the form $k_b(x_q - x_p)$ and $x_v + k_R(x_q - x_p)$. For each combination of values of sample size n , censoring number m , confidence level $1-\alpha$, and survival proportion R , an optimum choice of p , q , and v has been made. The criterion used in the selection is that the expected squared deviation of the bound from the parameter should be minimized. For samples up to size 22, values of the constant k_b corresponding to the optimum combination of p and q are presented. Tables of values of k_R are also in preparation.

For $2 \leq n \leq 25$, $2 \leq m \leq n$, tables are given for estimating b and x_R , where the estimator is best among linear estimators with expected loss invariant under translations. These best linear invariant (BLI) estimators have uniformly smaller expected loss than the Gauss-Markov best linear unbiased (BLU) estimators and are simple linear functions of the BLU estimators.

Expressions are derived for Cramer-Rao bounds for invariant estimators of general location and scale parameters. These bounds are applied to the extreme-value distribution, and compared with the expected losses of BLI and BLU estimators of u , b , and x_R , for certain values of R , for $2 \leq n \leq 25$, $2 \leq m \leq n$.

The one problem considered which concerns the Gaussian rather than the extreme-value distribution is the outlier problem for a size-three sample. One approach to the problem involves a simplified Bayesian analysis. This leads to recommendations for estimators of the Gaussian location parameter which depend only on the observations and a prior probability that the largest (or smallest) observed value is an outlier.

TABLE OF CONTENTS

Extreme-Value Distribution	1
Evaluation of Confidence Bounds for Distribution Percentage Points and for the Scale Parameter	1
Cramer-Rao Efficiencies of Best Linear Invariant Estimators	3
Tables for Obtaining Best Linear Invariant Estimates	5
Design of Over-Stress Life-Test Experiments	5
The Outlier Problem for Samples of Size Three	7
Definition of the Problem	7
Comparison of Estimators for the Mean	7
A Method of Dealing with the Unknown Parameter Δ/σ	13
References	16
<u>Appendix A: Design of Over-Stress Life-Test Experiments When Failure Times have the Two-Parameter Weibull Distribution</u>	17
Summary	17
Introduction	20
The Model	23
Design for Optimum Estimation	25
Properties of the Least-Squares Curve Under the General Model	32
A Comparison of the Traditional and the Derived Designs	40
References	44
<u>Appendix B: Exact Three-Order-Statistic Confidence Bounds on Reliability Parameters Under Weibull Assumptions</u>	45
Introduction	45
Tests and Confidence Sets for the Parameter b	47
Tests and Confidence Sets Based on all the Order Statistics	47
Tests and Confidence Sets Based on Two Order Statistics	52

Comparison of Bounds Based on Φ_1 and Φ_A	54
Unbiasedness of Φ_1	56
Induced Tests and Confidence Sets for Reliability and Reliable Life	57
Induced Tests and Confidence Sets for Reliability Based on all the Order Statistics	57
Induced Tests and Confidence Sets Based on Two or Three Order Statistics	61
Improvement of Derived Tests and Confidence Sets	65
Tests and Confidence Sets Concerning b	65
Tests and Confidence Sets Concerning Reliable Life	69
Obtaining Bounds on Reliability for Specified Required Life	71
Extension of Results	72
Extension to Other Two-Parameter Distributions	72
Extension to Three-Parameter Distributions	73
Calculation of the Coefficients Yielding the Exact Bounds and Use of the Tables	76
References	79
Table B.I	81
<u>Appendix C: Tables for Obtaining the Best Linear Invariant Estimates of Parameters of the Weibull Distribution</u>	85
Summary	85
Introduction	86
Maximum-Likelihood Estimation	88
Linear Estimation	90
Accuracy of the Tables	95
Estimation Procedure for Samples Larger than 25	96

References	99
<u>Table C.I Weights for Obtaining Best Linear Invariant Estimates of Parameters of the Extreme-Value Distribution</u>	101
<u>Appendix D: Cramer-Rao Efficiencies of Best Linear Invariant Estimates of Parameters of the Extreme-Value Distribution</u>	138
Efficiencies of Best Linear Invariant Estimates of Parameters of the Extreme-Value Distribution	143
References	148
<u>Appendix D.I: Cramer-Rao Lower Bounds for Invariant Estimates of Location and Scale Parameters</u>	149
<u>Appendix D.2: Cramer-Rao Lower Bounds for Estimates with Given Bias When a Nuisance Parameter is Present and the Sample is Censored</u>	155
Table D.I	160
Table D.II	168
Table D.III	176

EXTREME-VALUE DISTRIBUTION

EVALUATION OF CONFIDENCE BOUNDS FOR DISTRIBUTION PERCENTAGE POINTS AND FOR THE SCALE PARAMETER

Appendix B gives an analysis of the problem of obtaining confidence bounds on reliability parameters when the natural logarithms of failure times have the Type I extreme-value distribution of smallest values, and $(n-m)/n$ of the size n sample of ordered observations is censored from above. Exact lower confidence bounds on log reliable life x_R (the $100(1-R)$ percent point, where R is a specified survival proportion) are derived. These have smallest mean squared deviation from x_R among bounds of a specified form based on three order statistics only. The computer program and various subroutines for generating the tables for obtaining these bounds have been written. The subroutines, which perform the numerical integration for calculating distribution percentage points, calculate the risk (the expected squared deviation) of the bounds, read from tape the expected values, variances, and covariances of the reduced extreme-value order statistics, generate first guesses for percentage points, sort and order the risks for the various combinations of order statistics, etc., are all working as desired. The calculations based on the program will be made on the Wright-Patterson direct-coupled system due to the fact that a great deal of computer time will be required. This is true even though an approximation is being made in order to decrease substantially the number of distribution percentage points which will be calculated. If no such approximation is made, then for each combination of confidence level γ and specified R there are 20,615 percentiles which must be calculated, if only sample sizes 2, 3, ..., 20 are considered. Since several seconds, at

least, appear to be required for calculating each percentage point, it might take well over 2 days of computer time to determine the necessary values if only 2 values each of γ and R are considered.

It has therefore been decided to choose the three order statistics on which to base the bounds before calculating any percentage points. For each combination of sample size n , censoring number m , and specified survival proportion R , the estimator of x_R with smallest risk among those based on a linear combination, with risk invariant under translations, of one order statistic and the difference of two order statistics will be selected. The three order statistics specified by this estimation rule will then provide the basis for bounds at all confidence levels for each corresponding combination of m , n , and R . Indications are that very little increase in risk for the bounds will result from this procedure; and the number of computations will be decreased by a factor of over 100.

There is no apparent method of comparing the bounds directly with bounds, such as those obtained by Monte Carlo procedures by Johns and Lieberman [3], based on all of the first m order statistics. It is possible, however, to compare the risks for the three-order-statistic estimators described above with those of the best linear invariant (BLI) estimators, approximations to which form the basis for the bounds obtained by Johns and Lieberman. This has been done for sample sizes 2, 3, ..., 17, and demonstrates that the ratio of the risks of the BLI estimator and the best three-order-statistic estimator of $x_{.90}$ as described above is 0.877 for n as large as 17 and m equal to n . Ratios of this type are being determined for certain combinations of n , m , R , and will appear in a future report. Also included will be ratios of risks of the BLI estimator and the best estimator

of the extreme-value scale parameter b based on the two order statistics yielding the bound with smallest risk, for certain combinations of n , m , and γ .

Table B.I, which provides the means for calculation of the upper confidence bounds on b with smallest mean squared deviation from b among bounds based on two order statistics only, is included in Appendix B. At the same time distribution percentage points were being calculated as a basis for Table B.I, the power function of the tests associated with the bounds were also calculated for three prescribed values of b/b_0 (where the hypothesis tested is $H: b \geq b_0$). The calculations showed that the two-order-statistic bound with smallest risk seems to be either uniformly most powerful, locally most powerful, or most powerful for b/b_0 close to zero among two-order-statistic bounds. Moreover, when another two-order-statistic bound has greater power than the one with smallest risk for one of the prescribed values of b/b_0 , the difference between the calculated values of the two is almost negligible.

CRAMER-RAO EFFICIENCIES OF BEST LINEAR INVARIANT ESTIMATORS

The paper included as Appendix D gives the derivation of Cramér-Rao type bounds for invariant estimators of a scale parameter θ_2 and location parameters of the form $\theta_1 + A\theta_2$, where (θ_1, θ_2) is a location-scale parameter (that is, $f_{\theta_1, \theta_2}(x) = \frac{1}{\theta_2} g\left(\frac{x-\theta_1}{\theta_2}\right)$, for some g). These bounds, which are appropriate for the case in which any proportion of the sample observations may be censored, are shown to be functions of the bounds for unbiased estimators. They are applied specifically to invariant estimators of percentage points of the first extreme-value distribution of smallest values

for the case in which $(n-m)/n$ of a size n sample of ordered observations is censored from above. The Cramér-Rao efficiencies of the best linear invariant estimators are then tabulated (see Table D.III) for the 10 percent point (reliable life for a specified survival proportion R of 0.90) and $2 \leq n \leq 18$. Also tabulated on the basis of previous computations and the derived result (see Table D.I and Table D.II) are the mean squared errors of the best linear invariant and the best linear unbiased estimators, along with their respective Cramér-Rao bounds, for the extreme-value location parameter u , for the scale parameter b , and for the first and tenth percentiles of the distribution.

This paper was written as an extra task under the contract for the symposium on reliability and life-testing presented by the Society for Industrial and Applied Mathematics (SIAM) in Seattle, November 14-15, 1965. A special issue of the journal of the society was planned to include many of the papers presented at the symposium, and this material was submitted for consideration. The plans for the special issue were apparently dropped, however, so that the paper was accepted for publication in a regular issue of the SIAM Journal, subject to a few revisions in the introduction and an incorporation of the appendices into the body of the paper. Also, Table D.I and Table D.II will not be included. The elimination of these two tables provides part of the motivation for including this paper in this report, since, for example, there is no source other than Table D.II from which one may directly obtain the variances of the best linear unbiased estimators of the extreme-value parameters for $n = 21, 22, \dots, 25$. (They may be obtained indirectly from Table D.I or from Table C.I in Appendix C). The values of the two types of bounds, too, are of interest for comparison with each other and with the risks of other types of estimators.

TABLES FOR OBTAINING BEST LINEAR INVARIANT ESTIMATES

The entries for Table C.I, which appears in Appendix C, are based on computations made in part at the Health Sciences Computing Facility at the University of California at Los Angeles and in part at Rocketdyne, under the auspices of the Liquid Rocket Division with the support of Contract NAS 8-19. The values computed at that time (weights for obtaining best linear unbiased estimates of extreme-value parameters) were modified according to theory recently derived to obtain the weights for the best linear invariant (BLI) estimates. These weights for the BLI estimates were then published as part of a Rocketdyne research report under the contract. The report is included here because it has elicited considerable interest and appears to warrant a wide distribution. The paper has been submitted for publication but may present something of a problem in this respect because of the length of the tables.

DESIGN OF OVER-STRESS LIFE-TEST EXPERIMENTS

Appendix A gives the derivation of results specifying designs with certain optimum properties for life-test experiments under particular assumptions concerning the failure times of the population of items under consideration. A two-parameter Weibull model is assumed for the probability density function of the failure times; and further it is supposed that the logarithm of failure time is a polynomial function of the reciprocal of stress level. Finally, it is assumed that the level of stress to which the population of items being considered is subjected during normal usage (the nominal stress level), is not sufficient to produce a failure of an item within any reasonable amount of time after the application of the stress. Thus it is supposed that the life test,

which will allow one to estimate certain properties of the distribution of the failure times at the nominal stress level, is conducted at levels above nominal stress.

The designs derived under these assumptions specify where (at what stress levels) within a given interval of stress the life tests should be conducted and what proportion of the total number of items should be assigned to each testing level when all of the items are tested until failure and when least-squares estimation procedures are to be applied. Certain properties are demonstrated for the least-squares curve at the various testing levels and at the nominal stress level when a design of the form derived is used.

It should be noted that the assumption originally proposed for this task concerning a change of level of stress applied to an item during a life test was not incorporated in this work. The reason for this was the fact that the following became apparent after some analysis. For testing at various stress levels where any failure-time distribution parameter depends upon stress level, it is not possible to estimate such a parameter efficiently at any level unless the relationship between the parameter and the stress level can also be estimated. When stress level is changed during testing, it is not clear how one should determine or define the actual stress which has been applied to produce the failure. In other words, the testing level is not actually defined for this situation so that it is not possible to estimate the relationship between stress level and failure-time parameters.

THE OUTLIER PROBLEM FOR SAMPLES OF SIZE THREE

DEFINITION OF THE PROBLEM

Suppose three observations on a normally distributed random variable are made, and the largest (or smallest) is suspected of being an outlier. The chemist's approach to the problem of estimating the mean μ of the distribution has traditionally been to discard the observed value of the possible outlier and average the other two values. Use of a Winsorized estimator of μ , often recommended when outlying values are suspect, involves changing the observed value of the outlier to the value of the second ordered observation, and then averaging all three values. Sometimes the median of the three observations is used. Clearly, if the suspected value is not an outlier, or if the amount by which it is displaced is very small compared with the distribution standard deviation then the arithmetic mean of all three observed values is best for estimating μ . What if, however, the amount of displacement is moderate or large or there is a fairly high probability that the observation in question is an outlier? The following analysis gives some insight into this problem.

COMPARISON OF ESTIMATORS FOR THE MEAN

Assume that $Y_1 \leq Y_2 < Y_3$, and that either θ_o : Y_1 , Y_2 , and Y_3 are order statistics from $N(\mu, \sigma)$, or θ_A : Y_1 and Y_2 are order statistics from $N(\mu, \sigma)$ and Y_3 is a size 1 sample from $N(\mu + \Delta, \sigma)$. Because of the symmetry of the distribution, the case in which Y_1 is the observation which is suspect can also be handled.) The risk (expected loss, where loss is squared error divided by σ^2) can then be calculated for any estimator under the two alternatives θ_o and θ_A . All values given below are correct to within a unit in the final decimal place shown. Values which are exact are given in fractional form. The moments of the normal

order statistics used to calculate these values appear in [4].

$$\text{Consider } \hat{\mu}_0 = \frac{1}{3}(Y_1 + Y_2 + Y_3)$$

$$\hat{\mu}_1 = \frac{1}{2}(Y_1 + Y_2)$$

$$\hat{\mu}_2 = \frac{1}{3}(Y_1 + 2Y_2)$$

$$\text{and } \hat{\mu}_3 = Y_2.$$

If $R_k(\mu, \hat{\mu}_j)$ is the risk for estimator $\hat{\mu}_j$ ($j=0, 1, 2, 3$) when θ_k ($k=0$ or Δ) is true, then

$$R_0(\mu, \hat{\mu}_0) = \frac{1}{3}$$

$$R_\Delta(\mu, \hat{\mu}_0) = \frac{1}{3} + \Delta^2/9\sigma^2$$

$$R_0(\mu, \hat{\mu}_1) = .569$$

$$R_\Delta(\mu, \hat{\mu}_1) = \frac{1}{2}$$

$$R_0(\mu, \hat{\mu}_2) = .464$$

$$R_\Delta(\mu, \hat{\mu}_2) = .556$$

$$R_0(\mu, \hat{\mu}_3) = .449$$

$$R_\Delta(\mu, \hat{\mu}_3) = 1$$

Of the three estimators $\hat{\mu}_1$, $\hat{\mu}_2$, and $\hat{\mu}_3$, $\hat{\mu}_2$ has minimax risk (minimizes the maximum risk for all Δ , μ , and σ). It is not the true minimax estimator, however. Assume σ is not known and consider all estimators which are linear functions of Y_1 and Y_2 and which have expected loss independent of μ and σ . These linear invariant estimators will be of the form $\hat{\mu}(a_1) = a_1 Y_1 + (1-a_1) Y_2$ [5].

When θ_0 is true, the best linear unbiased estimators of μ and σ based on Y_1 and Y_2 are simply $\mu_0^* = Y_2$ and $\sigma_0^* = 1.1816(Y_2 - Y_1)$

with the variances and covariance of these estimators respectively given

$$\text{by } V(\mu_0^*) = .4487\sigma^2 \equiv A_0\sigma^2, V(\sigma_0^*) = .6378\sigma^2 \equiv C_0\sigma^2, C(\mu_0^*, \sigma_0^*) = .2044\sigma^2 \equiv B_0\sigma^2.$$

Thus, by the results in [], when θ_0 is true the best linear invariant

$$\text{estimator based on } Y_1 \text{ and } Y_2 \text{ is } \tilde{\mu}_0 = \mu_0^* - [B_0/(1+C_0)]\sigma_0^*$$

$$= .1475Y_1 + .8525Y_2. \text{ When } \theta_\Delta \text{ is true } \mu_\Delta^* = \hat{\mu}_1 = \frac{1}{2}(Y_1 + Y_2) \text{ and}$$

$$\sigma_\Delta^* = -.8862Y_1 + .8862Y_2 \text{ are, respectively, the best linear unbiased}$$

$$\text{estimators of } \mu \text{ and } \sigma. \text{ Since the covariance } B_\Delta\sigma^2 \text{ of } \mu_\Delta^* \text{ and } \sigma_\Delta^*$$

is equal to zero, the best linear invariant estimator $\tilde{\mu}_\Delta$ based on Y_1

$$\text{and } Y_2 \text{ for } \theta_\Delta \text{ true is equal to } \mu_\Delta^*. \text{ The risk } R_k(\mu, \tilde{\mu}_j) \text{ for } \tilde{\mu}_j$$

when $\theta_k (j, k=0, \Delta)$ is true is given as follows

$$R_0(\mu, \tilde{\mu}_0) = .423$$

$$R_\Delta(\mu, \tilde{\mu}_0) = .748$$

$$R_0(\mu, \tilde{\mu}_\Delta) = .569$$

$$R_\Delta(\mu, \tilde{\mu}_\Delta) = \frac{1}{2}.$$

Now, since $\tilde{\mu}_0$ is not equal to $\tilde{\mu}_\Delta$, which would imply $R_0(\mu, \tilde{\mu}_0) = R_0(\mu, \tilde{\mu}_\Delta)$ and $R_\Delta(\mu, \tilde{\mu}_0) = R_\Delta(\mu, \tilde{\mu}_\Delta)$, there is no guarantee that $\tilde{\mu}_\Delta$ has minimax risk among all linear functions of the form $\hat{\mu}(a_1)$. In fact,

$\tilde{\mu}_\Delta = \hat{\mu}_1$ has larger maximum risk than $\hat{\mu}_2$, as was noted earlier.

Define $\hat{\mu}_4$ to be the minimax-risk linear invariant estimator, that is,

the one such that $\max[R_0(\mu, \hat{\mu}_4), R_\Delta(\mu, \hat{\mu}_4)]$ is the minimum of

$\max[R_0(\mu, \hat{\mu}(a_1)), R_\Delta(\mu, \hat{\mu}(a_1))]$, $-\infty < a_1 < \infty$. The maximum risk of $\hat{\mu}_4$

can be no smaller than $\max[R_0(\mu, \tilde{\mu}_0), R_\Delta(\mu, \tilde{\mu}_\Delta)] = R_\Delta(\mu, \hat{\mu}(1/2)) = \frac{1}{2}$.

Furthermore, $R_0(\mu, \hat{\mu}(a_1))$ and $R_\Delta(\mu, \hat{\mu}(a_1))$ are continuous quadratic

functions of a_1 , each with a unique minimum. Therefore, if the value \bar{a}_1 of a_1 defined by

$$R_0(\mu, \hat{\mu}(\bar{a}_1)) = R_\Delta(\mu, \hat{\mu}(\bar{a}_1)) \quad (1)$$

is such that $.1475 < \bar{a}_1 < \frac{1}{2}$ (note that $\tilde{\mu}_0 = \hat{\mu}(.1475)$ and $\tilde{\mu}_\Delta = \hat{\mu}(1/2)$), then $\hat{\mu}(\bar{a}_1)$ is the minimax estimator $\hat{\mu}_4$. Solution of equation (1) gives $\bar{a}_1 = .42265$. Therefore, $\hat{\mu}(\bar{a}_1) = \hat{\mu}_4 = .42265Y_1 + .57735Y_2$, with $R_0(\mu, \hat{\mu}_4) = R_\Delta(\mu, \hat{\mu}_4) = .512$. Moreover, $\hat{\mu}_4$ can be expressed as $.5(Y_1 + Y_2) + .0830[.8862(Y_2 - Y_1)] = \hat{\mu}_\Delta^* + .0830\sigma_\Delta^*$, with σ_Δ^* equivalent to the unique best unbiased estimator of σ for sample size 2. Therefore, for θ_Δ true, distribution percentage points of $\frac{\hat{\mu}_4 - \mu}{\sigma^*}$ can be calculated from percentage points of the central t distribution.

In a real situation one might not want to use the minimax estimator, particularly if $|\Delta/\sigma|$ is apt to be small. A simplified Bayesian analysis may be employed to gain insight into how large $|\Delta/\sigma|$ must be before one would prefer another estimator to $\hat{\mu}_0$. Let γ be the prior probability of situation θ_Δ , with $|\Delta/\sigma|$ fixed, and $1-\gamma$ the probability of θ_0 . For comparative purposes the estimators $\hat{\mu}_0, \hat{\mu}_1, \hat{\mu}_2, \hat{\mu}_3$, and $\hat{\mu}_4$ will be used.

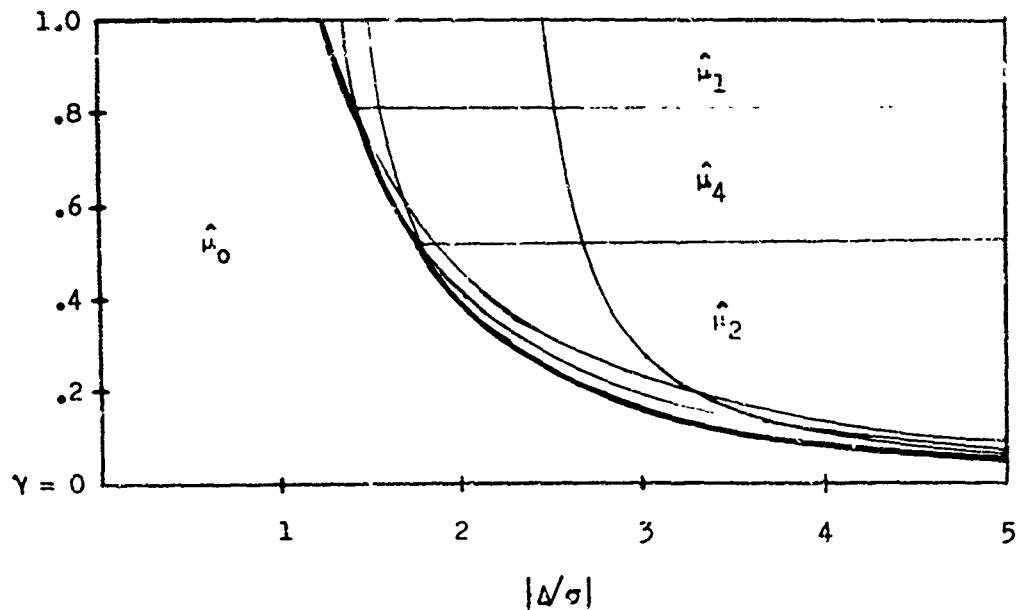
The risk using the estimator $\hat{\mu}_0$ is $1/3$ with probability $1-\gamma$ and $1/3 + \Delta^2/9\sigma^2$ with probability γ . The risk function for $\hat{\mu}_0$ can thus

be expressed as a function of γ and Δ , $R(\mu, \hat{\mu}_0, \gamma, \Delta) = 1/3 + \gamma(\Delta^2/9\sigma^2)$.
 For $\hat{\mu}_i$, $i=1,2,3,4$, the risk function $R(\mu, \hat{\mu}_i, \gamma, \Delta)$ is independent of Δ and can be expressed in terms of γ alone:

i	$R(\mu, \hat{\mu}_i, \gamma, \Delta)$
0	$1/3 + \gamma\Delta^2/9\sigma^2$
1	$.569 - .070\gamma$
2	$.464 + .092\gamma$
3	$.449 + .551\gamma$
4	$.512$

The last four of these expressions indicate the following: Of the estimators $\hat{\mu}_1, \hat{\mu}_2, \hat{\mu}_3, \hat{\mu}_4, \hat{\mu}_1 = \frac{1}{3}(Y_1 + Y_2)$ is to be preferred for $\gamma > .82$, for $.52 < \gamma \leq .82$, $\hat{\mu}_4$, the minimax estimator, and for $.03 < \gamma \leq .52$, $\hat{\mu}_2$, the Winsorized estimator $\frac{1}{3}(Y_1 + 2Y_2)$, are preferable. The median $\hat{\mu}_3$ is preferable to the other three only for $\gamma < .03$.

Figure 1



In practical situations it is likely that γ would be of small or moderate size and that Δ/σ would be positive and moderate or large. (If in fact $|\Delta/\sigma|$ were small one would not be apt to suspect the presence of outliers.) Thus, any of $\hat{\mu}_0$, $\hat{\mu}_2$, or $\hat{\mu}_4$ might be the preferable estimator. The median would be preferred to the other four estimators only if both $\gamma < .03$ and $|\Delta/\sigma| \geq 6$. It seems clear from this analysis that for each γ there is an estimator $\hat{\mu}(a_1(\gamma)) = a_1(\gamma)Y_1 + (1-a_1(\gamma))Y_2$ which minimizes the values of $|\Delta/\sigma|$ required such that a two-order-statistic estimator is preferred to $\hat{\mu}_0$.

The expression for $a_1(\gamma)$ has been found to be given by

$$a_1(\gamma) = \frac{.17301(1-\gamma)+\gamma}{.17301(1-\gamma)+2\gamma}.$$

Hence,

$$a_1(1) = \frac{1}{2}, \hat{\mu}(a_1(1)) = \frac{1}{2}(Y_1+Y_2),$$

$$\text{and } a_1(.5) = .3697, \hat{\mu}(a_1(.5)) = .3697Y_1 + .6303Y_2,$$

$$a_1(0) = .1474, \hat{\mu}(a_1(0)) = .1474Y_1 + .8526Y_2,$$

where $\hat{\mu}(a_1(1))$ is $\hat{\mu}_\Delta$, the best linear invariant (BLI) estimator when θ_Δ is true, and $\hat{\mu}(a_1(0))$ is $\hat{\mu}_0$, the BLI estimator when θ_0 is true. For $\hat{\mu}(a_1(\gamma))$ equal to the minimax estimator, $a_1(\gamma) = .42265$, so that γ is equal to .676.

It has also been demonstrated that $a_1(\gamma)$ increases monotonically with γ from .1474 for $\gamma = 0$ to .5 for $\gamma = 1$. Thus, the median would never be the two-order statistic estimator recommended in preference to $\hat{\mu}_c$.

A METHOD OF DEALING WITH THE UNKNOWN PARAMETER Δ/σ

A Monte Carlo analysis of a more general outlier problem is discussed in the final portion of Ferguson [2]. The results indicate that for a sample size as small as 3, there are no discernible differences between the values of the power functions of the locally most powerful test of $\Delta/\sigma = 0$ versus $\Delta/\sigma > 0$, based on the coefficient of skewness and two other tests, one of which is based on $R_{10} = (X_n - X_{n-1})/(X_n - X_1)$ with $X_1 \leq X_2 \leq \dots \leq X_{n-1} \leq X_n$, proposed by Dixon in [1].

Suppose we consider $\left(\frac{1}{R_{10}} - 1\right)^{-1} = \left\{ \left[(Y_3 - Y_2) / (Y_3 - Y_1) \right]^{-1} - 1 \right\}^{-1}$
 $= (Y_3 - Y_2) / (Y_2 - Y_1)$. Note that if $Z_{1,n}$ is the i^{th} order statistic

from a size n sample from the standard normal distribution,

$\left[(Y_3 - Y_2) / (Y_2 - Y_1) \right] (Z_{2,2} - Z_{1,2}) + Z_{2,2} = \Delta/\sigma + Z_{1,1}$ with probability γ , and $\left[(Y_3 - Y_2) / (Y_2 - Y_1) \right] (Z_{2,3} - Z_{1,3}) + Z_{2,3} = Z_{3,3}$, with probability $1 - \gamma$, where $(Y_i - \mu)/\sigma = Z_{i,2}$ ($i = 1, 2$), and $(Y_3 - \mu)/\sigma = \Delta/\sigma + Z_{1,1}$ with probability γ and $(Y_1 - \mu)/\sigma = Z_{1,3}$ and $(Y_3 - \mu)/\sigma = Z_{3,3}$ with probability $1 - \gamma$. Let $\left[(Y_3 - Y_2) / (Y_2 - Y_1) \right] (Z_{2,2} - Z_{1,2}) + Z_{2,2} - Z_{1,1}$ be identically equal to $t(Z_{2,2} - Z_{1,2}) + Z_{2,2} - Z_{1,1} = W(t)$, and let $\overline{\Delta/\sigma} > 0$ be specified. Then $\Pr[\Delta/\sigma > \overline{\Delta/\sigma}] = \Pr[\theta_\Delta \text{ is true}] \times \Pr[\Delta/\sigma > \overline{\Delta/\sigma} \mid \theta_\Delta \text{ is true}]$

or

$$\Pr[\Delta/\sigma > \overline{\Delta/\sigma}] = \gamma \int_{\overline{\Delta/\sigma}}^{\infty} dF[W(t)] .$$

The expression on the right-hand side of this equation can be calculated by considering the joint density of $Z_{1,2}$, $Z_{2,2}$ and $Z_{1,1}$. From this, one obtains

$$\gamma \int_{\overline{\Delta/\sigma}}^{\infty} dF[W(t)] = \gamma \left\{ 1 - \frac{1}{\sqrt{3}(2t+1)} \left\{ 3 \left[\Pr \left(Z < \frac{(2t+1)\overline{\Delta/\sigma}}{\sqrt{6(1+t+t^2)}} \right) \right]^2 \left[\Pr \left(Z > \frac{(2t+1)\overline{\Delta/\sigma}}{\sqrt{6(1+t+t^2)}} \right) \right] \right. \right. \\ \left. \left. + \left[\Pr \left(Z < \frac{(2t+1)\overline{\Delta/\sigma}}{\sqrt{6(1+t+t^2)}} \right) \right]^3 \right\} \right\} ,$$

where Z is the standard normal deviate and t is greater than zero.

The expression $\frac{2t+1}{\sqrt{6(1+t+t^2)}}$ is equal to $\frac{2Y_3 - Y_2 - Y_1}{\sqrt{6[(Y_3 - Y_2)^2 + (Y_3 - Y_2)(Y_2 - Y_1) + (Y_2 - Y_1)^2]}}$
 and $2t + 1$ equals $\frac{2Y_3 - Y_2 - Y_1}{Y_2 - Y_1}$.

An appropriate value for Δ/σ in terms of γ alone can be obtained by substituting $a_1(\gamma)$ into the original expression from which the value for $a_1(\gamma)$ is derived. This gives

$$\frac{\Delta/\sigma}{\sigma} = \left[\frac{2}{\gamma} \frac{(.18853\gamma^3 + .99076\gamma^2 - .20923\gamma + 1.029932)}{(.68391\gamma^2 + 1.9401\gamma + 1.3759)} - \frac{2}{\gamma} \right]^{\frac{1}{2}}.$$

Therefore, for any prior probability γ , that θ_A is true, the probability that Δ/σ is sufficiently large so that the risk of a two-order-statistic estimator is smaller than the risk of \hat{u}_0 can be calculated as a function of γ and the observations only. One could then choose some fixed value P , $0 < P < 1$ (a good choice might be $P = .5$), and for any known γ , estimate μ by $\hat{\mu}_0 = \frac{1}{3}(Y_1 + Y_2 + Y_3)$ if $\Pr[\Delta/\sigma > \bar{\Delta}/\bar{\sigma}]$ is less than P and by $\hat{\mu}(a_1(\gamma))$ otherwise.

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APPENDIX A

DESIGN OF OVER STRESS LIFE-TEST EXPERIMENTS WHEN FAILURE TIMES HAVE THE TWO-PARAMETER WEIBULL DISTRIBUTION

SUMMARY

The following paper deals with the situation in which estimation of reliability parameters associated with a failure-time distribution requires that life testing be conducted at stress levels above that which would normally be applied in standard usage (the nominal stress level). This situation may prevail when an inordinate amount of time is required to obtain a failure at the nominal stress level.

A range of stress for testing is prescribed, and a two-parameter Weibull model for failure times (a type I extreme-value distribution of smallest values for log failure time) is assumed. The extreme-value location parameter u , the logarithm of the Weibull scale parameters, is assumed to be a polynomial function of known degree k of the reciprocal of stress level. The Weibull shape parameter b , which is also the extreme-value scale parameter, is assumed to be independent of stress level. The number n of items in the total sample to be life tested is given, and it is assumed that stress level for each life test is sufficiently high so that each item can be tested until failure. The problem considered is that of determining the design for obtaining the least-squares-curve intercept with minimum variance at the nominal stress level. The design to be determined consists of the number and location of stress levels in the prescribed range at which the life tests will be conducted and proportion of total sample to be randomly allocated to each testing level.

The results of Hoel and Levine in [2] concerning determination of designs for minimum-variance polynomial extrapolation cannot be applied directly because the models for which these results are appropriate are those in which the observations are normally distributed, uncorrelated, and have uniform variance. In our model the logarithms of observed failure times have the Type I extreme-value distribution of smallest values, unequal variances, and covariances that are not zero except between stress levels. It is shown that the methods of proof utilized by Hoel and Levine are applicable, however, and rules for determining designs yielding the "approximately" minimum-variance least-squares intercept for the prescribed model are derived.

One of the interesting results in the derivation of the design is the delineation of the point through which the least-squares curve for the observations passes at the α^{th} stress level, $\alpha = 0, 1, \dots, k - 1$, when the number k of stress levels at which observations are made is $k + 1$. This point is $\frac{1}{\sigma_\alpha}, X^*(\frac{1}{\sigma_\alpha})$, where $X^*(\frac{1}{\sigma_\alpha})$ is a weighted average of the ordered observations and where the i^{th} weight consists of the elements in the i^{th} row, $i = 1, 2, \dots, n_\alpha$, of the covariance matrix of the n_α ordered observations made at the α^{th} level, $\alpha = 0, 1, \dots, k$. For $n_\alpha \geq 2$, $X^*(\frac{1}{\sigma_\alpha})$ can also be expressed as a specific function of the Gauss-Markov least-squares best linear unbiased estimators $u^*(\frac{1}{\sigma_\alpha})$ and b_α^* at $\sigma = \sigma_\alpha$ of u_α (the value of u at the α^{th} testing level) and

b , respectively, the variance of b_{α}^* and the covariance of $u^*(\frac{1}{\sigma_{\alpha}})$ and b_{α}^* , $\alpha = 0, 1, \dots, k$. This particular result is independent of the distribution of the observations and applies whether or not n_{α} is equal to n_{α} , where $n_{\alpha} = p_{\alpha}n$ and p_{α} is the proportion of the sample randomly assigned to the α^{th} sample point, $\alpha = 0, 1, \dots, k$, (that is, there may be censoring). It is shown that there is no linear combination $\bar{x}(\frac{1}{\sigma_{\alpha}})$ of ordered observations at the α^{th} testing level and no point along that ordinate such that the mean squared deviation of $\bar{x}(\frac{1}{\sigma_{\alpha}})$ from the point is less than or equal to the variance of $x^*(\frac{1}{\sigma_{\alpha}})$ for all u_{α} and b , $\alpha = 0, 1, \dots, k$. Similar properties are demonstrated for the least-squares intercept at the nominal stress level under the design prescribed by the derived results.

INTRODUCTION

Often an engineer may want an estimate of a parameter associated with the reliability of a population of items which are to be subjected to a fixed (or nominal) level of stress and fairly constant environmental conditions during normal usage. If a required life t_0 is specified, then he will want to estimate the reliability at time t_0 after the stress is applied. If, on the other hand, a survival proportion R is specified, then he will be interested in estimating the reliable life, or the time after the application of the stress at which $100(1-R)\%$ of the population of items will have failed.

He may know from theoretical considerations the family of distributions to which the failure times associated with the population of items belong. If so, he can conduct a life test by applying the nominal level of stress under appropriate environmental conditions to a sample chosen from the population of items and thus he can obtain an efficient estimate of the parameter of interest as a function of estimates of the distribution parameters (parameters of the failure-time distribution). These estimates will be based on the failure times observed during the life test.

Suppose, however, that the failure characteristics of the population are such that an excessively long period of time is required before even a single failure will occur at the nominal stress level. In such a case, the life test can be conducted at levels above nominal stress to obtain the failures required for estimation of the parameters, provided the form of the relationship between the parameters and the stress level is known. In the following discussion, the form of both this relationship and the failure-time distribution are assumed to be known from theory associated with the composition of the items.

It is assumed that in a life-testing situation the population failure times are identically distributed according to a given two-parameter Weibull law,

$$F(t) = \begin{cases} 1 - e^{-\left(\frac{t}{\xi}\right)^b}, & t \geq 0 \\ 0, & \text{otherwise} ; \xi, b > 0, \end{cases} \quad (1)$$

when the material and shape of the items tested, the environmental conditions of the test and the levels of stresses are fixed. We also assume that the size n sample which is tested has been randomly selected from a population of items composed of homogeneous material and that all environmental conditions are held fixed save level of stress σ for one type of stress of interest. Further, it is assumed, in agreement with [1], [8], and [9], that under these conditions the Weibull shape parameter b is constant and that only the scale parameter ξ changes as level of stress changes.

If the random variable T represents failure time, then X , the natural logarithm of T , has the Type I extreme-value distribution of smallest values with location parameter u (the natural logarithm of ξ) and scale parameter b , with $\pi^2 b^2/6$ the variance of X . We suppose that a given log failure time is a polynomial function of degree k of $1/\sigma$ (a special case of this assumption, $\log t = \beta_0 + \beta_1/\sigma$, is given in [1]). Finally, it

is assumed that the n_α failure times observable at the α^{th} of k experimental (or testing) stress levels are independent of those at any other of the $k - 1$ testing levels. This implies that the sample items are selected randomly for assignment to a stress level.

Under these assumptions it is desired to design the life test so that the least-squares curve (with expectation $x_{1/\sigma, b}$) has minimum variance at $\sigma = \frac{1}{\eta}$ when testing of the n sample items is conducted in the stress domain $c \leq \sigma \leq d$ and $\frac{1}{\eta} < c$. We define this to be optimum estimation for this situation, which is one of testing at levels above nominal stress. Because this is an over-stress situation, it is assumed here that the stress levels at which testing will be conducted are sufficiently high so that all items can be allowed to fail, with no consideration necessary for waiting time for failure. This over-stress problem is equivalent to one of obtaining an optimum design for linear estimation of the polynomial function $x_{1/\sigma, b}$ at a point outside the experimental range of the independent variable.

Specifically, it is necessary to determine (a) the value for k , the number of sample points, (b) where in the domain the k sample points should be assigned, and (c) the values of n_α , $\alpha = 0, 1, \dots, k - 1$, such that estimation is optimum for a given sample size n . The analysis involves approximation in terms of n_α , $\alpha = 0, 1, \dots, k - 1$, of the

variance of the least-squares curve at $\sigma = \frac{1}{\eta}$. Hence the optimal solution given is approximate.

It will be clear from the model given below that the results of Hoel and Levine in [2], which are applicable to the case in which the observations are independent, have equal variances, and are selected from a Gaussian distribution, cannot be used directly to provide the design for optimum estimation here.

THE MODEL

The derivations immediately following apply to the general case in which only the first m_α failure times, $m_\alpha \leq n_\alpha$, may be observed, so the assumptions $m_\alpha = n_\alpha$ will not be employed until later. Let

$X_{1,\alpha}, X_{1,\alpha} \leq X_{2,\alpha} \leq \dots \leq X_{m_\alpha,\alpha} \leq \dots \leq X_{n_\alpha,\alpha}$, be the logarithm of the i^{th} observed ordered failure time at the α^{th} stress level and let

$$Y_{i,\alpha} = \frac{X_{i,\alpha} - u_\alpha}{b}, \quad i = 1, 2, \dots, m_\alpha,$$

where u_α represents the value of $u\left(\frac{1}{\alpha}\right) = \beta_0 + \beta_1\left(\frac{1}{\alpha}\right)^2 + \dots + \beta_k\left(\frac{1}{\alpha}\right)^k$ at the α^{th} stress level, $\alpha = 0, 1, \dots, k - 1$. Then $Y_{i,\alpha}$ is the i^{th} order statistic, $i = 1, 2, \dots, m_\alpha$, of a sample of size n_α , $\alpha = 0, 1, \dots, k - 1$, from the distribution of $Y = \frac{X-u}{b}$, the

reduced first asymptotic distribution of smallest values.

Therefore,

$$E[X_{1,\alpha}] = u_\alpha + b E(Y_{1,\alpha}) \quad (2)$$

$$i = 1, 2, \dots, m_\alpha,$$

$$\alpha = 0, 1, \dots, k-1,$$

and Σ_X , the covariance matrix of the X 's, is given by

$$\Sigma_X = b^2 V. \quad (3)$$

Since it is assumed that the failure times at any given testing level are independent of those at any other level,

$$V = b^2 \begin{pmatrix} v_0 & & & \\ & v_1 & & \\ & & \ddots & \\ & & & v_{k-1} \end{pmatrix}, \quad (4)$$

where v_α , $\alpha = 0, 1, \dots, k-1$, is the known covariance matrix of the first m_α of n_α order statistics of the distribution of Y . From (2), (3), and (4), it can be seen that the generalized Gauss-Markov Theorem, given in [4], applies. Hence, least-squares estimators having uniformly minimum variance among unbiased linear estimators can be obtained for u_α and b when $k, m_\alpha, \alpha = 0, 1, \dots, k-1$, and testing levels for stress are fixed. The problem of determining these quantities for optimum estimation is now considered.

DESIGN FOR OPTIMUM ESTIMATION

The information matrix of the Gauss-Markov least-squares curve for any selection of n observations in the interval $c \leq \sigma \leq d$ can be duplicated by choosing at most $k + 1$ distinct stress levels in this interval and allocating the n observations appropriately to these new levels.

We therefore let the number of stress levels (testing levels for the stress) be $k + 1$, and the α^{th} testing level be σ_α , $\alpha = 0, 1, \dots, k$, with $\sigma_0 < \sigma_1 < \dots < \sigma_k$.

If b is not known, it is necessary that m_α be at least 2 for at least one stress level in order that u_α be estimable (an unbiased estimator exist), $\alpha = 0, 1, \dots, k$. This is true because $E(X_{1,\alpha})$ is not equal to u_α , but rather $E(X_{1,\alpha}) = u_\alpha + b E(Y_{1,\alpha})$, with $E(Y_{1,\alpha}) \neq 0$, $\alpha = 0, 1, \dots, k$. Note that if $Z_{i,n}$ is the i^{th} order statistic, $i = 1, 2, \dots, n$, of a size n sample from a reduced Gaussian distribution, $E(Z_{1,1}) = 0$. If b is known, m_α can be 1, $\alpha = 0, 1, \dots, k$. Optimum estimation for b known will be considered in the section following this one.

Let $v^{i,j,\alpha}$ be the element in the $\alpha + i^{\text{th}}$ row and the $\alpha + j^{\text{th}}$ column, $i, j = 1, 2, \dots, m_\alpha$, $\alpha = 0, 1, \dots, k$, of V^{-1} , the inverse matrix of V . It can easily be shown that when m_α observations are made at each of $k + 1$ points, the least-squares estimator $x^*(\frac{1}{\sigma})$ of the expected value of the least-squares curve at $(\frac{1}{\sigma})$,

$x_{1/\sigma, b} = \beta_0 + \beta_1 \left(\frac{1}{\sigma}\right) + \dots + \beta_k \left(\frac{1}{\sigma}\right)^k + x_0(b)$ (with $x_0(b)$ defined below), passes through

$$\frac{1}{\sigma}, \frac{\sum_{j=1}^{m_\alpha} \sum_{i=1}^{m_\alpha} v^{i,j,\alpha} x_{i,\alpha}}{\sum_{j=1}^{m_\alpha} \sum_{i=1}^{m_\alpha} v^{i,j,\alpha}} \quad (5)$$

and can be expressed in the form

$$x^*\left(\frac{1}{\sigma}\right) = \sum_{\alpha=0}^k L_\alpha\left(\frac{1}{\sigma}\right) \frac{\sum_{j=1}^{m_\alpha} \sum_{i=1}^{m_\alpha} v^{i,j,\alpha} x_{i,\alpha}}{\sum_{j=1}^{m_\alpha} \sum_{i=1}^{m_\alpha} v^{i,j,\alpha}} = \sum_{\alpha=0}^k L_\alpha\left(\frac{1}{\sigma}\right) x^*\left(\frac{1}{\sigma}\right), \quad (6)$$

where $L_\alpha\left(\frac{1}{\sigma}\right)$ is the Lagrange polynomial

$$\frac{\left(\frac{1}{\sigma} - \frac{1}{\sigma_0}\right) \dots \left(\frac{1}{\sigma} - \frac{1}{\sigma_{\alpha-1}}\right) \left(\frac{1}{\sigma} - \frac{1}{\sigma_{\alpha+1}}\right) \dots \left(\frac{1}{\sigma} - \frac{1}{\sigma_k}\right)}{\left(\frac{1}{\sigma} - \frac{1}{\sigma_0}\right) \dots \left(\frac{1}{\sigma} - \frac{1}{\sigma_{\alpha-1}}\right) \left(\frac{1}{\sigma} - \frac{1}{\sigma_{\alpha+1}}\right) \dots \left(\frac{1}{\sigma} - \frac{1}{\sigma_k}\right)}, \quad (7)$$

$$\alpha = 0, 1, \dots, k.$$

This represents a generalization of the better known result used by

Hoeffding and Levine in [2], where $m_\alpha = n_\alpha$ and the model is

$$E[W_{i,\alpha}] = u_\alpha = \beta_0 + \beta_1 (z_\alpha) + \dots + \beta_k (z_\alpha)^k, \quad (8)$$

$$i = 1, 2, \dots, n_\alpha,$$

$$\alpha = 0, 1, \dots, k-1,$$

with

$$\Sigma_W = b^2 I, \quad (9)$$

and I the identity matrix. Here, $w_{i,\alpha}$ is the i^{th} Gaussian order statistic, $i = 1, 2, \dots, n_\alpha$, $\alpha = 0, 1, \dots, k-1$, and for $\ell = k+1$,

the least-squares estimator W^* of $w = \sum_{j=0}^k \beta_j z^j$ passes through z_α, \bar{w}_α . W^* can be expressed in the form

$$\sum_{\alpha=0}^k L_\alpha(z) \bar{w}_\alpha,$$

with \bar{w}_α equal to $\frac{1}{n_\alpha} \sum_{i=1}^{n_\alpha} w_{i,\alpha}$, $\alpha = 0, 1, \dots, k$, and $L_\alpha(z)$

defined by (7). It might be noted that $\sum_{\alpha=0}^k L_\alpha(z) = 1$.

The variance $\text{Var}\left(X^*\left(\frac{1}{\sigma}\right)\right)$ of the least-squares estimator $X^*\left(\frac{1}{\sigma}\right)$ of $x_{1/\sigma, b}$ is simply the sum of the variances at the $k+1$ testing levels, or

$$\text{Var}\left(X^*\left(\frac{1}{\sigma}\right)\right) = b^2 \sum_{\alpha=0}^k L_\alpha^2\left(\frac{1}{\sigma}\right) \frac{\sum_{j=1}^{m_\alpha} \sum_{i=1}^{m_\alpha} v_{i,j,\alpha} \sum_{r=1}^{m_\alpha} v_{i,r,\alpha} \sum_{s=1}^{m_\alpha} v_{s,j,\alpha}}{\left(\sum_{j=1}^{m_\alpha} \sum_{i=1}^{m_\alpha} v_{i,j,\alpha}\right)^2}$$

which reduces to

$$\text{Var}\left(X^*\left(\frac{1}{\sigma}\right)\right) = b^2 \sum_{\alpha=0}^k L_\alpha^2\left(\frac{1}{\sigma}\right) / \sum_{j=1}^{m_\alpha} \sum_{i=1}^{m_\alpha} v_{i,j,\alpha}. \quad (10)$$

Here, $v_{i,j,\alpha}$ is the element in the $\alpha + i^{\text{th}}$ row and the $\alpha + j^{\text{th}}$ column, $i, j = 1, 2, \dots, m_\alpha$, $\alpha = 0, 1, \dots, k$, of v .

Let $u^*(\frac{1}{\sigma_\alpha})$ be

$$\frac{-\sum_{s=1}^{m_\alpha} \sum_{r=1}^{m_\alpha} \left[\sum_{j=1}^{m_\alpha} \sum_{i=1}^{m_\alpha} E(Y_{i,\alpha}) v^{i,j,\alpha} E(Y_{r,\alpha}) v^{i,s,\alpha} - \sum_{j=1}^{m_\alpha} \sum_{i=1}^{m_\alpha} E(Y_{i,\alpha}) E(Y_{j,\alpha}) v^{i,j,\alpha} v^{r,s,\alpha} \right] x_{s,\alpha}}{\Delta}$$

and b_α^* be

$$\frac{\sum_{s=1}^{m_\alpha} \sum_{r=1}^{m_\alpha} \left[\sum_{j=1}^{m_\alpha} \sum_{i=1}^{m_\alpha} v^{i,j,\alpha} E(Y_{r,\alpha}) v^{r,s,\alpha} - \sum_{j=1}^{m_\alpha} \sum_{i=1}^{m_\alpha} E(Y_{i,\alpha}) v^{i,j,\alpha} v^{r,s,\alpha} \right] x_{s,\alpha}}{\Delta},$$

where

$$\Delta = \sum_{j=1}^{m_\alpha} \sum_{i=1}^{m_\alpha} v^{i,j,\alpha} \sum_{j=1}^{m_\alpha} \sum_{i=1}^{m_\alpha} E(Y_{i,\alpha}) E(Y_{j,\alpha}) v^{i,j,\alpha} - \left(\sum_{j=1}^{m_\alpha} \sum_{i=1}^{m_\alpha} E(Y_{i,\alpha}) v^{i,j,\alpha} \right)^2.$$

The expressions $u^*(\frac{1}{\sigma_\alpha})$ and b_α^* are the least-squares uniformly minimum-variance unbiased linear estimators of $u(\frac{1}{\sigma})$ and b at the α^{th} sample point. Let the variance of the b_α^* be $\text{Var}(b_\alpha^*)$, the variance of $u^*(\frac{1}{\sigma_\alpha})$ be $\text{Var}(u^*(\frac{1}{\sigma_\alpha}))$, and the covariance of $u^*(\frac{1}{\sigma_\alpha})$ and b_α^* be $\text{Cov}(u^*(\frac{1}{\sigma_\alpha}), b_\alpha^*)$. Then $\text{Var}(x^*(\frac{1}{\sigma_\alpha}))$, as given by (10), can be shown to be equal to

$$[\text{Var}(u^*(\frac{1}{\sigma_\alpha})) - \text{Cov}^2(u^*(\frac{1}{\sigma_\alpha}), b_\alpha^*) / \text{Var}(b_\alpha^*)], \quad (11)$$

and it can also be shown that

$$x^*(\frac{1}{\sigma_\alpha}) = [u^*(\frac{1}{\sigma_\alpha}) - \text{Cov}(u^*(\frac{1}{\sigma_\alpha}), b_\alpha^*) b_\alpha^* / \text{Var}(b_\alpha^*)], \quad (12)$$

for $m_\alpha \geq 2$, $\alpha = 0, 1, \dots, k$. For $m_\alpha = 1$, $X^*\left(\frac{1}{\sigma_\alpha}\right)$ is simply $x_{1,\alpha}$, $\alpha = 0, 1, \dots, k$, with variance $\pi^2 \frac{b^2}{6}$. It can be seen from (12) that

$$x_0(b) \text{ in } x_{1/\sigma_\alpha} = u\left(\frac{1}{\sigma}\right) + x_0(b) \text{ is equal to } -\sum_{\alpha=0}^k L_\alpha\left(\frac{1}{\sigma}\right) \frac{\text{Cov}\left(u^*\left(\frac{1}{\sigma_\alpha}\right), b_\alpha^*\right)}{\text{Var}(b_\alpha^*)} b.$$

The expression (11) also defines, for $m_\alpha \geq 2$, the variance of

$$\bar{w}_\alpha = \sum_{i=0}^{n_\alpha} w_{i,\alpha}, \text{ described by (8) and (9) with } z_\alpha = \frac{1}{\sigma_\alpha} \text{ and } m_\alpha = n_\alpha,$$

where $u^*\left(\frac{1}{\sigma_\alpha}\right)$ and b_α^* are the least-squares best linear unbiased estimators of u and b , respectively, at the α^{th} sample point, $\alpha = 0, 1, \dots, k$.

When the density function of \bar{w}_α is symmetric about the location parameter

u , however, as when $w_{i,\alpha}$, $i = 0, 1, \dots, n_\alpha$, $\alpha = 0, 1, \dots, k$ is a

Gaussian order statistic, then the covariance between the least-squares

estimators $u^*\left(\frac{1}{\sigma_\alpha}\right)$ and b_α^* of the location parameter u_α , $\alpha = 0, 1, \dots, k$,

and the scale parameter b , respectively, is zero, as is shown in [4].

In this case the variance of \bar{w}_α is simply equal to the variance of

$u^*\left(\frac{1}{\sigma_\alpha}\right)$, as in [2], where $u^*\left(\frac{1}{\sigma_\alpha}\right) = \bar{w}_\alpha$, $\alpha = 0, 1, \dots, k$.

For $m_\alpha = 1$, $\text{Var}\left(X^*\left(\frac{1}{\sigma_\alpha}\right)\right) = \text{Var}(x_{1,\alpha}) = \pi^2 b^2 / 6 \approx 1.64493 b^2$. Also it is

possible for any given combination of values of m_α and n_α , $2 \leq m_\alpha \leq n_\alpha$,

to calculate a value for the variance of $X^*\left(\frac{1}{\sigma_\alpha}\right)$ using (11) and the tables

1
Where any m_α is equal to 1, $\frac{\text{Cov}\left(u^*\left(\frac{1}{\sigma_\alpha}\right), b_\alpha^*\right)}{\text{Var}(b_\alpha^*)}$ is taken to be $E(x_{1,\alpha})$,
 $\alpha = 0, 1, \dots, k$.

in [3] for $n_\alpha \leq 6$, [10] for $n_\alpha \leq 20$, or [6] for $n_\alpha \leq 25$. For $m_\alpha = n_\alpha$, one obtains (to within a unit in the fifth decimal place),

n_α	$\text{Var } X^*(\frac{1}{\sigma_\alpha})$
1	1.64493 b^2
2	.65373 b^2
3	.40108 b^2
4	.28810 b^2
.	.
.	.
.	.
$n_\alpha \rightarrow \infty$	b^2/n_α , $\alpha = 0, 1, \dots, k$.

A general expression for $\text{Var } X^*(\frac{1}{\sigma_\alpha})$ in terms of n_α , for $m_\alpha = n_\alpha$, can then be given approximately (to almost within a unit in the second significant figure) by $b^2/(n_\alpha - 0.43)$, $\alpha = 0, 1, \dots, k$.

Let $m_\alpha = n_\alpha$ and $p_\alpha = n_\alpha/n$, $\alpha = 0, 1, \dots, k$, so that $\sum_{\alpha=0}^k p_\alpha = 1$.

The variance of the least-squares estimator $X^*(\eta)$ at the stress level.

$1/\eta$ is of the approximate form

$$(b^2/n) \sum_{\alpha=0}^k L_\alpha^2(\eta)/(p_\alpha - 0.43/n). \quad (13)$$

For any choice of testing levels $\sigma_0, \sigma_1, \dots, \sigma_k$, the approximate variance given by (13) will be minimized, under the constraint

$$\sum_{\alpha=0}^k p_\alpha = 1, \text{ with } 0 \leq p_\alpha \leq 1 \text{ and with } \frac{1}{\eta} \neq \sigma_\alpha, \text{ if}$$

$$p_\alpha = \frac{(1 - 0.43(k+1)/n) |L_\alpha(\eta)|}{\sum_{j=0}^k |L_j(\eta)|} + \frac{0.43}{n}, \quad \alpha = 0, 1, \dots, k. \quad (14)$$

This result is obtained, as is Lemma 1 of [2], simply by standard calculus techniques. If the proportion p_α of the sample assigned to the stress level σ_α is given by (14), the variance of the least-squares estimator is approximately

$$(b^2/n) \left(\sum_{\alpha=0}^k |L_\alpha(\eta)| \right)^2 / (1 - 0.43(k+1)/n) \quad (15)$$

for η as defined.

Clearly, the expression (15) will be minimized if $\sum_{\alpha=0}^k |L_\alpha(\eta)|$ is minimized. Therefore, the theorem below follows immediately from the proof by Hoel and Levine (consisting of a minimization of $\sum_{\alpha=0}^k |L_\alpha(\eta)|$, $\eta > 1/c$) of a similar theorem in [2] for the model given by (8) and (9) plus the normality assumption.

THEOREM I. Under the assumptions (2), (3), and (4), let p_α , given by formula (14), be the proportion of the sample of n items tested at the stress level σ_α , $\sigma_0 \leq \sigma_1 \leq \dots \leq \sigma_k$, in the range $c \leq \sigma_\alpha \leq d$, $\alpha = 0, 1, \dots, k$, and let $1/\eta$ be less than c . The value of $\frac{1}{\sigma_\alpha}$ that will minimize the expression (15) giving the approximate variance of $X^*(\eta)$, the point on the least-squares curve at $\sigma = 1/\eta$, is

$$\frac{1}{\sigma_\alpha} = \left\{ -\cos[(k - \alpha)\pi/k] \right\} \left(\frac{1}{c} - \frac{1}{d} \right)/2 + \left(\frac{1}{c} + \frac{1}{d} \right)/2, \quad \alpha = 0, 1, \dots, k. \quad (16)$$

Theorem I then gives the solution to the problem of obtaining the least-squares curve with minimum-variance intercept at $\sigma = 1/\eta$ under the assumptions (2), (3), and (4). In the following section, properties of this minimum-variance intercept and the least-squares curve in general will be considered.

PROPERTIES OF THE LEAST-SQUARES CURVE UNDER THE GENERAL MODEL

An interesting property of the least-squares curve which holds at the $k + 1$ testing levels is first demonstrated. Consider any distribution with unknown location-scale parameter $\theta = (\theta_1, \theta_2)$ such that $f_\theta(x) = \frac{1}{\theta_2} g\left(\frac{x-\theta_1}{\theta_2}\right)$ for some g . Let θ_1^* and θ_2^* be the unique (with probability 1) uniformly minimum-variance unbiased estimators of θ_1 and θ_2 , respectively, in some class of estimators (linear estimators, for example, or all possible

estimators). Let $A\theta_2^2$ and $C\theta_2^2$ be the variances of θ_1^* and θ_2^* , respectively, and $B\theta_2^2$ their covariance, and let loss be squared error divided by θ_2^2 . It is shown in [7] that (1) for any given function of the form $\Phi = \lambda_1 \theta_1 + \lambda_2 \theta_2$ the unique estimator with smallest expected loss among estimators in the class invariant under transformations of location and scale (when the best unbiased estimator of Φ in the class is $\lambda_1 \theta_1^* + \lambda_2 \theta_2^*$) is

$$\tilde{\Phi} = \lambda_1 \theta_1^* + (\lambda_2 - \lambda_1 B) \theta_2^*/(1+C) \quad (17)$$

and (2) if $\tilde{\Phi}$ is linear in the observed x 's, then it is the unique admissible¹ minimax linear estimator of Φ . The proof of (1) is very similar to the derivation in [6] of the expression for Cramér-Rao type bounds for invariant estimators of location parameters of the form $\theta_1 + \lambda \theta_2$.

Let $\text{Var}\left(u^*\left(\frac{1}{\sigma_\alpha}\right)\right)$ be $A_\alpha b^2$, $\text{Var}(b_\alpha^*)$ be $C_\alpha b^2$, and $\text{Cov}\left(u^*\left(\frac{1}{\sigma_\alpha}\right), b_\alpha^*\right)$ be $B_\alpha^2 b^2$. Then, by (17), the unique admissible¹ minimax linear estimators of u_α and b at the α^{th} stress level are $\tilde{u}\left(\frac{1}{\sigma_\alpha}\right) = u^*\left(\frac{1}{\sigma_\alpha}\right) - B_\alpha b_\alpha^*/(1+C_\alpha)$ and $\tilde{b}_\alpha = b_\alpha^*/(1+C_\alpha)$, respectively, $\alpha = 0, 1, \dots, k$. Furthermore, it can be very readily seen that $X^*\left(\frac{1}{\sigma_\alpha}\right) = u^*\left(\frac{1}{\sigma_\alpha}\right) - B_\alpha b_\alpha^*/C_\alpha$ can also be expressed as $X^*\left(\frac{1}{\sigma_\alpha}\right) = \tilde{u}\left(\frac{1}{\sigma_\alpha}\right) - B_\alpha \tilde{b}_\alpha/C_\alpha$, and that $X^*\left(\frac{1}{\sigma_\alpha}\right)$ is the best

¹The proof of linear admissibility for $\tilde{\Phi}$, which had been shown in [5] to be the best linear invariant estimator of Φ , was outlined in detail to this author by M. R. Mickey of the University of California at Los Angeles by personal communication.

linear invariant estimator of $x_{1/\sigma_\alpha, b}$, its expected value, $\alpha = 0, 1, \dots, k$. This result is related to the fact that $X^*(\frac{1}{\sigma_\alpha})$ and b_α^* have zero covariance, $\alpha = 0, 1, \dots, k$.

Another property of the least-squares curve which will be demonstrated below is the following. Under the assumptions (2), (3), and (4), there exists no linear combination of the ordered observations at stress level σ_α and no point $u_\alpha + \zeta b$, $-\infty < \zeta < \infty$, along the $\frac{1}{\sigma_\alpha}$ ordinate such that the expected squared deviation of this linear combination from $u_\alpha + \zeta b$ is smaller than that of $X^*(\frac{1}{\sigma_\alpha})$, the intercept of the least-squares curve at $\sigma = \sigma_\alpha$, from its expected value,

$$x_{1/\sigma_\alpha, b} = \beta_0 + \beta(\frac{1}{\sigma_\alpha}) + \dots + \beta_k(\frac{1}{\sigma_\alpha})^k + \epsilon_0(b),$$

for at least one combination of values of u_α and b and at least as small for all combinations of values of u_α and b , $\alpha = 0, 1, \dots, k$. We say then that the "admissibility" of the linear combination $X^*(\frac{1}{\sigma_\alpha})$ will be demonstrated.

It will also be shown that when loss is squared error divided by b^2 , $X^*(\frac{1}{\sigma_\alpha})$ is a minimax linear combination of the observations (has smaller maximum expected loss from $x_{1/\sigma_\alpha, b}$ as a function of u_α and b than any other linear combination from any point $u_\alpha + \zeta b$, $-\infty < \zeta < \infty$, along the $\frac{1}{\sigma_\alpha}$ ordinate), $\alpha = 0, 1, \dots, k$. Properties of the least-squares curve at $\sigma = \frac{1}{\eta}$ will also be demonstrated.

Let $X_T^*(\eta)$ be the intercept on the least-squares curve at $\sigma = \frac{1}{\eta}$ when n observations are made at $\sigma_1 \leq \sigma_2 \leq \dots \leq \sigma_k$, with $c \leq \sigma_\alpha \leq d$ and $\frac{1}{\eta} < c$, and when σ_α and p_α , the proportion of the n failure times observed at the α^{th} level, are those specified by Theorem I. Assume (13) gives the exact variance of $X_T^*(\eta)$, defined by (10). The following theorem will now be proved.

THEOREM II. Let loss be squared error divided by b^2 . Under the assumptions (2), (3) and (4), $X^*\left(\frac{1}{\sigma_\alpha}\right)$, the intercept of the least-squares curve at $\frac{1}{\sigma_\alpha}$, is the unique admissible minimax linear combination of the ordered observations made at $\sigma = \sigma_\alpha$. $X_T^*(\eta)$, defined above, is the unique admissible minimax linear combination of n observations extrapolated to $\sigma = \frac{1}{\eta}$, when it is assumed that (15) gives its exact variance. $X_T^*(\eta)$ is also the linear function with uniformly smallest expected loss of best linear invariant estimators of u and b at $k+1$ stress levels at which life testing may occur, extrapolated to $\sigma = \frac{1}{\eta}$ (when it is assumed that (15) gives the exact variance of $X_T^*(\eta)$).

PROOF

Each of the statements in the demonstration of the proof of the first statement of Theorem II holds for $\alpha = 0, 1, \dots, k$. Let us suppose that there exists a linear function $\bar{X}\left(\frac{1}{\sigma_\alpha}\right)$ of the ordered observations

$x_{1,\alpha}, x_{2,\alpha} \dots, x_{n_\alpha, \alpha}$ and a point $u_\alpha + \zeta b$, $-\infty < \zeta < \infty$, along the $\frac{1}{\sigma_\alpha}$ coordinate, such that the expected squared deviation of $\bar{x}\left(\frac{1}{\sigma_\alpha}\right)$ from $u_\alpha + \zeta b$ is at least as small as that of $X^*\left(\frac{1}{\sigma_\alpha}\right)$ from $x_{1/\sigma_\alpha, b}$ for all combinations of values of u_α and b and smaller for at least one combination of values of u_α and b . Hence it is supposed that $X^*\left(\frac{1}{\sigma_\alpha}\right)$ is an inadmissible linear combination of the ordered observations.

Suppose that $\bar{x}\left(\frac{1}{\sigma_\alpha}\right)$ is not of the form $\ell_1 u^*\left(\frac{1}{\sigma_\alpha}\right) + \ell_2 b_\alpha^*$. Then by the generalized Gauss-Markov Theorem [4] there exists $\tilde{x}\left(\frac{1}{\sigma_\alpha}\right)$ of the form $\ell_1 u^*\left(\frac{1}{\sigma_\alpha}\right) + \ell_2 b_\alpha^*$ such that $E\left(\tilde{x}\left(\frac{1}{\sigma_\alpha}\right)\right) = E\left(\bar{x}\left(\frac{1}{\sigma_\alpha}\right)\right)$ and $\text{Var}\left(\tilde{x}\left(\frac{1}{\sigma_\alpha}\right)\right) < \text{Var}\left(\bar{x}\left(\frac{1}{\sigma_\alpha}\right)\right)$

for all u_α and b . Thus,

$$\text{Var}\left(\tilde{x}\left(\frac{1}{\sigma_\alpha}\right)\right) + \left[E\left(\tilde{x}\left(\frac{1}{\sigma_\alpha}\right)\right) - (u_\alpha - \zeta b) \right]^2 < \text{Var}\left(\bar{x}\left(\frac{1}{\sigma_\alpha}\right)\right) + \left[E\left(\bar{x}\left(\frac{1}{\sigma_\alpha}\right)\right) - (u_\alpha - \zeta b) \right]^2$$

for all u_α and b . Hence, it may as well be supposed that

$$\tilde{x}\left(\frac{1}{\sigma_\alpha}\right) = s_{1,\alpha} u^*\left(\frac{1}{\sigma_\alpha}\right) + s_{2,\alpha} b_\alpha^*$$

Then the expected loss function for $\tilde{x}\left(\frac{1}{\sigma_\alpha}\right)$ is

$$s_{1,\alpha}^2 A_\alpha + 2s_{1,\alpha} s_{2,\alpha} B_\alpha + s_{2,\alpha}^2 C_\alpha + [(s_{1,\alpha} - 1)u_\alpha + (s_{2,\alpha} - \zeta)b]^2 / b^2$$

which is assumed to be less than $A_\alpha - B_\alpha^2/C_\alpha$ for all u_α and b . The value of $s_{1,\alpha}$ must then be equal to 1 if this inequality is to hold identically in u_α and b .

Thus, it is assumed that $\bar{X}\left(\frac{1}{\sigma_\alpha}\right) = u^*\left(\frac{1}{\sigma_\alpha}\right) + s_{2,\alpha} b_\alpha^*$ with expected loss given by

$$A_\alpha + 2s_{2,\alpha} B_\alpha + s_{2,\alpha}^2 C_\alpha + (s_{2,\alpha} - \zeta)^2 \quad (18)$$

The expression (18) is minimized with respect to ζ and $s_{2,\alpha}$ jointly when $\zeta = s_{2,\alpha} = -B_\alpha/C_\alpha$. Hence $X^*\left(\frac{1}{\sigma_\alpha}\right)$ is an admissible linear combination of the observations at the α^{th} stress level, $\alpha = 0, 1, \dots, k$.

The proof of admissibility for $X^*\left(\frac{1}{\sigma_\alpha}\right), \alpha = 0, 1, \dots, k$, is similar to that referred to in the footnote on page 33. An alternative proof would begin with a demonstration that for every biased linear combination of the observations, there exists an unbiased combination with smaller risk (expected loss).

Suppose $X^*\left(\frac{1}{\sigma_\alpha}\right)$ is not a minimax-risk linear combination of the observations. Then there exists a linear combination having maximum risk smaller than that of $X^*\left(\frac{1}{\sigma_\alpha}\right)$, which has constant risk with respect to u_α and b , $\alpha = 0, 1, \dots, k$, since loss is squared error divided by b^2 . The existence of such an estimator would thus imply that $X^*\left(\frac{1}{\sigma_\alpha}\right), \alpha = 0, 1, \dots, k$, was inadmissible. Hence $X^*\left(\frac{1}{\sigma_\alpha}\right)$ is the unique (with probability 1) admissible minimax linear combination of the observations at the α^{th} stress level, $\alpha = 0, 1, \dots, k$. The uniqueness follows from the uniqueness of $u^*\left(\frac{1}{\sigma_\alpha}\right)$ and b_α^* , $\alpha = 0, 1, \dots, k$.

Now, consider

$$X_T^*(\eta) = \sum_{\alpha=0}^k L_\alpha(\eta) \left[u^*\left(\frac{1}{\sigma_\alpha}\right) - B_\alpha b_\alpha^*/C_\alpha \right],$$

the least-squares intercept at $\sigma = \frac{1}{\eta}$, where p_α , which represents the proportion of the n sample values tested at $\frac{1}{\sigma_\alpha}$, and $\frac{1}{\sigma_\alpha}$, $\alpha = 0, 1, \dots, k$, are chosen according to the specifications of Theorem I. It is assumed that $c \leq \sigma_\alpha \leq d$, $\alpha = 0, 1, \dots, k$, and $\frac{1}{\eta} < c$.

Let $\bar{X}(\eta) = \sum_{\alpha=0}^k L_\alpha(\eta) \sum_{i=1}^{n_\alpha} a_{i,\alpha} X_{i,\alpha}$, with $\sum_{\alpha=0}^k n_\alpha = n$, estimate a point $u(\eta) + \zeta b$, $-\infty < \zeta < \infty$, on the ordinate η . Suppose that a_i , $i = 1, 2, \dots, n_\alpha$, $p_\alpha = n_\alpha/n$, and σ_α , $\alpha = 0, 1, \dots, k$, are chosen so that the mean squared deviation of $\bar{X}(\eta)$ from $u(\eta) + \zeta b$ is less than or equal to the variance of $X_T^*(\eta)$ for all b , $u(\eta)$, and u_α , $\alpha = 0, 1, \dots, k$. Suppose that the expectation of $\bar{X}(\eta)$ is not $u(\eta) + \zeta b$. Then the expected squared deviation of $\bar{X}(\eta)$ from its expected value is less than that of $\bar{X}(\eta)$ from $u(\eta) + \zeta b$. Hence, it is assumed that $E(\bar{X}(\eta)) = u(\eta) + \zeta b$ for all b , $u(\eta)$, and $u\left(\frac{1}{\sigma_\alpha}\right)$, $\alpha = 0, 1, \dots, k$. Then when $\bar{X}(\eta)$ is of the form

$$\sum_{\alpha=0}^k L_\alpha(\eta) \left[u^*\left(\frac{1}{\sigma_\alpha}\right) + \tau_\alpha b_\alpha^* \right], \quad (19)$$

with variance

$$b^2 \sum_{\alpha=0}^k \left[L_\alpha^2(\eta) (A_\alpha + 2\tau_\alpha B_\alpha + \tau_\alpha^2 C_\alpha) \right], \quad (20)$$

it has uniformly smaller variance than any other linear combination with

uniform expectation $u(\eta) + \sum_{\alpha=0}^k L_\alpha(\eta) \tau_\alpha b = u(\eta) + \zeta b$ for any specified

combination of testing levels and allocation of the sample to the

$k+1$ levels. If any n_α is equal to 1, $u^*\left(\frac{1}{\sigma_\alpha}\right) + \tau_\alpha b_\alpha^*$ is taken to be $x_{1,\alpha}$ with variance $\pi^2 b^2/6$, $\alpha = 0, 1, \dots, k$.

The variance of $\tilde{x}(\eta)$ is minimized independently of the value of p_α

and $\frac{1}{\sigma_\alpha}$, $\alpha = 0, 1, \dots, k$ if $\tau_\alpha = -B_\alpha/C_\alpha$. Hence, $x^*(\eta)$ is admissible

among linear combinations of n sample observations when $\frac{1}{\sigma_\alpha}$

and τ_α , $\alpha = 0, 1, \dots, k$, are fixed. Then by Theorem I and the

reasoning applied in proving the first statement of this theorem, $x_T^*(\eta)$

is the unique admissible minimax linear combination of n sample failure-

time logarithms observed at $\sigma_1, \sigma_2, \dots, \sigma_k$, $c \leq \sigma_\alpha \leq d$, $\alpha = 0, 1, \dots, k$,

and extrapolated to $\sigma = \frac{1}{\eta}, \frac{1}{\eta} < c$ (under the assumption that (15) gives the exact variance of $x^*(\eta)$).

On the basis of the preceding derivation and the assumption (concerning

the variance of $x^*(\eta)$) it follows immediately that

$$x_T^*(\eta) = \sum_{\alpha=0}^k L_\alpha(\eta) \left[u^*\left(\frac{1}{\sigma_\alpha}\right) - \frac{B_\alpha b_\alpha^*}{(1+C_\alpha)} - \frac{B_\alpha b_\alpha^*}{C_\alpha(1+C_\alpha)} \right], \text{ with expectation}$$

$\sum_{\alpha=0}^k L_\alpha(\eta) \left[u_\alpha - \frac{B_\alpha b}{1+C_\alpha} - \frac{B_\alpha b}{C_\alpha(1+C_\alpha)} \right]$ and variance $\sum_{\alpha=0}^k L_\alpha(\eta) \left[A_\alpha - B_\alpha^2/C_\alpha \right]$, is

the linear combination with uniformly smallest expected loss of best linear invariant estimators of u and b at $k+1$ stress levels at which life testing may occur, extrapolated to $\sigma = \frac{1}{\eta}$. It is interesting to note that when the model is given by (8) and (9) plus the assumption of a Gaussian distribution for the observations,

$b^2 \sum_{\alpha=0}^k L_\alpha^2(\eta)/n_\alpha$ is the exact variance of $X^*(\eta) = \sum_{\alpha=0}^k L_\alpha \sum_{i=1}^{n_\alpha} z_{i,\alpha}$.

A COMPARISON OF THE TRADITIONAL AND THE DERIVED DESIGNS

As an illustration of the result given by Theorem I, consider the following example. It is assumed that u is of the form $B_0 + B_1 \left(\frac{1}{\sigma}\right) + B_2 \left(\frac{1}{\sigma}\right)^2 + B_3 \left(\frac{1}{\sigma}\right)^3 + B_4 \left(\frac{1}{\sigma}\right)^4$ and that 10 items are to be tested until failure over the stress interval $\frac{1}{3\sqrt{2}} \leq \sigma \leq \frac{1}{\sqrt{2}}$. Using a traditional design specifying equal numbers of items tested at equal intervals over the testing domain, one obtains the following.

$$\begin{array}{lllll} \frac{1}{\sigma_4} = \sqrt{2} & \frac{1}{\sigma_3} = 3\sqrt{2}/2 & \frac{1}{\sigma_2} = 2\sqrt{2} & \frac{1}{\sigma_1} = 5\sqrt{2}/2 & \frac{1}{\sigma_0} = 3\sqrt{2} \\ n_4 = 2 & n_3 = 2 & n_2 = 2 & n_1 = 2 & n_0 = 2 \end{array}$$

For optimum estimation at $\sigma = \frac{1}{4\sqrt{2}}$, the theorem specifies approximately the design given below.

$$\frac{1}{\sigma_4} = \sqrt{2} \quad \frac{1}{\sigma_3} = 2\sqrt{2}-1 \quad \frac{1}{\sigma_2} = 2\sqrt{2} \quad \frac{1}{\sigma_1} = 2\sqrt{2}+1 \quad \frac{1}{\sigma_0} = 3\sqrt{2}$$

$$n_4 = 1 \quad n_3 = 2 \quad n_2 = 2 \quad n_1 = 3 \quad n_0 = 2.$$

The least-squares curves for the two sets of 10 observations have variances at $\sigma = \frac{1}{4\sqrt{2}}$ equal to approximately (to the nearest integer) $2912 b^2$ for the traditional design and $1238 b^2$ for the derived design specified by the theorem.

It is shown in [7] that for b known, the best linear invariant estimator of u_α , for $n_\alpha \geq 2$, is $\hat{u}\left(\frac{1}{\sigma_\alpha}\right) = u^*\left(\frac{1}{\sigma_\alpha}\right) - (B_\alpha/C_\alpha)(b_\alpha^* - b)$, with mean squared error (variance, since $\hat{u}\left(\frac{1}{\sigma_\alpha}\right)$ is unbiased) $[A_\alpha - B_\alpha^2/C_\alpha] b^2$,

$\alpha = 0, 1, \dots, k$. The variance values given above for the two designs are, therefore, also appropriate for $\hat{u}(\eta) = \sum_{\alpha=0}^k L_\alpha(\eta) \left[X^*\left(\frac{1}{\sigma_\alpha}\right) + (B_\alpha/C_\alpha)b \right]$,

with B_α/C_α taken to be $-E(Y_{1,\alpha})$ for any n_α equal to 1, $\alpha = 0, 1, \dots, k$.

If b is not known, then the best linear unbiased estimator of this parameter based on any given design can easily be shown to be

$\sum_{\alpha=0}^k \frac{b_\alpha^*/C_\alpha}{\sum_{\alpha=0}^k \left(\frac{1}{C_\alpha}\right)}$, with variance $b^2 / \sum_{\alpha=0}^k \left(\frac{1}{C_\alpha}\right)$. The best linear invariant

estimator of b based on any given design is then

$$\frac{\sum_{\alpha=0}^k b_{\alpha}^*/c_{\alpha}}{\sum_{\alpha=0}^k \left(\frac{1}{c_{\alpha}}\right) \left(1 + 1/\sum_{\alpha=0}^k \left(\frac{1}{c_{\alpha}}\right)\right)} = \frac{\sum_{\alpha=0}^k b_{\alpha}^*/c_{\alpha}}{1 + \sum_{\alpha=0}^k \left(\frac{1}{c_{\alpha}}\right)}$$

with mean squared error given by

$$b^2 / \left(1 + \sum_{\alpha=0}^k \left(\frac{1}{c_{\alpha}}\right)\right)$$

For the traditional design the variance of the best linear unbiased estimator of b is $0.142 b^2$ and the mean squared error of the best linear invariant estimator is $0.125 b^2$. For the derived design, the two corresponding values for the expected squared deviation for estimators of b are based on those obtained at only the four stress levels for which n_{α} , $\alpha = 0, 1, \dots, k$, is greater than 1. They are equal to $0.141 b^2$ and $0.124 b^2$, respectively.

The uniformly minimum-variance unbiased estimator of u at $\sigma = \frac{1}{\sqrt{k}}$ under either model is $u^*(\eta) = \sum_{\alpha=0}^k L_{\alpha}(\eta) u^*\left(\frac{1}{\sigma_{\alpha}}\right)$, where for any n_{α} equal to 1, $u^*\left(\frac{1}{\sigma_{\alpha}}\right)$ will be taken to be $x_{1,\alpha} - E(Y_{1,\alpha}) \sum_{i=0}^k a_{i,\alpha} b_i^*$, with

$$a_{i,\alpha} = \frac{L_{\alpha}(\eta)E(Y_{1,\alpha})/c_i + \sum_{j=1}^k [L_i(\eta)b_j/(c_i c_j) - L_j(\eta)b_i/(c_i c_j)]}{L_{\alpha}(\eta)E(Y_{1,\alpha}) \sum_{j=1}^k (1/c_j)}, \quad \alpha = 0, 1, \dots, k.$$

Here, the number of coefficients of the form $a_{1,\alpha}$ at the α^{th} level is equal to 1 minus the number of testing levels for which n_α is equal to 1; and $E(Y_{1,\alpha})$ is the negative of Euler's constant, or approximately $-.577216, \alpha = 0, 1, \dots, k$. For the traditional model the variance of $u^*(\eta)$ is $2936 b^2$, and for the derived model it is $1248 b^2$. The amount of improvement obtained by using the best linear invariant estimator of $u(\eta)$ rather than $u^*(\eta)$ is trivial in both of these cases.

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APPENDIX B

EXACT THREE-ORDER-STATISTIC CONFIDENCE BOUNDS ON RELIABILITY PARAMETERS UNDER WEIBULL ASSUMPTIONS

INTRODUCTION

Assume that a random sample of n items is subjected to a life test until m (with $2 \leq m \leq n \leq 25$) of the items have failed. Assume further that the random variable T which represents an observable failure time from the population from which the sample of failure times is selected has the two-parameter Weibull density given by

$$\lim_{\Delta t \rightarrow 0} \frac{P[t < T \leq t + \Delta t]}{\Delta t} = f_{\delta, b}(t) = \begin{cases} (1/\delta b)(t/\delta)^{(1/b)-1} \exp[-(t/\delta)^{1/b}], & t > 0 \\ 0, & \text{otherwise} \end{cases}$$

with δ and b both positive. (1)

There are two related problems which are among the most important associated with the life-testing situation. First, one may suppose that a required life t_g is specified and a lower confidence bound, based on the censored sample, is sought for reliability or the survival proportion, $R(t_g) = \exp\{-(t_g/\delta)^{1/b}\}$, at time t_g . For the second and alternative problem a survival proportion R is given. Then a lower confidence bound is sought for $t_R = \delta(\log(1/R))^{1/b}$, the reliable life corresponding to R or, equivalently, for $x_R = u + b \log \log(1/R)$, the log reliable life, where u is equal to $\log \delta$ and all logarithms are natural. The

parameter u is a location parameter of the distribution of $X = \log T$, and b is a scale parameter of this distribution.¹ The bounds for t_R and x_R are often referred to as lower tolerance limits, and are confidence bounds for the $100(1-R)$ percent points of the distributions of T and of X , respectively, where R is the specified proportion between 0 and 1.

A method of obtaining confidence bounds on reliability parameters widely used for the Weibull distribution as well as for many others is as follows. Consider the observed ordered failure times $T_1 \leq T_2 \leq \dots \leq T_n$. For any T_k , a lower confidence bound on $R(T_k)$ at level $1 - \alpha$ can be obtained from $v_\alpha(n-k+1, k)$, the 100α percent point of the beta distribution with $n-k+1$ and k degrees of freedom (see Xiao and Goode [1]). This bound serves also as a conservative $(1 - \alpha)$ -level bound for $R(t_g)$, for any $t_g < T_k$. Similarly, if $v_\alpha(n-k+1, k)$ is greater than R for some k , a lower confidence bound on t_R , with level at least $1 - \alpha$, is given by the k^{th} observed failure time T_k .

This method, however, makes no use of information concerning the form of the underlying distribution of the populations sampled. It is in fact a nonparametric method requiring only the assumption that the unordered observations are independent and identically and continuously distributed. It seems likely that one could obtain improved bounds on the reliability parameters by assuming (correctly) that sampling is from the two-parameter Weibull distribution. In particular, one would ex-

¹ The distribution of the random variable X is the extreme-value distribution of smallest values.

pect a possible improvement when the required life t_g is small compared with the sample failure time which immediately follows it, or in the case in which a tolerance limit is desired, when v_{α} greatly exceeds R . If R is larger than any v_{α} , the nonparametric method is, in fact, completely inapplicable. In the following discussion, other methods for obtaining bounds are derived.

TESTS AND CONFIDENCE SETS FOR THE PARAMETER b

TESTS AND CONFIDENCE SETS BASED ON ALL THE ORDER STATISTICS

The two parameters, reliability and reliable life, for which confidence bounds are sought are

$R(t_g) = \exp\{-(t_g/\delta)^{1/b}\}$ and $x_R = u + b \log \log (1/R)$ or $t_R = \delta(\log(1/R))^b$, respectively. Thus, both are simply functions of the parameters δ (or u) and b . Therefore, bounds on the reliability parameters can be determined from distribution percentage points corresponding to appropriate functions of estimates of δ (or u) and b .

First consider estimates of b (functions of $T_1 \leq T_2 \leq \dots \leq T_n$) and confidence bounds, based on these estimates, which can be placed on b alone. The problem of obtaining such bounds, or tests from which such bounds are derived, is invariant under a change in scale in the time space or a change of location in log time space. A maximal invariant under this transformation is $Z = (z_2, z_3, \dots, z_n) = (T_2/T_1, T_3/T_1, \dots,$

T_m/T_1) or equivalently, $\log Z = [\log(T_2/T_1), \log(T_3/T_1), \dots, \log(T_m/T_1)] = (X_2 - X_1, X_3 - X_1, \dots, X_m - X_1)$. Hence, tests concerning b and confidence bounds on b will be independent of δ or u if and only if they depend on T_1, T_2, \dots, T_m or X_1, X_2, \dots, X_m^1 only through Z .

The joint probability density function of $T_1 \leq T_2 \leq \dots \leq T_m$ is given by

$$f_{\delta, b}(t_1, t_2, \dots, t_m) = \frac{n!}{(n-m)!} \left(\frac{1}{b\delta}\right)^m \prod_{i=1}^m \left(\frac{t_i}{\delta}\right)^{(1/b)-1} \exp \left\{ - \left[\sum_{i=1}^{m-1} \left(\frac{t_i}{\delta}\right)^{1/b} + (n-m+1) \left(\frac{t_m}{\delta}\right)^{1/b} \right] \right\}, \quad 0 \leq t_1 \leq t_2 \leq \dots \leq t_m \leq t_n, \quad (2)$$

so that the joint density of $Z_2 \leq Z_3 \leq \dots \leq Z_m$ is

$$f_b(z_2, z_3, \dots, z_m) = \frac{n!(m-1)!}{(n-m)!} \left(\frac{1}{b}\right)^{m-1} \frac{\prod_{i=2}^m z_i^{(1/b)-1}}{\left[1 + \sum_{i=2}^{m-1} z_i^{1/b} + (n-m+1)z_m^{1/b} \right]^m}, \quad 1 \leq z_2 \leq z_3 \leq \dots \leq z_m. \quad (3)$$

Consider any invariant test $\Phi = \Phi(Z)$ of $H: b \geq b_0$ versus $K: b < b_0$ which accepts H when $\Phi = 0$ and rejects H when $\Phi = 1$. One chooses a significance level α , $0 < \alpha < 1$, and looks for an invariant test which rejects H with probability $\leq \alpha$ when $b \geq b_0$ and which, in some sense, maximizes

¹ X_1, X_2, \dots, X_m are order statistics from the extreme-value distribution of smallest values, the distribution of the random variate $X = \log T$.

the power $\beta_p(b)$ (or probability of rejecting H_0) when $b < b_0$. The boundary of the acceptance region of a uniformly most powerful invariant test δ_0 (most powerful against all alternative hypotheses) yields a uniformly most accurate invariant upper bound \bar{b}_{\min} for b . Thus, $P_b\{b \leq \bar{b}_{\min}\} \geq 1-\alpha$ for all b , and furthermore, for any $b' > b$, $P_b\{\bar{b}_{\min} \geq b'\}$ is minimum among tests based on Z . It can be demonstrated that the Neyman-Pearson Fundamental Lemma (Lehmann [2]) applied to (3) for a given n and $m > 2$ and given simple hypothesis, $b = b_0$, will yield a most powerful invariant test which varies accordingly as the simple alternative $b = b_1$ changes. Thus, there is no test of H which is uniformly most powerful among invariant tests for all alternatives.

One might then naturally consider basing tests and confidence sets on estimators of b which have certain optimality properties in terms of their ability to estimate. From [3], [4] and [5] it might be concluded that likely candidates for such bases for tests, etc., would be the best linear invariant estimator and the maximum-likelihood estimator. Unfortunately, however, the derivations of the distributions of these estimators of b , u , and $x_R = u + b \log \log(1/R)$ for $m > 2$ are very difficult, if not impossible, to obtain except by simulation methods.¹

¹ Tables from which one may obtain confidence bounds on $R(t_g)$ or on t_R have been computed by Johns and Lieberman [6] by simulating the distribution of a function of approximations to the best linear invariant estimates of u and b . These tables can be used for n equal to 10, 15, 20, 30, 50, and 100, and 4 values of m for each n .

A locally most powerful invariant test depends upon the maximum-likelihood estimator of b .

Thus, one is faced with a situation in which statistics which may possibly be optimum in terms of their ability to estimate have not provided an analytical basis for exact tests concerning, or exact confidence bounds on, the parameters they are estimating.

One is thus led to consider estimators whose distributions can be determined exactly and then to compare the properties of these estimators with those of the best linear invariant estimators, the expected loss of which is known or can be calculated for $n \leq 25$. We first perform the following derivation proceeding from (3). Let $v_1 = 1$, $v_j = z_j^{1/b}$, $j = 2, 3, \dots, n$. Then,

$$f(v_2, v_3, \dots, v_n) = \frac{n!(n-1)!}{(n-n)!} \frac{1}{\left[n + \sum_{i=2}^n (n-i+1)(v_i - v_{i-1}) \right]^n} \quad (4)$$

$$1 = v_1 \leq v_2 \leq \dots \leq v_n.$$

Thus, if

$$F = \sum_{i=2}^n \frac{n-i+1}{n(n-1)} (v_i - v_{i-1}) = \sum_{i=2}^n \frac{n-i+1}{n(n-1)} (z_i^{1/b} - z_{i-1}^{1/b}),$$

then

$$f(F) = \frac{(n-1)^n F^{n-2}}{[1+(n-1)F]^n}, \quad F \geq 0, \quad (5)$$

or

$$F^0 = \sum_{i=2}^m \frac{n-i+1}{n(m-1)} \left(z_i^{1/b_0} - z_{i-1}^{1/b_0} \right)$$

is distributed as $F[2(m-1), 2]$, Snedecor's

F with $2(m-1)$ and 2 degrees of freedom, when $b = b_0$. A test Φ_A , at level α , based on the statistic F^0 will therefore reject $H: b \geq b_0$ when

$$\sum_{i=2}^m \frac{n-i+1}{n(m-1)} \left(z_i^{1/b_0} - z_{i-1}^{1/b_0} \right)$$

is less than $F_\alpha[2(m-1), 2]$, the 100α percent point

of the F distribution with the appropriate number of degrees of freedom. The value of $F_\alpha[2(m-1), 2]$ as a function of α and m can be calculated by letting

$$W^0 = [1 + (m-1)F^0]^{-1} = n \left[1 + \sum_{i=2}^{m-1} z_i^{1/b_0} + (n-m+1)z_m^{1/b_0} \right]^{-1}$$

and finding the distribution of W^0 when $b = b_0$. From (5) one obtains

$$f(v^0) = (m-1)(1-v^0)^{m-2}, \quad 0 \leq v^0 \leq 1,$$

and

$$P[F^0 \leq F_\alpha[2(m-1), 2]] = P[W^0 \geq \bar{W}^0] = (1-\bar{W}^0)^{m-1}. \quad (6)$$

If (6) is set equal to α , then \bar{W}^0 is seen to be $1 - \alpha^{1/(m-1)}$ and

$$F_\alpha[2(m-1), 2] \text{ is equal to } \frac{1}{m-1} \frac{\alpha^{1/(m-1)}}{1 - \alpha^{1/(m-1)}}.$$

An upper confidence bound at level $1-\alpha$ for b may be obtained by setting

$$F = \frac{\sum_{i=2}^m (n-i+1)(z_i^{1/b} - z_{i-1}^{1/b})}{n(m-1)}$$

equal to $F_\alpha[2(m-1), 2]$ and solving for b .

One then uses some good estimate of b as a first approximation and Newton-Raphson iteration procedures until $F-F_\alpha[2(m-1), 2]$ is sufficiently small.

TESTS AND CONFIDENCE SETS BASED ON TWO ORDER STATISTICS

Next it will be demonstrated that, for m sufficiently small, a family of confidence bound based on $Z_m = T_m/T_1$ alone is preferable to that based on the test $\hat{\epsilon}_A$ (just derived). To obtain the density function for Z_m , one may successively integrate out $Z_2^{1/b}, Z_3^{1/b}, \dots, Z_{m-1}^{1/b}$ from (3). Thus,

$$f(z_m) = \frac{n!}{(n-m)!(m-2)!} \sum_{k=0}^{m-2} \frac{(-1)^k}{b^k} \binom{m-2}{k} \frac{z_m^{(1/b)-1}}{[(m-k-1)+(n-m-k+1)z_m^{1/b}]^2}, \quad (7)$$

$$1 \leq z_m < \infty.$$

Now, let $V = Z_m^{1/b} \geq 1$. A test $\hat{\epsilon}_1$ based on Z_m , therefore, rejects $H: b \geq b_0$ whenever $V_0 = Z_m^{1/b}$ is less than $C_1(\alpha)$ (or $\log Z_m$ is less than $b_0 \log C_1(\alpha)$), with $C_1(\alpha)$ determined from the expression

$$\frac{n!}{(n-m)!(m-2)!} \sum_{k=0}^{m-2} \frac{(-1)^k}{b^k} \binom{m-2}{k} \frac{1/(n-m+k+1)}{[(m-k-1)+(n-m+k+1)C_1(\alpha)]} = 1 - \alpha. \quad (8)$$

An upper confidence bound $\bar{b}_1(\alpha)$ for b will then be given by

$\bar{b}_1(\alpha) = \log Z_m / \log C_1(\alpha) = \log Z_m / \log C_1(\alpha)$. In order to ascertain whether there is a unique root of the equation (8) which is greater than unity, let $D_1(\alpha) = C_1(\alpha) - 1$ and reject H when $Z_m^{1/b} - 1 < D_1(\alpha)$.

Then (8) may be expressed as a function of $D_1(\alpha)$

$$\frac{n!}{(n-m)!(m-2)!} \sum_{k=0}^{m-2} (-1)^k \binom{m-2}{k} \frac{1/(n-m+k+1)}{[n+(n-m+k+1)D_1(\alpha)]} = 1-\alpha$$

or as a polynomial $g(D_1(\alpha))$ given by

$$(1-\alpha) D_1(\alpha) \sum_{k=1}^{m-1} \binom{m-1}{k} (n-m+k) - \alpha \left\{ D_1(\alpha) \sum_{i=1}^{m-2} n \sum_{k=1}^{m-1} \binom{m-1}{k} (n-m+k) \right. \\ \left. + \dots + D_1(\alpha) \sum_{i=1}^{m-2} n^{m-2-i} (n-m+i) + n^{m-1} \right\} = 0 . \quad (9)$$

For $0 < \alpha < 1$, the coefficient of the first term of the polynomial is positive and each of the remaining $m-1$ terms is negative. Thus by Descartes' Rule of Signs [7], there is no more than one positive root. Also, since $g(0) < 0$ and $g(D_1(\alpha))$, for $D_1(\alpha)$ very large, is positive, there is at least one positive root. Therefore, there is a unique $D_1(\alpha) > 0$ and a unique $C_1(\alpha) = D_1(\alpha) + 1 > 1$.

It can be easily demonstrated from equation (9) that when n is

$$\text{sufficiently large compared with } m, D_1(\alpha) = \frac{\alpha^{1/(m-1)}}{1 - \alpha^{1/(m-1)}} = (m-1)F_\alpha[2(m-1), 2]$$

and from Table IX in [8] it may be corroborated that, for $m \leq 20$, $LC_1(\alpha) = \log(1+D_1(\alpha))$ is approximately given by

$$\log \left[n \sum_{i=2}^m \frac{1}{n-i+1} \frac{\alpha^{1/(m-1)}}{(m-1)(1-\alpha^{1/(m-1)})} + 1 \right] \quad (10)$$

$$\log \left[n \sum_{i=2}^m \frac{1}{n-i+1} F_\alpha [2(m-1), 2] + 1 \right].$$

This result has been demonstrated empirically using the fact that (10) was used as a first approximation in the Newton-Raphson iterative procedure employed to generate $LC_1(\alpha)$ and the amount of deviation from this first guess is shown in the machine computation output to be small. Thus, except for large m , the test Φ_1 rejects $H: b \geq b_0$ approximately when

$$\log Z_m / \left\{ b_0 \log \left[n \sum_{i=2}^m \frac{1}{n-i+1} F_\alpha [2(m-1), 2] + 1 \right] \right\} < 1.$$

COMPARISON OF BOUNDS BASED ON Φ_1 AND Φ_A

Very roughly, with probability $1 - \gamma$ the statistic $\log Z_m$ is greater than $b \log \left[n \sum_{i=2}^m \frac{1}{n-i+1} F[2(m-1), 2] + 1 \right]$ and with probability γ is less than this value, as long as m is not large. Next, the statistic

$$\sum_{i=2}^m (n-i+1) \left(\frac{z_{i-1} - z_{i-1}}{n(m-1)} \right) = \frac{1}{n} \left[\sum_{i=2}^m \left(\frac{z_{i-1}}{m-1} \right) + (n-m+1) \left(\frac{z_{m-1}}{m-1} \right) \right], \quad z_1 = 1,$$

upon which the test Φ_A is based can be considered to be $\frac{n-1}{n} \left(\frac{z_{\mu-1}}{m-1} \right)$ for some μ with $2 \leq j \leq \mu \leq k \leq m$, j, k , and m integers and

$Z_j \leq Z_\mu \leq Z_k$. (When $m = 2$, $\mu = 2$, and Φ_A is equivalent to Φ_1). Then, from (5) H_0 is rejected on the basis of Φ_A when

$$\log Z_\mu / b_n \log \left[\frac{n(m-1)}{n-1} F_\alpha [2(m-1), 2] + 1 \right] < 1,$$

with the γ^{th} percentage point of the distribution of $\log Z_\mu$ equal to

$$b \log \left[\frac{n(m-1)}{n-1} F_\gamma [2(m-1), 2] + 1 \right].$$

For either of the two $(1-\alpha)$ -level confidence bounds based on Φ_1 and Φ_A then, with approximate probability γ for small m , the upper bound \bar{b} is less than

$$\frac{b \log(F_\gamma [2(m-1), 2] x+1)}{\log(F_\alpha [2(m-1), 2] x+1)}, \quad (11)$$

where

$$x = \frac{n}{n-1}(m-1), \quad x = n \sum_{i=2}^m \frac{1}{n-i+1} \geq n \sum_{i=2}^m \frac{1}{n-i} = \frac{n(m-1)}{n-1} > 1.$$

(When $m=2$, the two expressions for x are equal.) At confidence level $1-\alpha$, therefore, the test (Φ_1 or Φ_A) which yields the larger value of (11) for $\gamma < \alpha$ ($1-\gamma > 1-\alpha$) may be considered superior since it is therefore the more accurate bound. Accuracy of the bound is in the sense of the definition of a most accurate bound as found in [2] and on page 5.

If the expression

$$\frac{\log(ax+1)}{\log(cx+1)}, \quad x > 0, \quad 0 < a < c, \quad (12)$$

is differentiated, one obtains

$$\frac{-\log(ax+1) \frac{c}{cx+1} + \log(cx+1) \frac{a}{ax+1}}{\log^2(cx+1)} = \frac{-\frac{ax+1}{ax} \log(ax+1) + \frac{cx+1}{cx} \log(cx+1)}{\frac{cx+1}{c} \cdot \frac{ax+1}{a} \cdot \frac{1}{x} \log^2(cx+1)} \quad (13)$$

Now consider $\frac{y+1}{y} \log(y+1)$ whose derivative is $\frac{1}{y} + \log(1+y)(-\frac{1}{y^2})$.

Since $y > \log(1+y)$, this derivative is always positive and $\frac{y+1}{y} \log(y+1)$ is increasing in y . Therefore, since $a < c$, the right hand term in the numerator of (13) is larger than the left, (13) is always positive, and (12) is increasing in x . Hence the larger the value of x , $\frac{n(m-1)}{n-1}$ or $n \sum_{i=2}^m \frac{1}{n-i+1}$, the more desirable the associated confidence bound.

Then, since $n \sum_{i=2}^m \frac{1}{n-i+1} > \frac{1}{-1}$ for $m > 2$, an upper confidence bound based on $\hat{\epsilon}_1$ is more accurate than one based on $\hat{\epsilon}_A$ for small m .

UNBIASEDNESS OF $\hat{\epsilon}_1$

The test $\hat{\epsilon}_1(z_m)$ can be shown to be unbiased in the following manner.

The power function $\beta_{\hat{\epsilon}_1}(b)$ of $\hat{\epsilon}_1$ can be expressed as a function of $C_1(\alpha)$,

$$\beta_{\hat{\epsilon}_1}(b) = E_b(\hat{\epsilon}_1) = 1 - \frac{n!}{(n-m)!(m-2)!} \sum_{k=0}^{m-2} (-1)^k \binom{m-2}{k} \frac{1}{[(m-k-1)+(n-m+k+1)(C_1(\alpha))^b]^b} \quad (13)$$

¹ The form of the right side of (13) and this step of the proof were suggested by Prof. Wayne F. Smith of the University of California at Los Angeles.

and the derivative $\beta'_{\phi_1}(b)$ thus has the form

$$\beta'_{\phi_1}(b) = \frac{-n!}{(n-m)!(m-2)!} (c_1(\alpha))^{b_0/b} \log(c_1(\alpha))^{b_0} \sum_{k=0}^{m-2} \frac{(-1)^k}{b^2} \binom{m-2}{k} \frac{1}{[(m-k-1)+(n-m+k+1)(c_1(\alpha))^{b_0/b}]^2}. \quad (14)$$

Then from (5) and (7),

$$\beta'_{\phi_1}(b) = -\frac{1}{b^2} (c_1(\alpha))^{b_0/b} \log(c_1(\alpha))^{b_0} \cdot f(v) \Big|_{v=c_1(\alpha)^{b_0/b}} < 0$$

since $c_1(\alpha) > 1$. Hence, $\beta_{\phi_1}(b)$ is monotonically decreasing in b . For ϕ_1 the two criteria for unbiasedness are satisfied, that is

$$\beta_{\phi_1}(b) \leq \alpha \text{ for } b \geq b_0$$

$$\beta_{\phi_1}(b) > \alpha \text{ for } b < b_0.$$

Satisfaction of the first of these criteria insures that the test is of size α or that $\sup \beta_{\phi_1}(b) = \alpha$ for $b \geq b_0$ since $\beta_{\phi_1}(b_0) = \alpha$.

INDUCED TESTS AND CONFIDENCE SETS FOR RELIABILITY AND RELIABLE LIFE

INDUCED TESTS AND CONFIDENCE SETS FOR RELIABILITY BASED ON ALL THE ORDER STATISTICS

Suppose that the matter of concern is the problem of testing that

$R(t_g) = \exp[-(t_g/\delta)^{1/b}]$, the proportion of the population surviving

at a specified time t_g , is less than some given R_o . Let

$\xi = \delta^{1/b} \cdot t_g^{1/b} / \log[1/R(t_g)]$. The distribution of

$$\frac{2m\xi}{\xi} = \frac{2 \left(\sum_{i=1}^{m-1} T_i^{1/b} + (n-m+1)T_m^{1/b} \right)}{\xi}$$

is χ^2_{2m} ; and when b is known (see [10]) a uniformly most powerful α' -level test ξ_2 of H' : $\delta^{1/b} \leq \delta_o^{1/b}$, or equivalently, since $R(t_g) = \exp[-(t_g/\delta_o)^{1/b}]$, H' : $R(t_g) \leq R_o = \exp[-(t_g/\delta_o)^{1/b}]$ versus K : $R(t_g) > R_o$

is: Reject H' when $2m\xi/t_g$ is greater than $\chi^2_{2m}(1-\alpha)/\log 1/R_o$ (accept otherwise). Therefore H' is accepted at level α' if

$$2 \left[\sum_{i=1}^{m-1} \frac{T_i}{t_g}^{1/b} + (n-m+1) \frac{T_m}{t_g}^{1/b} \right] \leq \chi^2_{2m}(1-\alpha')/\log(1/R_o) . \quad (15)$$

The left side of (15) increases monotonically as b decreases if

$$t_g^{1/b} / \left(\frac{T_1}{t_g}^{1/b} + \frac{T_2}{t_g}^{1/b} + \dots + \frac{T_m}{t_g}^{1/b} \right) \geq \frac{(n-m+1)T_m^{1/b}}{\Delta}, \text{ with } \Delta = T_1^{1/b} + T_2^{1/b} + \dots +$$

$(n-m+1)T_m^{1/b}$, and certainly if $t_g \leq (T_1 \cdot T_2 \cdot \dots \cdot T_m)^{1/m}$. Thus for

t_g sufficiently small, if H' is accepted under the assumption that $b = b_o$ when the value of b_o is inserted for b in (15), then it would surely be accepted if b were greater than b_o and the true value of b were somehow to be substituted for the symbol b in (15).

Hence one may form an induced test Φ^* of H^* ($H: b \geq b_0$ is true and H' is true) versus K^* (H^* is not true) which uses the test Φ_2 with $b = b_0$ in (15) to test H' only if the hypothesis H is accepted on the basis of the test Φ_1 . Now, consider

$$m\hat{\xi} = \left[\sum_{i=1}^{m-1} T_i^{1/b} + (n-m+1)T_m^{1/b} \right] = \sum_{i=1}^m (n-i+1) \left(T_i^{1/b} - T_{i-1}^{1/b} \right), \quad (T_0 = 0).$$

The joint density of $w_i = T_i^{1/b}$, $i = 1, 2, \dots, m$, is

$$f(w_1, w_2, \dots, w_m) = \left[\prod_{i=1}^m (n-i+1)/\delta^{1/b} \right] \exp \left\{ -\frac{1}{\delta^{1/b}} [n w_1 + (n-1)(w_2 - w_1) + \dots + (n-m+1)(w_m - w_{m-1})] \right\}, \quad \begin{array}{l} 0 \leq w_1 < \infty, \\ w_1 \leq w_2 < \infty, \\ \vdots \\ w_{m-1} \leq w_m < \infty. \end{array}$$

Thus the joint density of $s_i = (n-i+1)(w_i - w_{i-1}) = (n-i+1)(T_i^{1/b} - T_{i-1}^{1/b})$, $T_0 = 0$, $i = 1, 2, \dots, m$, is

$$f(s_1, s_2, \dots, s_m) = \left(\frac{1}{\delta^{1/b}} \right)^m \exp \left[-\left(\frac{1}{\delta^{1/b}} \sum_{i=1}^m s_i \right) \right], \quad \begin{array}{l} 0 \leq s_1 < \infty, \\ \vdots \\ 0 \leq s_m < \infty. \end{array}$$

and each $s_i = (n-i+1) \left(T_i^{1/b} - T_{i-1}^{1/b} \right)$, $i = 1, 2, \dots, m$, has an independent gamma distribution with scale parameter $\delta^{1/b}$. Therefore, by a result of Lukacs in [9], $m\hat{\xi} = \sum_{i=1}^r (n-i+1)(T_i^{1/b} - T_{i-1}^{1/b})$ is independent of any of $m-1$ linear combinations of

$$1, \frac{(n-1)[T_2^{1/b} - T_1^{1/b}]}{nT_1^{1/b}}, \frac{(n-2)[T_3^{1/b} - T_2^{1/b}]}{nT_1^{1/b}}, \dots \text{ and } \frac{(n-m+1)[T_m^{1/b} - T_{m-1}^{1/b}]}{nT_1^{1/b}}$$

which are equal to

$$1, \frac{n-1}{n} (z_2^{1/b} - 1), \frac{n-2}{n} (z_3^{1/b} - z_2^{1/b}), \dots, \text{ and } \frac{(n-m+1)}{n} (z_m^{1/b} - z_{m-1}^{1/b}).$$

Therefore, $\hat{\psi}_1^*$ is independent of $z_2^{1/b}, z_3^{1/b}, \dots, z_m^{1/b}$ and hence of Z_m . Darroch and Silvey [11] show that when the two tests which form the induced test are similar ($\beta_{\psi_1}(t_0) = \alpha, \beta_{\psi_2}(t_0) = \alpha'$), of size α and α' , respectively, and are based on independent test statistics,¹ then the induced test is similar and of size $1-(1-\alpha)(1-\alpha')$. Since unbiasedness of a test with a continuous power function implies both that the test is similar and that the size is equal to the significance level, these conditions are satisfied for both ψ_1 and ψ_2 (see [10]). Thus ψ^* is similar and of size $1-(1-\alpha)(1-\alpha')$.

Now, just as the tests ψ_1 and ψ_2 have been combined to form the induced test ψ^* , the boundaries of the acceptance regions of the two tests may be combined to form joint confidence bounds for b and $R(t_g)$ at confidence level $(1-\alpha)(1-\alpha')$. This is possible because ψ^* is similar and of size $1-(1-\alpha)(1-\alpha')$. From the acceptance region of the test ψ_2 of $H': R(t_g) \leq R_0$ versus $K': R(t_g) > R_0$, with probability $1-\alpha'$,

¹ The expression $\left[\sum_{i=1}^{m-1} (t_i)^{1/b} + (n-m+1)t_m^{1/b} \right]$ is considered a statistic even though it contains the parameter b since the value of b here is assumed known.

$$R(t_g) \geq \exp \left\{ - \frac{\chi_{2m}^2(1-\alpha')}{2 \left[(T_1/t_g)^{1/b} + (T_2/t_g)^{1/b} + \dots + (n-m+1)(T_m/t_g)^{1/b} \right]} \right\}, \quad (16)$$

where the right side of (16) is monotonically decreasing in b as long as

$$t_g < T_1^{1/b}/\Delta \cdot T_2^{1/b}/\Delta \cdot \dots \cdot T_m^{1/b}/\Delta \quad \text{with}$$

$$\Delta = T_1^{1/b} + T_2^{1/b} + \dots + (n-m+1)T_m^{1/b}, \text{ and certainly if } t_g \leq (T_1 \cdot \dots \cdot T_m)^{1/m}.$$

Thus, if $\bar{b} = \bar{b}_1(\alpha)$ (the boundary of the acceptance region of ξ_1) is equal to $\log Z_m / L_C(\alpha)$,

$$R(t_g) \geq \exp \left\{ - \frac{\chi_{2m}^2(1-\alpha)}{2 \left[(T_1/t_g)^{1/b} + (T_2/t_g)^{1/b} + \dots + (n-m+1)(T_m/t_g)^{1/b} \right]} \right\}$$

(for t_g sufficiently small) is true with probability at least $(1-\alpha)(1-\alpha')$.¹

INDUCED TESTS AND CONFIDENCE SETS BASED ON TWO OR THREE ORDER STATISTICS

Darroch and Silvey [11] show that the two statistics upon which an induced test is based need not be independent. As long as the tests are similar and of size α and α' , then the induced test will be similar and of size α'' with $\max(\alpha, \alpha') \leq \alpha'' \leq \alpha + \alpha'$. Moreover, even though $\hat{\xi}$ gives a uniformly most accurate confidence bound and uniformly most powerful tests for functions of $\xi = \delta^{1/b}$ when b is known, it does not necessarily follow that this situation holds when b is not known. We therefore consider the following one-order-statistic

¹ This inequality containing \bar{b} and the inequality $b \leq \bar{b}$ are jointly true with probability $(1-\alpha)(1-\alpha')$ exactly.

bound for ξ which allows for hand computation of test statistics and bounds for $R(t_g)$ with t_g specified and also for t_R , when alternatively a survival proportion R is specified. When b is known, a test Φ_3 of $H': \xi \leq \xi_0 = \delta_0^{1/b}$ versus $K': \xi > \xi_0$ can be obtained from any one order statistic, say T_v , as shown in [12].¹ If one uses such a test, H' is rejected at level α' when

$$T_v^{1/b} > \xi_0 / B_v(\alpha'),$$

where $B_v(\alpha')$ is equal to $-\frac{1}{\log v_{\alpha'}(n-v+1, v)}$ and $v_{\alpha'}(n-v+1, v)$ is the $100\alpha'$ percent point of the beta distribution with $n-v+1$ and v degrees of freedom (see [13]). Then, since $R(t_g) = \exp[-(t_g/\delta)^{1/b}]$, $t_g > 0$, if t_g is specified, the hypothesis H' can be expressed as

$R(t_g) \leq R_{\delta_0, b}(t_g) = R_0$ and will be rejected when

$$(T_v/t_g)^{1/b} > [B_v(\alpha') \log(1/R_0)]^{-1} \quad (17)$$

Alternatively, if a survival proportion R is specified, H' may be expressed by $t_R \geq t_R^0 = \delta_0 (\log(1/R))^b$ and rejected when

$$(B_v(\alpha') \log(1/R))^b > t_R^0 / T_v. \quad (18)$$

The left side of each of the two inequalities (17) and (18) is monotonically decreasing or increasing in b depending upon whether t_g is less than or greater than T_v or $B_v(\alpha') \log(1/R)$ is less than or greater than 1, respectively. Suppose $t_g < T_v$ or $B_v(\alpha') \log(1/R) < 1$ and H' is accepted

¹ In [12] T_v is actually the order statistic yielding smallest expected squared deviation of the bound, based on the acceptance region of Φ_3 , from ξ .

at significance level α on the basis of Φ_3 and the assumption that b is equal to b_0 . Suppose also that the hypothesis $H: b \geq b_0$ has been accepted at level α on the basis of the test Φ_1 . Then the induced test of H^* (H and H' both true) has size and significance level α'' , and $\max(\alpha, \alpha') \leq \alpha'' < (\alpha + \alpha')$, as long as the test Φ_3 is similar and of size α' . As noted earlier, unbiasedness of a test with continuous power function and significance level α' implies that the test is similar and of size α' . Therefore, it is sufficient to demonstrate that Φ_3 is unbiased in order to guarantee that α'' , the size and the significance level of the induced test have the lower and upper limits $\max(\alpha, \alpha')$ and $\alpha + \alpha'$, respectively. This is shown in the following steps.

First, if T_v is the v^{th} order statistic of a size n sample from a Weibull distribution, then $(T_v)^{1/b}$ is equivalent to the v^{th} order statistic W_v of a size n sample from the negative exponential distribution with scale parameter ξ . Thus, the power function of the test Φ_3 is given by

$$\beta_{\Phi_3}(\xi) = \int_{\xi_0/B_v(\alpha')}^{\infty} \frac{n!}{(v-1)!(n-v)!} e^{-(n-v+1)} \left[\frac{v}{\xi} \right]^{v-1} \left[1 - e^{-\frac{v}{\xi}} \right]^{n-v} dv$$

or

$$\beta_{\Phi_3}(\xi) = \frac{n!}{(v-1)!(n-v)!} \sum_{k=0}^{v-1} (-1)^k \binom{v-1}{k} \frac{e^{-(n-v+k+1)}}{(n-v+k+1)} \xi_0 / \xi B_v(\alpha')$$

Therefore,

$$\begin{aligned}\beta'_{\Phi_3}(\xi) &= \frac{n!}{(v-1)!(n-v)!} \sum_{k=0}^{v-1} (-1)^k \binom{v-1}{k} \left[\xi_0 / \xi^2 B_v(\alpha') \right] e^{-[(n-v+k+1)\xi_0 / \xi B_v(\alpha')]} \\ &= \left[\xi_0 / (\xi B_v(\alpha')) \right] f(w_v) \Big|_{w_v = \xi_0 / \xi B_v(\alpha')}$$

Then, since ξ , ξ_0 , $B_v(\alpha')$, and $f(\xi_0 / \xi B_v(\alpha'))$ are each greater than zero, $\beta'_{\Phi_3}(\xi)$ is positive for all ξ and the power function is monotonically increasing in ξ . (The power function of the dual test Φ_3 of K' versus H' can in like manner be shown to be monotonically decreasing in ξ .) Hence, both tests are unbiased, and the size and significance level of the induced test are equal to α'' .

A confidence bound for $R(t_g)$ or t_R can then be obtained from the boundary of the acceptance region of the test Φ_3 with

$$P\{R(t_g) \geq \exp\left[-(t_g/T_v)^{1/\bar{b}}/B_v(\alpha')\right]\} \geq 1-\alpha'', \quad t_g < T_v \quad (19)$$

or

$$P\{t_R \geq T_v \left[B_v(\alpha') \log(1/R) \right]^{\bar{b}}\} \geq 1-\alpha'', \quad B_v(\alpha') \log(1/R) < 1 \quad (20)$$

and $\bar{b} = \bar{b}_1(\alpha)$ the boundary of the acceptance region of Φ_1 at confidence level $1-\alpha$. Alternatively, then, one may write (19) as

$$P\left\{\log(\log(1/R)(t_g)) \leq LC_1(\alpha) \frac{\log(t_g/T_v)}{\log(T_m/T_1)} - \log B_v(\alpha')\right\} \geq 1-\alpha'',$$

$$t_g < T_v,$$

and (20) as

$$P\left\{\log t_R \geq \log \underline{t}_R = \log T_v + \left[\frac{\log(T_m/T_1)}{LC(\alpha)} \right] \left[\log(\log(1/R)) + \log B_v(\alpha') \right] \right\} \geq 1-\alpha. \quad (21)$$

for $\log(\log(1/R)) + \log B_v(\alpha') < 0$.

IMPROVEMENT OF DERIVED TESTS AND CONFIDENCE SETS

TESTS AND CONFIDENCE SETS CONCERNING b

Now, suppose one is no longer restricted to the use of the order statistics T_1 and T_m for obtaining tests and confidence sets for b , but instead considers any two order statistics as possible candidates upon which to base these tests and confidence sets. Suppose one uses as a criterion in choosing a confidence bound of the form

$(\log T_q - \log T_p)/k_{p,q}$, smallest expected squared deviation of the bound from the parameter b (see Harter [14]). It can easily be shown that there exists a combination of n and m for which the combination of $\log T_1$ and $\log T_m$ does not provide the linear invariant two-order-statistic estimate of b that has smallest mean squared deviation from this parameter. Therefore, for each combination of n , m , and α considered, a coefficient, $LC_{p,q}(\alpha)$, yielding an upper bound $\bar{b}_{p,q}(\alpha) = (\log T_q - \log T_p)/LC_{p,q}(\alpha)$, $1 \leq p < q \leq m$ and the mean squared deviation of $\bar{b}_{p,q}(\alpha)$ from b have been calculated using

results obtained in [8]. The combination of p and q yielding the most efficient bound, that is, the one satisfying the specified criterion, is listed in Table B.I along with values of $LC = LC_{p,q}(\alpha)$ from which the bound may be obtained. Also in preparation is an additional table which will list, for selected values of α , the ratio of the mean squared errors of the best linear invariant estimators of b based on (1) all m available order statistics and (2) the combination of X_p and X_q yielding the most efficient bound.

Consider the power function $\beta_{p,q}(b)$ of the test $\epsilon_{p,q}$ of $H: b \geq b_0$ versus $K: b < b_0$ at significance level α which rejects the hypothesis when

$$(\log T_q - \log T_p)/b_0 \leq LC_{p,q}(\alpha).$$

Proceeding from (3) it can be shown that if $C_{p,q}(\alpha) = \exp(LC_{p,q}(\alpha))$, then $\beta_{p,q}(b)$ has the form

$$\begin{aligned} \beta_{p,q}(b) &= E_b(\epsilon_{p,q}) = 1 - \frac{n!}{(p-1)!(q-p-1)!(n-q)!} \sum_{k=0}^{p-1} \sum_{j=0}^{q-p-1} (-1)^{k+j} \binom{p-1}{k} \binom{q-p-1}{j} \\ &\quad \frac{1/(n-q+j+1)}{((q-p-j+k)+(n-q+j+1)) (C_{p,q}(\alpha))^{b_0/b})} \end{aligned}$$

Thus, as in the case in which $T_p = T_1$, $T_q = T_m$, and $C_{p,q}(\alpha) = C_1(\alpha)$, it follows that

$$\beta'_{p,q}(b) = -\frac{1}{b^2} \left(c_{p,q}(\alpha) \right)^{b_0/b} \log \left(c_{p,q}(\alpha) \right)^{b_0} f(s) \Big|_{s = \left(c_{p,q}(\alpha) \right)^{b_0/b}}$$

Then, as before, $c_{p,q}(\alpha)$ is greater than 1 (since p is less than q), and $\beta'_{p,q}(b)$ is negative. Therefore the power function is monotonically decreasing in b . This insures that the test is unbiased and that an induced test of H^* ($H: b \geq b_0$ is true and $H': \xi \leq \xi_0$ is true) based on $\Phi_{p,q}$ at significance level α and Φ_3 at significance level α' will be similar and of size α'' with $\max(\alpha, \alpha') \leq \alpha'' \leq \alpha + \alpha'$ as when

$\Phi_{p,q} = \Phi_{1,m} = \Phi_1$. The value of the power function $\beta'_{p,q}(b)$ was calculated for b/b_0 equal to 0.25, 0.5 and 0.75 for each combination of p and q corresponding to each combination of n , m , and α so that the relative general sizes of the power functions of the tests for $b < b_0$ (related to the accuracy of the bound) could be compared with the relative sizes of the mean squared deviations of the bounds from the parameter.

It was found that the test based on the combination of p and q providing the most efficient bound for each combination of n , m , and α is not in general uniformly most powerful. That is, it is not always most powerful among tests based on two order statistics for all three of the values of b/b_0 calculated. In each case, however, the test corresponding to the most efficient bound appears to be if not uniformly most powerful, at least either locally most powerful or most powerful for b/b_0 close to zero. Furthermore, whenever a test

associated with a bound which is not the most efficient has higher power than that based on the most efficient combination of X_p and X_q for any value of b/b_0 calculated, the power functions of the two tests differ only slightly and the mean squared deviations of the two bounds are very nearly equal.

For example, the computed values of the power functions, for $\alpha = 0.05$, $n = m = 16$, and b/b_0 equal to 0.25, 0.50, and 0.75, are for the test based on the most efficient combination X_3 and X_{16} equal to 0.999997, 0.890903, and 0.296701, respectively, and for the test based on X_4 and X_{16} equal to 0.999999, 0.882135, and 0.283704, respectively. The expected squared deviations of the two corresponding bounds are 0.4289 and 0.4470, respectively.

TESTS AND CONFIDENCE SETS CONCERNING RELIABLE LIFE

It can also be shown that among lower bounds on x_R at confidence level $\geq 1 - \alpha'' \geq 1 - (\alpha + \alpha')$ of the form

$$\log T_v + \frac{\log \log (1/R) + B_v(\alpha')}{LC_{p,q}(\alpha)} (\log T_q - \log T_p), \quad 1 \leq p < q \leq m, \quad (22)$$

(as defined in (21)), the one with smallest expected squared deviation does not necessarily have $T_q = T_m$ and $T_p = T_1$ and $LC_{p,q}(\alpha) = LC_1(\alpha)$. Furthermore, an additional improvement can be made in the following

manner. Consider the identity,

$$X_v + \frac{\log \log (1/R) - Y_v}{Y_q - Y_p} (X_q - X_p) = u + b \log \log (1/R) = \underline{x}_R , \quad (23)$$

$$1 \leq p < q \leq m,$$

where $Y_k = (X_k - u)/b$ and $X_k = \log T_k$ for any k . Hence, if

$$\frac{\log \log (1/R) - Y_v}{Y_q - Y_p} \geq \underline{v} \text{ with probability exactly equal to } 1 - \alpha^*, \text{ then}$$

$$P \left\{ \underline{x}_R \geq X_v + \underline{v} (X_q - X_p) \right\} = 1 - \alpha^*.$$

Call $\frac{\log \log (1/R) + B_v(\alpha')}{LC_1(\alpha)}$ in (21), \underline{w} , and call the bound defined by

$$(22), \underline{x}_R(\underline{w}). \text{ From (22) and (23)} \frac{\log \log (1/R) - Y_v}{Y_q - Y_p} \geq \underline{w} \text{ with proba-}$$

bility greater than or equal to $1 - (\alpha + \alpha')$. Thus, if $1 - \alpha^*$ is equal to $1 - (\alpha + \alpha')$, \underline{w} is less than or equal to \underline{v} and $X_v + \underline{v} (X_q - X_p)$ is less than or equal to $X_v + \underline{w} (X_q - X_p)$. It follows that for any value $\underline{x}_R' < \underline{x}_R$ the probability that $X_v + \underline{v} (X_q - X_p)$ is less than \underline{x}_R' is smaller than or equal to the probability that $X_v + \underline{w} (X_q - X_p)$ is less than \underline{x}_R' .

The more accurate bound is therefore given by

$$\underline{x}_R(v) = X_v + \underline{v} (X_q - X_p).$$

Moreover, since the test associated with the bound $\underline{x}_R(w)$ is of size $\leq (\alpha + \alpha') = \alpha^*$, the test associated with the bound $\underline{x}_R(v)$ is also of

size $\leq \alpha^*$, hence of size α^* since α^* is the significance level.

Since it is not possible by calculation and examination of the power function to demonstrate that the test associated with the bound $\underline{x}_R(v)$ is unbiased, this is of interest.

It was originally planned that the combination of p , q , and v yielding a most efficient bound for \underline{x}_R would be determined for each combination of n , m , R , and α considered. Doing this, however, would require iterative calculations of 20,615 percentage points of the distribution of V from the expression (or an expression similar to that given) on page 77 for each combination of α and R , if only sample sizes 2, 3, ..., 20 were considered. Since several seconds, at least, appear to be required to perform the numerical integrations involved in calculating each percentage point, it has been decided to cut down on the number of necessary calculations by choosing the three order statistics on which to base the bounds before any values of \underline{v} are computed. For each combination of sample size n , censoring number m , and specified survival proportion R , the estimator of \underline{x}_R with smallest risk among those of the form $X_v + C(X_q - X_p)$, $1 \leq v \leq m$, $1 \leq p < q \leq m$, will be selected. The three order statistics specified by this estimation rule will then provide the basis for bounds at all confidence levels for each corresponding combination of n , m , and R . Indications are that very little increase in risk for the bounds will result from this procedure; and the number of percentage points to be calculated for each combination of α and R will be reduced to 171.

OBTAINING BOUNDS ON RELIABILITY FOR SPECIFIED REQUIRED LIFE

Suppose that required life t_g rather than a survival proportion R is specified. Then it will often be possible to use the values of \underline{Y} which will be tabulated to obtain an upper confidence bound on $R(t_g)$, the proportion surviving at time $t_g = \exp(x_g)$.

The bounds on x_R or t_R , referred to immediately above, depend on the identity

$$x_R = u + b \log \log (1/R) = x_v + \frac{\log \log (1/R) - Y_v}{Y_q - Y_p} (x_q - x_p). \quad (24)$$

This can also be written in the form:

$$\log \log (1/R(t_g)) = \frac{x_v - u}{b} + \frac{x_g - x_v}{x_q - x_p} \frac{x_q - x_p}{b}$$

by subtracting u from both sides of the identity in (24), dividing by b , and replacing R by $R(t_g)$. Let x_g or t_g be specified so that $\frac{x_g - x_v}{x_q - x_p}$ can be calculated. Then a lower confidence bound on $R(t_g)$ is given by the value of R corresponding to the \underline{Y} which is equal to

$\frac{x_g - x_v}{x_q - x_p}$ and which represents a bound at the appropriate level on

$$V = \frac{\log \log (1/R) - Y_v}{Y_q - Y_p} = \frac{x_R - x_v}{x_q - x_p} \text{ when } R \text{ is specified. It will often}$$

be the case, of course, that the required value of \underline{Y} is not available in the table, in which case a larger value can be used to provide a conservative bound on $R(t_g)$.

EXTENSION OF RESULTS

EXTENSION TO OTHER TWO-PARAMETER DISTRIBUTIONS

A natural extension of the results given above is the application of the methods used in obtaining confidence bounds to various other distributions. The fact that bounds based on three order statistics can be found for a percentage point x_R of the distribution of X (the extreme-value distribution of smallest values) depends, as noted above, upon the identity

$$x_v + \frac{y_R - y_v}{y_q - y_p} (x_q - x_p) = x_R = u + b \log \log (1/R), \quad 1 \leq p < q \leq m \leq n \quad (25)$$
$$1 < v < m < n,$$

where $y_k = x_k - u/b$ and $y_R = \log \log (1/R)$, with R a specified proportion of the population to the right of the point x_R . For the extreme-value distribution, R may represent a proportion of the population surviving at time x_R . The value of $y_R = \log \log (1/R)$ has been tabulated in [15] for the extreme value distribution of largest values, but can also be calculated relatively easily. For other distributions, values of y_R can often also be calculated or have been tabulated. For any distribution which can be transformed to one having a location-scale parameter, that is, with density of the form

$$f_{\theta_1, \theta_2}(x) = \frac{1}{\theta_2} g\left(\frac{x-\theta_1}{\theta_2}\right), \text{ for some } g, \text{ the identity (25) holds. Three-}$$

order-statistic bounds can therefore be obtained on x_R for such a distribution if values of y_R are obtainable and if percentiles of $(y_R - Y_{q,p})/(Y_q - Y_p)$ can be calculated. If the first and second moments of the distribution of the order statistics of the distribution are available as well, a most efficient one of these bounds can be found for various combinations of n, m, R and confidence level $1 - \alpha$. This method of obtaining bounds may be useful when samples from distributions for which classical bounds are available have been censored so that classical theory does not apply.

EXTENSION TO THREE-PARAMETER DISTRIBUTIONS

A further extension of the above results is to a random variable $T - \lambda$, with X equal to the natural logarithm of $T - \lambda$, and the distribution of X dependent upon a location-scale parameter $\theta = (\theta_1, \theta_2)$. These include the three-parameter log normal, the three-parameter Pareto and the three-parameter Weibull distributions. The latter distribution is applicable to the situation in which a threshold λ exists such that no failures can occur prior to the time λ . There is a proof given in Kaufman and Lipow [16] concerning confidence bounds on $t_R = \exp(x_R)$, which they have obtained as a function of order statistics T_1 and T_n from any distribution of the type described above. The following is a generalization of that proof.

Consider a specified proportion $R = 1 - F(y_R)$

$= 1 - P\left(\frac{\log(t_R - \lambda) - \theta_1}{\theta_2}\right)$ of a population and a lower confidence bound t_R which can be obtained on a percentage point t_R corresponding to $1 - R$ when λ is zero. Let t_R be of the form $\exp(x_R) = T_v(T_q/T_p)^{v/n}$, $1 \leq p < q \leq n$, $1 \leq v \leq n < n$. Then $t_R(\lambda) = \lambda + (T_v - \lambda)[(T_q - \lambda)/(T_p - \lambda)]^{v/n}$ gives a suitable bound for $t_R(\lambda) = \lambda + \exp(\theta_1 + \theta_2 y_R)$ when λ is known. It will be shown that t_R gives a conservative lower bound for $t_R(\lambda)$ as long as certain conditions are satisfied.

THEOREM I

If

$P\left\{t_R(\lambda) = \lambda + \exp(\theta_1 + \theta_2 y_R) \geq t_R(\lambda) = \lambda + (T_v - \lambda)[(T_q - \lambda)/(T_p - \lambda)]^{v/n}\right\} = 1 - \alpha$,
then $P\left\{t_R(\lambda) \geq t_R = \exp(x_R)\right\} \geq 1 - \alpha$, for y_R
satisfying certain requirements dependent upon the relationship of T_v to T_p and T_q .

It is sufficient to demonstrate that $t_R \leq t_R(\lambda)$ or that $t_R(\lambda)$ is non-decreasing in λ . Consider

$$t_R(\lambda) = \lambda + (T_v - \lambda)[(T_q - \lambda)/(T_p - \lambda)]^{v/n}$$

The derivative of this expression with respect to λ is given by

$$\begin{aligned}
 \frac{d t_R(\lambda)}{d \lambda} &= 1 - v \left[(T_q - \lambda) / (T_p - \lambda)^{V-1} \right] \left[(T_v - \lambda) / (T_p - \lambda) \right] \\
 &\quad - \left[(T_q - \lambda) / (T_p - \lambda) \right]^V + v \left[(T_v - \lambda) / (T_p - \lambda) \right] \left[(T_q - \lambda) / (T_p - \lambda) \right]^V \quad (26) \\
 &= 1 - \left[(T_q - \lambda) / (T_p - \lambda) \right]^V - v \left[(T_v - \lambda) / (T_p - \lambda) \right] \left\{ \left[(T_q - \lambda) / (T_p - \lambda) \right]^{V-1} \right. \\
 &\quad \left. - \left[(T_q - \lambda) / (T_p - \lambda) \right]^V \right\}
 \end{aligned}$$

Now let $\eta = (T_q - \lambda) / (T_p - \lambda)$, which is greater than or equal to 1 since $\lambda \leq T_1 \leq T_p \leq T_q$. Then (26) can be written

$$1 - \frac{v}{\eta} - v \left[(T_v - \lambda) / (T_p - \lambda) \right] \eta^{V-1} (1-\eta)$$

and it is required to demonstrate that this expression is non-negative or that

$$1 \geq \frac{v}{\eta} + v \left[(T_v - \lambda) / (T_p - \lambda) \right] \eta^{V-1} (1-\eta). \quad (27)$$

Assume $T_p \leq T_v \leq T_q$. Then if $v \leq 0$, $v \eta^{V-1} (1-\eta) \geq 0$ and the right side of (27) has its highest (or worst) value when T_v is equal to T_q . T_q is therefore substituted for T_v in (27), which becomes

$$1 \geq \frac{v}{\eta} + v \eta^V (1-\eta) \quad (28)$$

Then for $v \leq 0$ the right side of (28) is equal to 1 and 0, respectively, for η equal to 1 and ∞ , respectively. Furthermore the right side of (28) is monotonically non-increasing in η for $\eta \geq 1$,

if and only if $\underline{Y} \leq -1$ for $\underline{Y} \leq 0$. Thus, the inequality (26) is satisfied, $t_R(\lambda)$ is non-decreasing in λ , and t_R is a conservative lower bound for t_R , for $T_p \leq T_{\underline{Y}} \leq T_q$ as long as a negative \underline{Y} is less than or equal to -1. If \underline{Y} is positive, then T_p gives the worst value for $T_{\underline{Y}}$ and $1 + \frac{\underline{Y}}{\eta} + \underline{Y} \frac{\underline{Y}-1}{\eta} (1-\eta)$ is equal to 1 for $\eta = 1$ and $-\infty$ for $\eta = \infty$ and is monotonically non-increasing in η for $\eta \geq 1$ if and only if $\underline{Y} \geq 1$. For $T_{\underline{Y}} \leq T_p$ and for $T_{\underline{Y}} \geq T_q$ it can be shown by the method used above that t_R is a conservative lower bound for t_R if $\underline{Y} \leq 0$ and if $\underline{Y} \geq 0$, respectively.

CALCULATION OF THE COEFFICIENTS YIELDING THE EXACT BOUNDS AND USE OF THE TABLES

To obtain the coefficient of an exact upper confidence bound for b at level $1 - \alpha$ based on X_q and X_p one may proceed from (3) as in obtaining the power function. The coefficient $LC_{p,q}(\alpha)$ defining the bound is thus given by iteratively solving the equation

$$1 - \frac{n!}{(p-1)!(q-p-1)!(n-q)!} \sum_{k=0}^{p-1} \sum_{j=0}^{q-p-1} (-1)^{k+1} \binom{p-1}{k} \binom{q-p-1}{j} \frac{1/(n-q+j+1)}{((q-p-j+k)+(n-q+j+1)) c_{p,q}(\alpha)} \approx \alpha, \quad (29)$$

where $c_{p,q}(\alpha) = \exp(LC_{p,q}(\alpha))$.

The coefficient defining an exact upper bound for x_R at confidence level $1 - \alpha^*$, as described above, is the $100\alpha^*$ percent point of the

distribution of $V = \frac{\log \log (1/R) - X_v}{X_q - X_p}$. The expression from which

the distribution percentiles of V may be obtained differs accordingly as $v < p$, $v = p$, $p < v < q$, $v = q$, or $v > q$. For example, if $p < v < q$, the solution to

$$\int_1^{\infty} \frac{n!}{(p-1)!(v-p-1)!q(q-v-1)!(n-q)!} \sum_{k=0}^{p-1} \sum_{j=0}^{v-p-1} \sum_{m=0}^{q-v-1} (-1)^{j+k+m} \binom{p-1}{k} \binom{v-p-1}{j} \binom{q-v-1}{m}$$

$$\left\{ -cs \exp \{-c(n-p+k+1)s\}/(n-q+m+1)(n-v+m-j+k+1)s \right.$$

$$+ c s \exp \left\{ -c \left[(q-p-m+k) s + (n-q+m+1) s^{1-1/v} \right] \right\} / (n-q+m+i) \left[(q-v-j+k) s + (n-q+m+1) s^{1-1/v} \right]$$

$$+ c s \exp \left\{ -c \left[(n+v-q-p+j+1)s + (q-v-j+k)s^{1+1/v} \right] \right\} / (q-v-j+k) \left[(q-v-j+k)s^{1+1/v} + (n-q+m+1)s \right]$$

$$- c s \exp \left\{ c(n+v-p+k+1)s \right\} / (q-v-j+k)(n-v+m-j+k+1)s \right\} ds = \alpha,$$

where $c = \log(1/R)$, defines the appropriate $v = \underline{v}$ when \underline{v} is negative or zero. For $0 < \underline{v} < \infty$, the limits of integration for s are 0 to 1, and $1 - \alpha$ rather than α appears on the right side of the equation. The equations to be solved for \underline{v} under other restrictions on v are slightly less complicated.

The values of $LC_{p,q}(a) = LC_1(a)$ for $X_p = X_1$ were calculated iteratively by means of both equation (29) and equation (9) so that any loss of accuracy with increasing number of terms of (29) could be determined. The calculations were made in Fortran IV built-in double precision (16 significant figures), and the values of $\exp[LC_1(a)]$ calculated agreed to at least seven significant figures no matter how large the number of terms involved, through n equal to 20. An additional external check is given by the values of percentiles of

$$\frac{\frac{T_p}{1/b}}{\frac{T_q}{1/b} - \frac{T_p}{1/b}} = \left[\left(\frac{T_q}{T_p} \right)^{1/b} - 1 \right]^{-1} \quad \text{for } 2 \leq n \leq 10, 1 \leq p < q \leq n, \text{ ex-}$$

hibited in Table I of [17]. The values of LC given in Table B.I of this report are thus accurate to within a unit in the final decimal place shown.

Characteristic of the values of ratios of mean squared errors of best linear invariant estimators of b (based on all m order statistics and on the combination of X_p and X_q yielding a most efficient bound) is 0.793 for $n = m = 17$. For the same values of n and m , the corresponding ratio associated with the v , p , and q yielding a best invariant estimator of $x_{.90}$ of the form $X_v + C(X_q - X_p)$ is 0.877. The additional information contained in the v^{th} order statistic appears to contribute considerably to the efficiency of estimators and bounds.

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**TABLE B.I - VALUES OF P, Q, AND LC FOR OBTAINING MOST EFFICIENT EXACT CONFIDENCE
INTERVALS OF THE FORM $(\log T_Q - \log T_P) / LC$, FOR THE WEIBULL SHAPE PARAMETER,
WHICH IS ANY TWO OF THE FIRST N OF N WEIBULL ORDER STATISTICS, $T_1 \leq T_2 \leq \dots \leq T_N$**

N	n	CONFIDENCE LEVEL											
		0.99			0.95			0.90					
P	Q	LC	P	Q	LC	P	Q	LC	P	Q	LC	P	Q
4	2	1	2	0.020	1	2	0.100	1	2	0.201			
5	2	1	2	0.015	1	2	0.076	1	2	0.154			
3	3	1	3	0.213	1	3	0.482	1	3	0.693			
4	4	1	2	0.013	1	2	0.068	1	2	0.138			
3	3	1	3	0.167	1	3	0.387	1	3	0.565			
4	4	1	4	0.481	1	4	0.847	1	4	1.099			
5	2	1	2	0.013	1	2	0.066	1	2	0.130			
3	3	1	3	0.149	1	3	0.348	1	3	0.513			
4	4	1	4	0.392	1	4	J.706	1	4	0.928			
5	5	1	5	0.737	1	5	1.151	1	5	1.419			
6	2	1	2	0.012	1	2	0.061	1	2	0.125			
3	3	1	3	0.139	1	3	0.327	1	3	0.483			
4	4	1	4	0.353	1	4	J.642	1	4	0.851			
5	5	1	5	0.617	1	5	0.983	1	5	1.226			
6	6	1	6	0.964	1	6	1.403	1	6	1.680			
7	2	1	2	0.012	1	2	J.060	1	2	0.122			
3	3	1	3	0.133	1	3	0.314	1	3	0.465			
4	4	1	4	0.330	1	4	J.605	1	4	0.805			
5	5	1	5	0.560	1	5	0.902	1	5	1.133			
6	6	1	6	0.824	1	6	1.219	1	6	1.474			
7	7	1	7	1.164	1	7	1.618	2	7	1.284			
8	2	1	2	0.011	1	2	0.058	1	2	0.120			
3	3	1	3	0.129	1	3	0.304	1	3	0.452			
4	4	1	4	0.315	1	4	0.581	1	4	0.775			
5	5	1	5	0.526	1	5	0.853	1	5	1.076			
6	6	1	6	0.754	1	6	1.127	1	6	1.371			
7	7	1	7	1.010	1	7	1.424	2	7	1.101			
6	8	1	8	1.340	2	8	1.263	2	8	1.479			
9	2	1	2	0.011	1	2	0.056	1	2	0.118			
3	3	1	3	0.125	1	3	0.298	1	3	0.443			
4	4	1	4	0.305	1	4	J.564	1	4	0.754			
5	5	1	5	0.503	1	5	0.820	1	5	1.037			
6	6	1	6	0.710	1	6	1.069	1	6	1.306			
7	7	1	7	0.930	1	7	1.323	2	7	1.008			
8	8	1	8	1.177	2	8	1.091	2	8	1.286			
9	9	2	9	1.067	2	9	1.430	2	9	1.649			
10	2	1	2	0.011	1	2	0.057	1	2	0.116			
3	3	1	3	0.123	1	3	0.292	1	3	0.435			
4	4	1	4	0.297	1	4	0.551	1	4	0.738			
5	5	1	5	0.486	1	5	0.796	1	5	1.009			
6	6	1	6	0.680	1	6	1.029	1	6	1.261			
7	7	1	7	0.876	1	7	1.259	2	7	0.950			
8	8	1	8	1.089	2	8	1.002	2	8	1.186			
9	9	2	9	0.923	2	9	1.250	2	9	1.450			
10	10	2	10	1.209	2	10	1.579	2	10	1.801			
11	2	1	2	0.011	1	2	0.056	1	2	0.115			
3	3	1	3	0.121	1	3	0.288	1	3	0.429			
4	4	1	4	0.291	1	4	0.541	1	4	0.725			
5	5	1	5	0.473	1	5	0.778	1	5	0.988			
6	6	1	6	0.658	1	6	1.000	1	6	1.228			
7	7	1	7	0.843	1	7	1.214	2	7	0.910			
8	8	1	8	1.032	2	8	0.944	2	8	1.122			
9	9	2	9	0.866	2	9	1.154	2	9	1.345			
10	10	2	10	1.057	2	10	1.394	2	10	1.598			
11	11	2	11	1.338	2	11	1.713	2	11	1.936			
12	2	1	2	0.011	1	2	J.056	1	2	0.114			
3	3	1	3	0.120	1	3	0.285	1	3	0.425			
4	4	1	4	0.286	1	4	0.532	1	4	0.715			
5	5	1	5	0.463	1	5	0.763	1	5	0.971			
6	6	1	6	0.641	1	6	0.977	1	6	1.202			
7	7	1	7	0.816	1	7	1.180	2	7	0.880			
8	8	1	8	0.992	2	8	0.904	2	8	1.077			
9	9	2	9	0.796	2	9	1.092	2	9	1.276			
10	10	2	10	0.974	2	10	1.293	2	10	1.488			
11	11	2	11	1.181	2	11	1.524	2	11	1.730			
12	12	2	12	1.457	2	12	1.835	2	12	2.059			

TABLE B.I - CONTINUED

N	M	CONFIDENCE LEVEL											
		0.99				0.95				0.90			
		P	Q	LC	P	Q	LC	P	Q	LC	P	Q	LC
13	2	1	2	0.011	1	2	0.055	1	2	0.114			
	3	1	3	0.118	1	3	0.282	1	3	0.421			
	4	1	4	0.282	1	4	0.526	1	4	0.707			
	5	1	5	0.455	1	5	0.751	1	5	0.957			
	6	1	6	0.627	1	6	0.959	1	6	1.182			
	7	1	7	0.795	1	7	1.154	2	7	0.857			
	8	1	8	0.961	2	8	0.874	2	8	1.043			
	9	2	9	0.760	2	9	1.047	2	9	1.227			
	10	2	10	0.919	2	10	1.227	2	10	1.416			
	11	2	11	1.093	2	11	1.420	2	11	1.618			
	12	2	12	1.295	2	12	1.643	3	12	1.491			
	13	2	13	1.566	2	13	1.947	2	13	1.801			
14	2	1	2	0.011	1	2	0.055	1	2	0.113			
	3	1	3	0.117	1	3	0.280	1	3	0.418			
	4	1	4	0.279	1	4	0.520	1	4	0.700			
	5	1	5	0.449	1	5	0.742	1	5	0.946			
	6	1	6	0.616	1	6	0.944	1	6	1.165			
	7	1	7	0.778	1	7	1.133	2	7	0.839			
	8	1	8	0.937	2	8	0.850	2	8	1.017			
	9	2	9	0.733	2	9	1.014	2	9	1.190			
	10	2	10	0.880	2	10	1.179	2	10	1.363			
	11	2	11	1.034	2	11	1.350	2	11	1.543			
	12	2	12	1.203	2	12	1.536	3	12	1.384			
	13	2	13	1.401	3	13	1.427	3	13	1.605			
	14	2	14	1.667	3	14	1.713	3	14	1.907			
15	2	1	2	0.011	1	2	0.055	1	2	0.112			
	3	1	3	0.116	1	3	0.278	1	3	0.415			
	4	1	4	0.276	1	4	0.516	1	4	0.694			
	5	1	5	0.443	1	5	0.734	1	5	0.937			
	6	1	6	0.607	1	6	0.932	1	6	1.151			
	7	1	7	0.765	1	7	1.116	2	7	0.824			
	8	1	8	0.918	2	8	0.831	2	8	0.995			
	9	2	9	0.712	2	9	0.987	2	9	1.161			
	10	2	10	0.849	2	10	1.142	2	10	1.323			
	11	2	11	0.991	2	11	1.300	2	11	1.488			
	12	2	12	1.142	2	12	1.464	3	12	1.313			
	13	2	13	1.306	3	13	1.326	3	13	1.495			
	14	2	14	1.499	3	14	1.530	3	14	1.709			
	15	3	15	1.476	3	15	1.811	3	15	2.005			
16	2	1	2	0.011	1	2	0.055	1	2	0.112			
	3	1	3	0.116	1	3	0.276	1	3	0.413			
	4	1	4	0.273	1	4	0.512	1	4	0.689			
	5	1	5	0.439	1	5	0.727	1	5	0.929			
	6	1	6	0.599	1	6	0.922	1	6	1.139			
	7	1	7	0.753	1	7	1.101	2	7	0.812			
	8	1	8	0.902	2	8	0.816	2	8	0.978			
	9	2	9	0.695	2	9	0.966	2	9	1.137			
	10	2	10	0.825	2	10	1.113	2	10	1.292			
	11	2	11	0.959	2	11	1.260	2	11	1.446			
	12	2	12	1.096	2	12	1.411	3	12	1.261			
	13	2	13	1.242	3	13	1.258	3	13	1.421			
	14	2	14	1.403	3	14	1.427	3	14	1.598			
	15	3	15	1.319	3	15	1.425	3	15	1.806			
	16	3	16	1.565	3	16	1.901	3	16	2.097			
17	2	1	2	0.011	1	2	0.054	1	2	0.112			
	3	1	3	0.115	1	3	0.275	1	3	0.411			
	4	1	4	0.271	1	4	0.508	1	4	0.685			
	5	1	5	0.435	1	5	0.721	1	5	0.922			
	6	1	6	0.593	1	6	0.913	1	6	1.129			
	7	1	7	0.744	1	7	1.089	2	7	0.801			
	8	1	8	0.888	2	8	0.803	2	8	0.963			
	9	2	9	0.680	2	9	0.948	2	9	1.117			
	10	2	10	0.806	2	10	1.089	2	10	1.266			
	11	2	11	0.932	2	11	1.229	2	11	1.412			
	12	2	12	1.061	2	12	1.370	3	12	1.221			
	13	2	13	1.194	3	13	1.207	3	13	1.367			
	14	2	14	1.336	3	14	1.356	3	14	1.522			
	15	3	15	1.228	3	15	1.521	3	15	1.693			
	16	3	16	1.406	3	16	1.716	3	16	1.897			
	17	3	17	1.649	3	17	1.986	3	17	2.182			

TABLE B.I - CONTINUED

N	M	CONFIDENCE LEVEL											
		0.99			0.95			0.90					
P	Q	LC	P	Q	LC	P	Q	LC	P	Q	LC	P	Q
18	2	1	2	0.011	1	2	0.054	1	2	0.111			
	3	1	3	0.114	1	3	0.273	1	3	0.409			
	4	1	4	0.270	1	4	0.505	1	4	0.681			
	5	1	5	0.431	1	5	0.716	1	5	0.916			
	6	1	6	0.587	1	6	0.905	1	6	1.121			
	7	1	7	0.735	1	7	1.078	2	7	0.792			
	8	1	8	0.877	2	8	0.792	2	8	0.951			
	9	2	9	0.669	2	9	0.933	2	9	1.101			
	10	2	10	0.790	2	10	1.070	2	10	1.244			
	11	2	11	0.911	2	11	1.204	2	11	1.384			
	12	2	12	1.033	2	12	1.337	3	12	1.189			
	13	2	13	1.157	3	13	1.168	3	13	1.325			
	14	2	14	1.286	3	14	1.304	3	14	1.466			
	15	3	15	1.165	3	15	1.448	3	15	1.616			
	16	3	16	1.313	3	16	1.609	3	16	1.783			
	17	3	17	1.488	3	17	1.800	3	17	1.981			
	18	3	18	1.727	3	18	2.066	3	18	2.261			
19	2	1	2	0.011	1	2	0.054	1	2	0.111			
	3	1	3	0.114	1	3	0.272	1	3	0.407			
	4	1	4	0.268	1	4	0.503	1	4	0.678			
	5	1	5	0.428	1	5	0.711	1	5	0.910			
	6	1	6	0.582	1	6	0.899	1	6	1.113			
	7	1	7	0.728	1	7	1.069	2	7	0.784			
	8	1	8	0.867	2	8	0.782	2	8	0.940			
	9	2	9	0.658	2	9	0.920	2	9	1.086			
	10	2	10	0.776	2	10	1.053	2	10	1.226			
	11	2	11	0.893	2	11	1.182	2	11	1.361			
	12	2	12	1.009	2	12	1.310	3	12	1.162			
	13	2	13	1.127	3	13	1.137	3	13	1.291			
	14	2	14	1.247	3	14	1.263	3	14	1.423			
	15	3	15	1.118	3	15	1.394	3	15	1.559			
	16	3	16	1.248	3	16	1.535	3	16	1.704			
	17	3	17	1.393	3	17	1.691	4	17	1.608			
	18	3	18	1.565	3	18	1.878	4	18	1.799			
	19	3	19	1.802	3	19	2.141	4	19	2.069			
20	2	1	2	0.011	1	2	0.054	1	2	0.111			
	3	1	3	0.113	1	3	0.271	1	3	0.406			
	4	1	4	0.267	1	4	0.500	1	4	0.675			
	5	1	5	0.425	1	5	0.707	1	5	0.905			
	6	1	6	0.578	1	6	0.893	1	6	1.106			
	7	1	7	0.722	1	7	1.061	2	7	0.777			
	8	1	8	0.858	2	8	0.774	2	8	0.931			
	9	2	9	0.650	2	9	0.909	2	9	1.074			
	10	2	10	0.765	2	10	1.039	2	10	1.211			
	11	2	11	0.878	2	11	1.164	2	11	1.342			
	12	2	12	0.990	2	12	1.287	3	12	1.140			
	13	2	13	1.102	3	13	1.111	3	13	1.264			
	14	2	14	1.216	3	14	1.230	3	14	1.387			
	15	3	15	1.081	3	15	1.352	3	15	1.514			
	16	3	16	1.199	3	16	1.480	3	16	1.646			
	17	3	17	1.327	3	17	1.616	4	17	1.532			
	18	3	18	1.469	4	18	1.532	4	18	1.688			
	19	3	19	1.638	4	19	1.712	4	19	1.875			
	20	3	20	1.872	4	20	1.964	4	20	2.141			

TABLE B.I - CONTINUED

N	M	CONFIDENCE LEVEL								
		0.99		0.95		0.90				
P	Q	LC	P	Q	LC	P	Q	LC		
41	2	1	2	0.011	1	2	0.054	1	2	0.114
	3	1	3	0.113	1	3	0.270	1	3	0.404
	4	1	4	0.265	1	4	0.498	1	4	0.672
	5	1	5	0.423	1	5	0.704	1	5	0.901
	6	1	6	0.574	1	6	0.887	1	6	1.100
	7	1	7	0.716	1	7	1.053	2	7	0.771
	8	1	8	0.851	2	8	0.767	2	8	0.922
	9	2	9	0.642	2	9	0.899	2	9	1.063
	10	2	10	0.754	2	10	1.025	2	10	1.197
	11	2	11	0.863	2	11	1.148	2	11	1.325
	12	2	12	0.973	2	12	1.267	3	12	1.122
	13	2	13	1.081	3	13	1.090	3	13	1.240
	14	2	14	1.190	2	14	1.203	3	14	1.358
	15	3	15	1.051	3	15	1.318	3	15	1.477
	16	3	16	1.161	3	16	1.436	3	16	1.599
	17	3	17	1.277	3	17	1.560	4	17	1.475
	18	3	18	1.401	4	18	1.459	4	18	1.611
	19	3	19	1.541	4	19	1.606	4	19	1.763
	20	3	20	1.709	4	20	1.783	4	20	1.947
	21	3	21	1.939	4	21	2.032	4	21	2.210
42	2	1	2	0.011	1	2	0.054	1	2	0.110
	3	1	3	0.113	1	3	0.269	1	3	0.463
	4	1	4	0.264	1	4	0.496	1	4	0.670
	5	1	5	0.421	1	5	0.700	1	5	0.897
	6	1	6	0.570	1	6	0.883	1	6	1.095
	7	1	7	0.711	1	7	1.047	2	7	0.766
	8	1	8	0.844	2	8	0.760	2	8	0.915
	9	2	9	0.635	2	9	0.891	2	9	1.034
	10	2	10	0.746	2	10	1.015	2	10	1.185
	11	2	11	0.853	2	11	1.135	2	11	1.310
	12	2	12	0.959	2	12	1.251	3	12	1.106
	13	2	13	1.063	3	13	1.071	3	13	1.220
	14	2	14	1.168	3	14	1.180	3	14	1.333
	15	3	15	1.027	3	15	1.289	3	15	1.447
	16	3	16	1.130	3	16	1.401	3	16	1.562
	17	3	17	1.237	3	17	1.515	4	17	1.430
	18	3	18	1.350	4	18	1.405	4	18	1.553
	19	3	19	1.472	4	19	1.533	4	19	1.655
	20	4	20	1.405	4	20	1.677	4	20	1.835
	21	4	21	1.565	4	21	1.851	4	21	2.016
	22	4	22	1.787	4	22	2.097	4	22	2.274

APPENDIX C

TABLES FOR OBTAINING THE BEST LINEAR INVARIANT ESTIMATES OF PARAMETERS OF THE WEIBULL DISTRIBUTION

SUMMARY

A censored life-test situation is considered and the assumption of a Weibull distribution for failure times is made. Tables are given for estimating log reliable life, where the estimator is best among linear estimators with expected loss invariant under translations. These best linear invariant (BLI) estimators have uniformly smaller expected loss than the Gauss-Markov best linear unbiased (BLU) estimators and are simple linear functions of the BLU estimators. The preliminary discussion involves a comparison of the BLI estimators with other widely used estimators. Solutions to the problem of obtaining confidence bounds are also discussed.

INTRODUCTION

Assume a random sample of n items is subjected to life test until $m \leq n$ failures occur. Assume further that the failure times associated with the n items are from a population of random variables identically distributed according to a two-parameter Weibull law.

Let the random variable T represent failure time in this population.

Then

$$\Pr[T \leq t] = F_{\delta, b}(t) = 1 - \exp\{-(t/\delta)^{1/b}\} ,$$

for $t \geq 0$, and $F_{\delta, b}(t) = 0$ otherwise. Both parameters δ and b are positive. The logarithms of the failure times have the extreme-value distribution of smallest values. If $X = \log T$ and $u = \log \delta$, then

$$\Pr[X \leq x] = F_{u, b}(x) = 1 - \exp\{-\exp[(x-u)/b]\} .$$

The parameter b is the scale parameter of the distribution of X ; the variance of X is $\frac{\pi^2 b^2}{6}$. The parameter u is a location parameter, the mode of the probability density function associated with the distribution of X .

The reliability function, which gives the proportion of the population surviving at log time x , is given by $R(x) = 1 - F(x)$, or

$$R_{u, b}(x) = \exp\{-\exp[(x-u)/b]\} . \quad (1)$$

Suppose that a value R is specified for $R_{u,b}(x)$ and that the problem of interest is the estimation of the value of x , call it x_R , corresponding to the specified R on the basis of a censored sample. The value x_R is simply the log time at which 100% of the population will have survived, and is often referred to as log reliable life. Since, from (1), $R = \exp\{-\exp[(x_R - u)/b]\}$, or $x_R = u + b \log \log(1/R)$, x_R is a parametric function of the location parameter u and the scale parameter b . In this report methods for estimating the general parametric function $\varphi = \ell_1 u + \ell_2 b$ (which includes u , b , and x_R) are considered.

MAXIMUM-LIKELIHOOD ESTIMATION

Because of the regularity properties of the Weibull density function (see Kimball [1]), maximum-likelihood estimators of Weibull parameters enjoy the properties of consistency, asymptotic efficiency, asymptotic unbiasedness and asymptotic normality. The maximum-likelihood estimates cannot, however, be calculated explicitly, but must be determined by iterative procedures applied to sample data. Since this is so, the expected squared error of a Weibull maximum-likelihood estimator cannot be determined except for large samples, for which the variances of these asymptotically unbiased estimators are given by the Cramer-Rao bounds for regular unbiased estimators. Thus, for small sample sizes, the expected loss of the estimator cannot be compared with that of other estimators whose exact mean squared error can be calculated. Furthermore, in [2] it is shown that when no censoring occurs, the n order statistics, $\{\log T_{(1,n)} \leq \log T_{(2,n)} \leq \dots \leq \log T_{(n,n)}\} = \{X_{(1,n)} \leq X_{(2,n)} \leq \dots \leq X_{(n,n)}\}$ from a size n sample are minimally sufficient for (u,b) . They are, therefore, minimally sufficient for (δ,b) or for any couple consisting of nonsingular functions of δ and b . In [3] this result is extended to show that in the case in which $\frac{n-m}{n}$ of a size n ordered sample is censored from above, the first m order statistics, $X_{(1,n)} \leq X_{(2,n)} \leq \dots \leq X_{(m,n)}$ are minimally sufficient so that for $m > 2$, the number of minimally sufficient statistics

exceeds the number of parameters to be estimated. Hence, there is no guarantee that when m is greater than 2 the maximum-likelihood estimators of Weibull parameters are the minimum-variance estimators of their expected values, as would be the case if the number of sufficient statistics equaled the number of parameters to be estimated (see Rao [4]). One cannot, therefore, claim the usual optimality properties for the maximum-likelihood estimators of the Weibull (or extreme-value) parameters when m is greater than two, but n is not large enough for asymptotic theory to apply. Moreover, it is not known when, for a given $p = m/n, n$ is sufficiently large.

LINEAR ESTIMATION

For estimating the general parametric function $\varphi = \ell_1 u + \ell_2 b$, the generalized Gauss-Markov Theorem (see Lloyd [5]) specifies the least-squares estimator as the unique best one among unbiased linear functions of $X_{(1,n)}, X_{(2,n)}, \dots$, and $X_{(m,n)}$ for all m and n . Weibull estimates obtained graphically from probability plots are simply approximations to the least-squares estimate, with the major source of error being the necessarily subjective visual fitting of the least-squares line. Let $\varphi^* = \ell_1 u^* + \ell_2 b^*$ be the true least-squares or best linear unbiased (BLU) estimator of φ based on the first m of n ordered sample observations, with u^* and b^* the BLU estimators of u and b , respectively. These estimators (u^* , b^* , and φ^*) enjoy all the large sample properties attributed to maximum-likelihood estimators, including that of asymptotic normality (see Blom [6]).

By analogy with other distributions such as the normal, one might expect u , being a location parameter, to be estimated most efficiently by a linear function of the sufficient statistics, $X_{(1,n)}, X_{(2,n)}, \dots, X_{(m,n)}$. For a scale parameter such as b , however, one might conjecture that considerably more efficient estimation could be achieved by some other means. That such a conjecture may well be unjustified is demonstrated by Table A-8B(6) in Dixon and Massey [7]. This table demonstrates the

extremely high efficiency of the best linear unbiased estimator of the Gaussian scale parameter σ with respect to the uniformly minimum variance unbiased estimator which is nonlinear. The efficiency is 100% $= m = 2$, is at its lowest (98.8%) for $n = m = 6$, and increases n for $n > 6$. This fact, along with results given in [8], supports author's conjecture that the best linear unbiased estimator of b has very high efficiency with respect to any unbiased estimator of b which is obtainable. The least-squares estimator φ^* of φ also has an advantage in that the estimate can be calculated directly as a linear function $\sum_{i=1}^m w_i X_{(i,n)}$ of weights $\{w_i\} = \ell_1\{a_i\} + \ell_2\{c_i\}$, $i=1,2,\dots,m$, which can be determined from the first moments and second-moment matrix of the reduced order statistics, $Y_1, Y_2, \dots, Y_m = (X_{(1,n)} - u)/b, (X_{(2,n)} - u)/b, \dots, (X_{(m,n)} - u)/b$ for any given m and n . The weights $\{a_i\}$ and $\{c_i\}$ allow for calculation of the BLU estimates of u and b respectively. The first- and second-moment matrices of the reduced order statistics and the weights for obtaining the estimates were determined in [3] for $2 \leq n \leq 25$, $2 \leq m \leq n$. The variances σb^2 and φb^2 of u^* and b^* , respectively, and σb^2 , the covariance of these estimators, were also calculated for the same values of m and n . In [9], it is shown that for the class of linear estimators of φ based on the first m of n extreme-value order statistics and with expected squared-error loss independent of u , there is a unique best

one given by $\tilde{\varphi} = \ell_1(u^* - [\beta/(1+\gamma)]b^* + [\ell_2/(1+\gamma)]b^*) \equiv \ell_1\tilde{u} + \ell_2\tilde{b}$, and with expected squared error equal to

$$\begin{aligned} & [\ell_1^2 E(LU) + 2\ell_1\ell_2 E(CP) + \ell_2^2 E(LB)]b^2 = \\ & \{ \ell_1^2 \alpha + 2\ell_1\ell_2 \beta + \ell_2^2 \gamma - [(\ell_1\beta + \ell_2\gamma)^2/(1+\gamma)] \} b^2, \end{aligned} \quad (2)$$

for all m and n . Let loss be defined as squared error divided by b^2 . Then $\tilde{\varphi}$ is the best among linear estimators of φ invariant under location and scalar transformations (the best linear invariant estimator) and has been shown in [10] to be the unique admissible mini-max linear estimator of φ based on $X_{(1,n)}, X_{(2,n)}, \dots, X_{(m,n)}$ for all m and n . It also has all the asymptotic properties of the BLU estimator plus that of asymptotic unbiasedness. Therefore, for the values of m and n for which tables of weights for obtaining the estimates based on the estimation rules u^* and b^* and tables of the covariance matrices of these estimators are available, weights

$\{W_i\} = \ell_1\{A_i\} + \ell_2\{C_i\}$ for obtaining the BLI estimator $\tilde{\varphi}$ of φ , hence of u , b , or $x_R = u + b \log \log(1/R)$, are easily obtainable. The expected error for \tilde{u} , \tilde{b} , or \tilde{x}_R (the BLI estimator of x_R) can also be calculated from (2). The weights, $\{A_i\} = \{a_i - [\beta/(1+\gamma)]c_i\}$ and $\{C_i\} = \{c_i/(1+\gamma)\}$, functions of m and n , have been calculated and are given in Table C.I for $2 \leq n \leq 25$, $2 \leq m \leq n$. Values of $E(LU)$ and $E(LB)$, the expected losses of u and b , respectively, and

$E(CP) \equiv E(\tilde{ub} - ub)/b^2$ were also calculated and appear in Table C.I. The indices n , m , and i all appear in Table C.I as capital letters since no lower-case letters are available for the computer output. The method of utilizing the weights for estimating the parameters is illustrated in Figure 1. In this example, the ordering of the failure times and the calculation of the estimates has been achieved via a computer program which uses tapes upon which both the BLU and BLI weights are stored. It is evident, however, that a hand calculation of the estimates can be made with little difficulty.

EXAMPLE SHOWING METHOD OF COMPUTING PARAMETER ESTIMATES FROM FAILURE-TIME DATA

FAILURE TIMES				WEIGHTS		
n = 24	x = 24					
RANDOMIZED ORDER	ASCENDING ORDER	NATURAL LOGARITHMS		A ₁		C ₁
119.0000	6.0000	1.7917595		0.0112481		-0.0244931
138.0000	8.6000	2.1517622		0.0137390		-0.0298709
146.0000	17.8000	2.8791985		0.0160213		-0.0309171
151.0000	18.0000	2.8903718		0.0182155		-0.0314605
27.5000	27.5000	3.3141860		0.0203699		-0.0316140
69.3000	33.5000	3.5115454		0.0225141		-0.0314243
150.0000	50.5000	3.9219733		0.0246466		-0.0309363
8.6000	51.5000	3.9415818		0.0268383		-0.0300915
51.5000	69.0000	4.2341065		0.0290150		-0.0289885
89.0000	74.0000	4.3040651		0.0313289		-0.0274772
109.0000	74.0000	4.3040651		0.0335892		-0.0256841
6.0000	89.0000	4.4886364		0.0359094		-0.0234404
74.0000	109.0000	4.6913479		0.0385429		-0.0207397
118.0000	118.0000	4.7706847		0.0411308		-0.0175568
141.0000	119.0000	4.7791235		0.0439276		-0.0137101
18.0000	138.0000	4.9272537		0.0468615		-0.0091529
33.5000	141.0000	4.9487599		0.0500545		-0.0036386
144.0000	144.0000	4.9698133		0.0535307		0.0030549
17.8000	146.0000	4.9836066		0.0573800		0.0113897
153.0000	150.0000	5.0106353		0.0617825		0.0219454
153.1000	151.0000	5.0172799		0.0669268		0.0360073
153.2000	155.0000	5.0304379		0.0733312		0.0559322
50.5000	153.1000	5.0310913		0.0821530		0.0882378
74.0000	153.2000	5.0317443		0.1008632		0.1981225
				$\bar{u} = 4.61398$		$\bar{b} = 0.56889$
SUMMARY						
	$\bar{u} = 4.61398$				$\bar{b} = 0.56889$	
loglog(1/.90) ≈ -2.25037		loglog(1/.95) ≈ -2.97020				
$\bar{x}_{.90} = \bar{u} + \bar{b} \loglog(1/.90) = 3.33376$		$\bar{T}_{.90} = 28.04366$				
$\bar{x}_{.95} = \bar{u} + \bar{b} \loglog(1/.95) = 2.92426$		$\bar{T}_{.95} = 18.62038$				
		$\bar{T}_R = \exp(\bar{x}_R)$				

Figure 1

ACCURACY OF THE TABLES

The calculation of the moments of the order statistics, the original BLU weights $\{a_i\}$ and $\{c_i\}$, and the estimator covariance matrices were all based on derivations and results of Lieblein in [11] and [12]. All of the computer programs involved in making these calculations incorporated Rocketdyne's N-precision (somewhat more accurate than double precision) subroutines. Three constants, $\pi^2/6$, $\pi^2/12$, and Euler's constant, correct to 22 significant figures, were read in. All other preliminary values used in the computations were generated by using N-precision floating-point arithmetic. Differencing of the tabled values indicated that the numbers given were accurate to within a unit in the eighth decimal place. It should be noted, too, that the weights and the covariance matrices agreed precisely with those given by White for $2 \leq n \leq 20$ in [13] for the number of significant figures listed by him. In our computations the variances and covariances of the estimators were given by the values of the Lagrange multipliers specifying the constraints of invariance and unbiasedness for u^* and b^* as indicated in [9], and thus did not require a separate calculation. The BLI weights with the expected losses were obtained directly from the BLU weights and the variances and covariances of u^* and b^* . Six decimal places only are given for the weights. The eight decimal places included for the expected losses imply additional accuracy for the weights.

ESTIMATION PROCEDURE FOR SAMPLES LARGER THAN 25

If n is greater than 25, the weights in Table C.I or the computer routine using these weights cannot be used directly. Estimates may be obtained, however, by randomly dividing the sample into an arbitrary number of sub-samples each of which has sample size less than 25. An estimate of b , u , or x_R is then obtained as an average of the best linear unbiased sub-estimates where each is weighted by the reciprocal of the variance of the sub-estimator. An approximation to the best linear invariant estimate of each parameter can then be obtained from this average which is an unbiased linear estimate. If the total sample is divided into a set of k uncensored sub-samples of equal size, the Cramér-Rao efficiency of the estimate obtained by averaging is a function of the size n_j of the sub-sample only, increasing with increasing n_j (see Lieblein [12]). For more irregular partitionings of the sample, the determination of efficiency becomes more complex. For a fixed number k of sub-samples, however, the manner in which the sample is divided (e.g., two equal sub-samples or one large and one small) has little effect on efficiency. In any case, when the total sample is greater than 25, it can be seen from [8] that the Cramér-Rao efficiency of the estimate of reliable λ will not usually fall below 87% even for R close to 1 unless there is a great deal of censoring.

Obtaining the proper unbiased estimate of $\ell_1 u + \ell_2 b$ (for each sub-sample) from which a weighted average may be obtained involves converting the estimates obtained from \tilde{u} and \tilde{b} to unbiased estimates. To accomplish this, we note that since

$$\tilde{\varphi} = \ell_1 \tilde{u} + \ell_2 \tilde{b} = \ell_1 [u^* - (\beta/(1+\gamma))b^*] + [\ell_2/(1+\gamma)]b^*, \text{ for all } \ell_1 \text{ and } \ell_2, \text{ then } b^* = (1+\gamma)\tilde{b} \text{ and } u^* = \tilde{u} + (\beta/(1+\gamma))b^* = \tilde{u} + E(CP)b^*.$$

Furthermore, since $E(LB) = \gamma/(1+\gamma)$ and $E(CP) = \beta/(1+\gamma)$, $\gamma = E(LB)/[1-E(LB)]$, $b^* = \tilde{b}/[1-E(LB)]$, and $\beta = E(CP)/[1-E(LB)]$. Thus $u^* = \tilde{u} + [E(CP)/[1-E(LB)]]\tilde{b}$. The variance σ of u^* is $[E(LU) + \beta^2/(1+\gamma)]b^2 = [E(LU) + [E(CP)]^2/[1-E(LB)]]b^2$. We let k be the total number of sub-samples and we let Q_j be equal to $\ell_1^2 \alpha_j + 2\ell_1 \ell_2 \beta_j + \ell_2^2 \gamma_j, j = 1, 2, \dots, k$.

Then the variance of the unbiased estimator formed by the weighted

$$\text{average, } \tilde{\varphi} = \frac{1}{\sum_{j=1}^k (1/Q_j)} \sum_{j=1}^k (1/Q_j)(\ell_1 u_j^* + \ell_2 b_j^*) \text{ is}$$

$$\frac{b^2}{\left[\sum_{j=1}^k (1/Q_j) \right]^2} \sum_{j=1}^k (1/Q_j)^2 (\ell_1^2 \alpha_j + 2\ell_1 \ell_2 \beta_j + \ell_2^2 \gamma_j) = \frac{b^2}{\sum_{j=1}^k (1/Q_j)^2}, \text{ where}$$

the subscript j indicates with which of the sub-samples a quantity is associated. It is simple to demonstrate that $\tilde{\varphi}$ has the minimum variance among unbiased estimators based on the sub-estimators based on the given sub-samples.

The estimator $\hat{\varphi} = \bar{\varphi} - \bar{b} \bar{b}/(1 + \sum_{j=1}^k (1/\gamma_j))$ (where $\bar{b} = \frac{1}{k} \sum_{j=1}^k (1/\gamma_j) b_j^*$)

is the minimum-variance unbiased estimator of b based on the given sub-

estimators $\bar{b} = \frac{1}{\sum_{j=1}^k (1/Q_j) \sum_{j=1}^k (1/\gamma_j)} \sum_{j=1}^k (1/Q_j)(1/\gamma_j)(L_1 b_j + L_2 \gamma_j)$ is the

covariance between $\hat{\varphi}$ and \bar{b}) is the invariant linear function of φ and b with smallest expected squared deviation from φ . It can be shown, by using methods very similar to those used in [8] to derive the form of the Cramér-Rao bound for invariant estimators of location parameters, that $\hat{\varphi}$ is the best linear invariant estimator of φ based on the given sub-estimators.

An alternative method of handling samples larger than 25 has been derived by McCool and is explained in [14]. For large m , however, this method requires considerable additional computation until such time as additional tables combining McCool's results with those in Table C.I are made available. Another approach is described by Johns and Lieberman in [15]. The estimates which can be obtained from tables of weights given by Johns and Lieberman are good approximations to the best linear invariant estimates of u and b . These weights are given for n equal to 10, 15, 20, 30, 50, and 100 and four values of m for each n .

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TABLE C.I
WEIGHTS FOR OBTAINING BEST LINEAR INVARIANT ESTIMATES
OF PARAMETERS OF THE EXTREME-VALUE DISTRIBUTION

$A(N,M,I)$ = WEIGHT FOR ESTIMATING μ
 $C(N,M,I)$ = WEIGHT FOR ESTIMATING σ
 $E(LU)$ = EXPECTED LOSS FOR ESTIMATE OF μ
 $E(CP)$ = EXPECTED CROSS PRODUCT
 $E(LB)$ = EXPECTED LOSS FOR ESTIMATE OF σ

N	M	I	$A(N,M,I)$	$C(N,M,I)$	N	M	I	$A(N,M,I)$	$C(N,M,I)$	
2	2	1	0.110731	-0.421383	5	2	1	-0.481434	-0.472962	
		2	0.889269	0.421383			2	1.481434	0.472962	
$E(LU)$			0.65712995		$E(LU)$			1.24921018		
$E(CP)$			0.03757418		$E(CP)$			0.53379141		
$E(LB)$			0.41583918		$E(LB)$			0.47230837		
3	2	1	-0.166001	-0.452110	5	3	1	-0.137958	-0.306562	
		2	1.166001	0.452110			2	-0.025510	-0.257087	
$E(LU)$			0.79546061				3	1.163468	0.563650	
$E(CP)$			0.25750956		$E(LU)$			0.49029288		
$E(LB)$			0.45003549		$E(CP)$			0.16612899		
3	3	1	0.081063	-0.278666			$E(LB)$	0.29419197		
		2	0.251001	-0.190239	5	4	1	-0.006983	-0.217766	
		3	0.667936	0.468904			2	0.059652	-0.199351	
$E(LU)$			0.40240741				3	0.156664	-0.118927	
$E(CP)$			-0.01842169				4	0.790668	0.536044	
$E(LB)$			0.25634620		$E(LU)$			0.29062766		
4	2	1	-0.346974	-0.465455			$E(CP)$	0.03076329		
		2	1.346974	0.465455			$E(LB)$	0.20241844		
$E(LU)$			1.01477788		5	5	1	0.052975	-0.158131	
$E(CP)$			0.41350875				2	0.103531	-0.155707	
$E(LB)$			0.46438768				3	0.163808	-0.111820	
4	3	1	-0.044975	-0.297651				4	0.246092	-0.005600
		2	0.088057	0.234054				5	0.433593	0.431259
		3	0.956918	0.531705	$E(LU)$				0.23040495	
$E(LU)$			0.42315147		$E(CP)$				-0.02913523	
$E(CP)$			0.08477554		$E(LB)$				0.14284288	
$E(LB)$			0.28172930		6	2	1	-0.588298	-0.477782	
4	4	1	0.064336	-0.203052			2	1.588298	0.477782	
		2	0.147340	-0.182749	$E(LU)$				1.48102383	
		3	0.261510	-0.070109	$E(CP)$				0.63148980	
		4	0.526813	0.455910	$E(LB)$				0.47734078	
$E(LU)$			0.29247651		6	3	1	-0.211474	-0.311047	
$E(CP)$			-0.02831210				2	-0.112994	-0.271381	
$E(LB)$			0.18386193		$E(LU)$			3	1.324468	0.583229
					$E(CP)$				0.57539484	
					$E(LB)$				0.23269610	
									0.30173252	

TABLE OF WEIGHTS (CONTINUED)

N	M	I	A(N,M,I)	C(N,M,I)	N	M	I	A(N,M,I)	C(N,M,I)
6	4	1	-0.063569	-0.225141	7	6	1	0.013524	-0.138436
		2	-0.006726	-0.209083			2	0.041588	-0.140342
		3	0.079882	-0.146386			3	0.075499	-0.121821
		4	0.990412	0.580610			4	0.117461	-0.082938
E(LU)			0.31552097				5	0.172092	-0.015394
E(CP)			0.08035062				6	0.579835	0.498931
E(LB)			0.21242254		E(LU)			0.18269947	
					E(CP)			-0.00130057	
					E(LB)			0.12760617	
6	5	1	0.007521	-0.169920	7	7	1	0.038743	-0.108323
		2	0.048328	-0.166319			2	0.064086	-0.113479
		3	0.101608	-0.129510			3	0.090785	-0.103569
		4	0.172859	-0.054453			4	0.120971	-0.078268
		5	0.669685	0.520201			5	0.157657	-0.032632
E(LU)			0.22351297				6	0.207825	0.054727
E(CP)			0.00888019				7	0.319934	0.382022
E(LB)			0.15690540						
6	6	1	0.044826	-0.128810	E(LU)			0.16219070	
		2	0.079377	-0.132102	E(CP)			-0.02578937	
		3	0.117541	-0.111951	E(LB)			0.09836496	
		4	0.163591	-0.064666					
		5	0.226486	0.031796	8	2	1	-0.752513	-0.483610
		6	0.368179	0.405733			2	1.752513	0.483616
E(LU)			0.19030430		E(LU)			1.91861540	
E(CP)			-0.02771574		E(CP)			0.78453314	
E(LB)			0.11657671		E(LB)			0.48337662	
7	2	1	-0.676894	-0.481140	8	3	1	-0.323875	-0.317890
		2	1.676894	0.481140			2	-0.243808	-0.288231
E(LU)			1.70468001				3	1.567683	0.606120
E(CP)			0.71366553		E(LU)			0.76198737	
E(LB)			0.48082310		E(CP)			0.33734068	
					E(LB)			0.31047652	
7	3	1	-0.272195	-0.315369	8	4	1	-0.149973	-0.232805
		2	-0.184061	-0.281139			2	-0.105015	-0.220324
		3	1.456255	0.596507			3	-0.032257	-0.176675
E(LU)			0.66758707				4	1.287245	0.629805
E(CP)			0.28885432		E(LU)			0.39805551	
E(LB)			0.30681307		E(CP)			0.15928131	
					E(LB)			0.22335819	
7	4	1	-0.110274	-0.229691	8	5	1	-0.062656	-0.180231
		2	-0.060226	-0.215613			2	-0.032248	-0.176510
		3	0.018671	-0.164168			3	0.012767	-0.149566
		4	1.151829	0.609472			4	0.072446	-0.101642
E(LU)			0.35349223				5	1.009691	0.607948
E(CP)			0.12260834		E(LU)			0.25192092	
E(LB)			0.21884662		E(CP)			0.07129172	
					E(LB)			0.17037848	
7	5	1	-0.030368	-0.176203	8	6	1	-0.013509	-0.143834
		2	0.004333	-0.172399			2	0.010292	-0.145006
		3	0.052957	-0.141218			3	0.041357	-0.128393
		4	0.117599	-0.082820			4	0.080475	-0.095696
		5	0.855480	0.572649			5	0.130327	-0.043280
E(LU)			0.23316740				6	0.751058	0.556209
E(CP)			0.04212562		E(LU)			0.18599844	
E(LB)			0.16497315		E(CP)			0.02247163	
					E(LB)			0.13422386	

TABLE OF WEIGHTS (CONTINUED)

N	M	I	A(N,M,I)	C(N,M,I)	N	M	I	A(N,M,I)	C(N,M,I)	
8	7	1	0.015973	-0.116317	9	7	1	-0.004220	-0.120988	
		2	0.036729	-0.120331			2	0.013386	-0.124245	
		3	0.060439	-0.110582			3	0.035068	-0.115091	
		4	0.088239	-0.088450			4	0.061198	-0.093508	
		5	0.122062	-0.050995			5	0.093013	-0.064162	
		6	0.165529	0.009700			6	0.132740	-0.017187	
		7	0.511030	0.476975			7	0.668815	0.537180	
E(LU)			0.15505149		E(LU)			0.15547192		
E(CP)			-0.00641304		E(CP)			0.01139509		
E(LB)			0.10726405		E(LB)			0.11276822		
8	8	1	0.034052	-0.093270	9	8	1	0.016797	-0.100011	
		2	0.093552	-0.098886			2	0.032919	-0.104750	
		3	0.073452	-0.093994			3	0.050582	-0.099608	
		4	0.095062	-0.079752			4	0.070497	-0.086226	
		5	0.119768	-0.053918			5	0.093635	-0.063541	
		6	0.149934	-0.010179			6	0.121560	-0.028346	
		7	0.191236	0.069325			7	0.157175	0.026525	
		8	0.282943	0.360675			8	0.456836	0.455956	
E(LU)			0.14136026		E(LU)			0.13496842		
E(CP)			-0.02386561		E(CP)			-0.00906894		
E(LB)			0.08501680		E(LB)			0.09236358		
9	2	1	-0.818444	-0.485517	9	9	1	0.030338	-0.081777	
		2	1.818444	0.485517			2	0.045872	-0.087308	
E(LU)			2.12272209		E(CP)			0.061368	-0.085084	
E(CP)			0.84680378		E(LB)			0.077742	-0.016470	
E(LB)			0.48532951					0.095769	-0.060667	
9	3	1	-0.368833	-0.319786			6	0.116517	-0.035136	
		2	-0.295280	-0.293621			7	0.141932	0.006001	
		3	1.664113	0.613497			8	0.176764	0.078828	
E(LU)			0.85621748		E(LU)			9	0.253697	0.341614
E(CP)			0.37995861		E(CP)			0.12529518		
E(LB)			0.31324611		E(LB)			-0.02209438		
								0.07482425		
9	4	1	-0.184461	-0.235080	10	2	1	-0.876869	-0.487022	
		2	-0.143505	-0.223891			2	1.876869	0.487022	
		3	-0.075815	-0.185970	E(LU)			2.31744054		
		4	1.403781	0.644941	E(CP)			0.90232208		
E(LU)			0.44625568		E(LB)			0.48687150		
E(CP)			0.19160927							
E(LB)			0.22671251							
9	5	1	-0.090726	-0.183061	10	3	1	-0.408602	-0.321265	
		2	-0.063541	-0.179515			2	-0.340443	-0.297858	
		3	-0.021495	-0.155825	E(LU)			3	1.749045	0.619124
		4	0.034159	-0.115133	E(CP)			0.94907551		
		5	1.141604	0.633534	E(LB)			0.41795081		
E(LU)			0.27605014					0.31541467		
E(CP)			0.09715351							
E(LB)			0.17429417							
9	6	1	-0.037118	-0.147411	E(LU)			-0.214930	-0.236817	
		2	-0.016377	-0.148150	E(CP)			2 -0.177223	-0.226688	
		3	0.012499	-0.133219	E(LB)			3 -0.113820	-0.193159	
		4	0.049305	-0.105060				4 1.505973	0.656663	
		5	0.053614	-0.062073				0.49619736		
		6	0.896078	0.595913				0.22047816		
E(LU)			0.19579592					0.22930885		
E(CP)			0.04378261							
E(LB)			0.13880129							

TABLE OF WEIGHTS (CONTINUED).

N	M	I	A(N,M,I)	C(N,M,I)	N	M	I	A(N,M,I)	C(N,M,I)	
10	5	1	-0.115524	-0.185169	10	10	1	0.027331	-0.072734	
		2	-0.090868	-0.181821			2	0.040034	-0.077971	
		3	-0.051341	-0.160697			3	0.052496	-0.077242	
		4	0.000975	-0.125311			4	0.065408	-0.071876	
		5	1.250144	0.652997			5	0.074263	-0.061652	
E(LU)			0.30364549				6	0.094638	-0.045420	
E(CP)			0.1210305				7	0.112414	-0.020698	
E(LB)			0.17727542				8	0.134239	0.017927	
							9	0.164179	0.085070	
					10		1	0.230001	0.324597	
10	6	1	-0.058017	-0.149985	E(LU)			0.11252220		
		2	-0.039595	-0.150451	E(CP)				-0.02050852	
		3	-0.012513	-0.136941	E(LB)				0.06679250	
		4	0.022314	-0.112224						
		5	0.065750	-0.075721						
		6	1.022062	0.625321	11	2	1	-0.929310	-0.488243	
E(LU)			0.20973843				2	1.929310	0.488243	
E(CP)			0.06299841		E(LU)			2.50340024		
E(LB)			0.14219828		E(CP)			0.95239887		
					E(LB)				0.48812000	
10	7	1	-0.022198	-0.124170						
		2	-0.006909	-0.126854	11	3	1	-0.444245	-0.322452	
		3	0.013224	-0.118392			2	-0.380642	-0.301277	
		4	0.037994	-0.100924			3	1.824887	0.62729	
		5	0.068153	-0.073988	E(LU)			1.03995578		
		6	0.105164	-0.035501	E(CP)			0.45220741		
		7	0.804572	0.579868	E(LB)				0.31715330	
E(LU)			0.16066059							
E(CP)			0.02762724		11	4	1	-0.242206	-0.238188	
E(LB)			0.11670571				2	-0.207204	-0.228941	
							3	-0.147490	-0.198888	
10	8	1	0.001179	-0.104082				4	1.596900	0.666017
		2	0.014889	-0.108163	E(LU)			0.54681985		
		3	0.030998	-0.103119	E(CP)			0.24633583		
		4	0.049734	-0.090835	E(LB)			0.23138012		
		5	0.071745	-0.070902						
		6	0.098114	-0.041560	11	5	1	-0.137718	-0.186803	
		7	0.130649	0.000799			2	-0.115110	-0.183651	
		8	0.602892	0.517864			3	-0.077762	-0.164597	
E(LU)			0.13403554				4	-0.028411	-0.133278	
E(CP)			0.00474963				5	1.359000	0.668329	
E(LB)			0.29704810		E(LU)			0.33282848		
					E(CP)			0.14129911		
10	9	1	0.016841	-0.087538	E(LB)			0.17962678		
		2	0.029807	-0.092405						
		3	0.043570	-0.089839	11	6	1	-0.076739	-0.151936	
		4	0.058640	-0.081428			2	-0.060142	-0.152221	
		5	0.075576	-0.066855			3	-0.034581	-0.139907	
		6	0.095169	-0.044670			4	-0.001490	-0.117886	
		7	0.118707	-0.011816			5	0.039510	-0.086131	
		8	0.148575	0.038159			6	1.133434	0.648081	
		9	0.413116	0.436394	E(LU)			0.22640907		
E(LU)			0.11965747		E(CP)			0.08045010		
E(CP)			-0.01043859		E(LB)			0.14483423		
E(LB)			0.08100409							
					11	7	1	-0.038349	-0.126507	
							2	-0.024842	-0.128838	
							3	-0.005964	-0.120951	
							4	0.017632	-0.105219	
							5	0.646354	-0.081602	
							6	0.081182	-0.048929	
							7	0.923987	0.612047	
					E(LU)			0.16905710		
					E(CP)			0.04246025		
					E(LB)			0.11966982		

TABLE OF WEIGHTS (CONTINUED)

N	M	I	A(N,M,I)	C(N,M,I)	N	M	I	A(N,M,I)	C(N,M,I)	
11	8	1	-0.012943	-0.106922	12	3	1	-0.476530	-0.323426	
		2	-0.001050	-0.110498			2	-0.416836	-0.304093	
		3	0.013869	-0.105662			3	1.893357	0.627519	
		4	0.031661	-0.094495	E(LU)			1.12857097		
		5	0.052723	-0.076693	E(CP)			0.48338667		
		6	0.077815	-0.051525	E(LB)			0.31859354		
		7	0.108161	-0.016860						
		8	0.729765	0.562564	12	4	1	-0.266888	-0.239300	
			E(LU)	0.13669382			2	-0.234180	-0.230796	
			E(CP)	0.01751192			3	-0.177681	-0.203562	
			E(LB)	0.10043756			4	1.678749	0.673657	
					E(LU)			0.59748043		
11	9	1	0.004425	-0.091115	E(CP)			0.27023774		
		2	0.015498	-0.095437	E(LB)			0.23307201		
		3	0.028023	-0.092780						
		4	0.042178	-0.084833	12	5	1	-0.157792	-0.1881C9	
		5	0.058340	-0.071581			2	-0.136884	-0.185142	
		6	0.077093	-0.052182			3	-0.101445	-0.167790	
		7	0.099349	-0.024880			4	-0.054640	-0.139643	
		8	0.126592	0.013605			5	1.450761	0.680734	
		9	0.548502	0.499201	E(LU)			0.36338878		
			E(LU)	0.11809425	E(CP)			0.16042600		
			E(CP)	0.00058414	E(LB)			0.18153147		
			E(LB)	0.08503131						
11	10	1	0.016502	-0.077717	12	6	1	-0.093679	-0.153471	
		2	0.027205	-0.082449			2	-0.078561	-0.153632	
		3	0.038291	-0.081388			3	-0.054320	-0.142329	
		4	0.050160	-0.075977			4	-0.022769	-0.122474	
		5	0.063170	-0.066222			5	0.016136	-0.094355	
		6	0.077772	-0.051429			6	2.233193	0.666261	
		7	0.094625	-0.030120	E(LU)			0.24690094		
		8	0.114811	0.000537	E(CP)			0.09641022		
		9	0.140333	0.046381	E(LB)			0.14694548		
		10	0.377130	0.418384						
			E(LU)	0.10756449	12	7	1	-0.052987	-0.128308	
			E(CP)	-0.01109747			2	-0.040893	-0.130339	
			E(LB)	0.0720Y183			3	-0.023072	-0.123C07	
							4	-0.000515	-0.10^712	
11	11	1	0.024850	-0.065444				5	0.026930	-0.087681
		2	0.035456	-0.070318				6	0.059918	-0.059256
		3	0.045727	-0.070456	E(LU)			7	1.030620	0.637304
		4	0.056215	-0.067076	E(CP)			0.17967935		
		5	0.067261	-0.060207	E(LB)			0.05607919		
		6	0.079220	-0.049300				0.12200601		
		7	0.092560	-0.033156	12	8	1	-0.025785	-0.109045	
		8	0.108034	-0.009427			2	-0.015312	-0.112224	
		9	0.127068	0.026879			3	-0.001353	-0.107627	
		10	0.153197	0.089148			4	0.015634	-0.097276	
		11	0.210412	0.309357			5	0.035853	-0.081361	
			E(LU)	0.102i2039			6	0.059835	-0.059315	
			E(CP)	-0.01910164			7	0.088444	-0.029900	
			E(LB)	0.06030372			8	0.842684	0.596748	
					E(LU)			0.14186580		
12	2	1	-0.976872	-0.489254	E(CP)			0.02930146		
		2	1.976872	0.489254	E(LB)			0.10304331		
			E(LU)	2.68127021						
			E(CP)	0.99799849						
			E(LB)	0.48915157						

TABLE OF WEIGHTS (CONTINUED)

N	M	I	A(N,M,I)	C(N,M,I)	N	M	I	A(N,M,I)	C(N,M,I)
12	9	1	-0.006944	-0.093658	13	3	1	-0.506031	-0.324239
		2	0.002669	-0.097540			2	-0.449735	-0.306454
		3	0.014239	-0.094893			3	1.955765	0.630694
		4	0.027669	-0.087448	E(LU)			1.21490934	
		5	0.043189	-0.075371	E(CP)			0.51198847	
		6	0.061225	-0.058180	E(LB)			0.31979363	
		7	0.082441	0.034802					
		8	0.107856	0.003342	13	4	1	-0.289420	-0.240219
		9	0.667655	0.545234			2	-0.258687	-0.232349
		E(LU)	0.11929957				3	-0.205024	-0.207450
		E(CP)	0.01087297				4	1.753131	0.680016
		E(LB)	0.08799386		E(LU)			0.64778295	
					E(CP)			0.29204583	
					E(LB)			0.23448055	
12	10	1	0.006411	-0.080881					
		2	0.015598	-0.085171	13	5	1	-0.176109	-0.189177
		3	0.025675	-0.083952			2	-0.156637	-0.186381
		4	0.036799	-0.073714			3	-0.122893	-0.170454
		5	0.049211	-0.069610			4	-0.078337	-0.144971
		6	0.063256	-0.062337			5	1.533976	0.690983
		7	0.07947	-0.037675	E(LU)			0.39459617	
		8	0.098522	-0.012272	E(CP)			0.1.799724	
		9	0.121752	0.022956	E(LB)			0.18310709	
		10	0.503338	0.481555					
		E(LU)	0.10573141						
		E(CP)	-0.00210755		13	6	1	-0.109140	-0.154711
		E(LB)	0.07557504				2	-0.095246	-0.154785
							3	-0.072165	-0.144347
12	11	1	0.012382	-0.069793			4	-0.041997	-0.126268
		2	0.024957	-0.074285			5	-0.004940	-0.101028
		3	0.034103	-0.074131			6	1.323488	0.681140
		4	0.043790	-0.070017	E(LU)			0.26460952	
		5	0.054149	-0.063891	E(CP)			0.11109896	
		6	0.065515	-0.053621	E(LB)			0.14867755	
		7	0.078264	-0.039034					
		8	0.092952	-0.018715	13	7	1	-0.066358	-0.129743
		9	0.110521	0.009948			2	-0.055414	-0.131538
		10	0.132666	0.052280			3	-0.038503	-0.124701
		11	0.347033	0.401864			4	-0.016879	-0.111609
		E(LU)	0.09775217				5	0.009416	-0.092649
		E(CP)	-0.01134890				6	0.040810	-0.067475
		E(LB)	0.06487266				7	1.126930	0.657714
					E(LU)			0.19187273	
12	12	1	0.022771	-0.059449	E(CP)			0.06864731	
		2	0.031776	-0.063952	E(LB)			0.12390133	
		3	0.040408	-0.064601					
		4	0.049122	-0.062489	13	8	1	-0.037540	-0.110704
		5	0.058175	-0.057754			2	-0.028206	-0.113563
		6	0.067800	-0.050337			3	-0.015049	-0.109206
		7	0.078261	-0.039010			4	0.001231	-0.099644
		8	0.090017	-0.023199			5	0.020686	-0.085204
		9	0.103664	-0.000505			6	0.043677	-0.065581
		10	0.120475	0.033696			7	0.070830	-0.039995
		11	0.143566	0.091751			8	0.944372	0.623896
		12	0.193747	0.295648	E(LU)			0.14885020	
		E(LU)	0.09348388		E(CP)			0.04022462	
		E(CP)	-0.01785537		E(LB)			0.10512398	
		E(LB)	0.05495436						
13	2	1	-1.020378	-0.490105					
		2	1.020377	0.490105					
		E(LU)	2.85169694						
		E(CP)	1.03985071						
		E(LB)	0.49001823						

TABLE OF WEIGHTS (CONTINUED)

N	M	I	A(N,M,I)	C(N,M,I)	N	M	I	A(N,M,I)	C(N,M,I)		
13	9	1	-0.017389	-0.095590	13	13	1	0.021005	-0.054436		
		2	-0.008934	-0.099109			2	0.028757	-0.058585		
		3	0.001863	-0.096521			3	0.036127	-0.059535		
		4	0.014684	-0.089554			4	0.043501	-0.058259		
		5	0.029637	-0.078490			5	0.051078	-0.054942		
		6	0.047027	-0.063068			6	0.059028	-0.049472		
		7	0.067346	-0.042607			7	0.067533	-0.041504		
		8	0.091328	-0.015928			8	0.076631	-0.030398		
		9	0.774437	0.580865			9	0.087274	-0.015037		
		E(LU)	0.12250342				10	0.099441	0.006644		
		E(CP)	0.02046326				11	0.114446	0.038943		
		E(LB)	0.09030201				12	0.135068	0.093324		
							13	0.179913	0.283257		
13	10	1	-0.002927	-0.083170	E(LU)			0.08619744			
		2	0.005067	-0.087085	E(CP)			-0.01674714			
		3	0.014356	-0.085792	E(LB)			0.05046988			
		4	0.024891	-0.080789			14	2	1		
		5	0.036816	-0.072325	E(LU)			-1.060461	-0.490831		
		6	0.050389	-0.060181	E(CP)			2	2.060411	0.490831	
		7	0.065995	-0.043768	E(LB)			3.01527198			
		8	0.084201	-0.022048				1.07852097			
		9	0.105863	0.006715	E(LU)			0.49075663			
		10	0.615348	0.528441	E(CP)						
		E(LB)	0.10607774		E(LB)						
						14	3	1	-0.533185	-0.324929	
		E(CP)	0.00635741		E(LU)			2	-0.479874	-0.308462	
		E(LB)	0.07818835		E(CP)			3	2.013059	0.633391	
					E(LB)				1.29865775		
13	11	1	0.007628	-0.072617	E(LU)				0.53840104		
		2	0.015408	-0.076746	E(CP)					0.32081269	
		3	0.023732	-0.076418	E(LB)						
		4	0.032743	-0.072938			14	4	1	-0.310144	-0.240992
		5	0.042611	-0.066531	E(LU)			2	-0.281132	-0.233670	
		6	0.053556	-0.057014	E(CP)			3	-0.229990	-0.210735	
		7	0.065876	-0.043886	E(LB)			4	1.821266	0.685397	
		8	0.080005	-0.026244					0.69748231		
		9	0.096594	-0.002552	E(LU)					0.31216081	
		10	0.116703	0.029910	E(CP)					0.23567174	
		11	0.465143	0.465037	E(LB)						
		E(LU)	0.09583611			14	5	1	-0.192947	-0.199058	
		E(CP)	-0.00388188				2	-0.174709	-0.187427		
		E(LB)	0.06795140				3	-0.142478	-0.172710		
							4	-0.099930	-0.149393		
13	12	1	0.015382	-0.063288	E(LU)			5	1.610065	0.699598	
		2	0.023100	-0.067492	E(CP)				0.42609561		
		3	0.030818	-0.067892	E(LB)					0.19423903	
		4	0.038824	-0.065622						0.18443288	
		5	0.047302	-0.060887			14	6	1	-0.123352	-0.155736
		6	0.056444	-0.053540	E(LU)			2	-0.110490	-0.155747	
		7	0.066482	-0.043158	E(CP)			3	-0.088443	-0.146054	
		8	0.077739	-0.028970	E(LB)			4	-0.059523	-0.129460	
		9	0.090699	-0.009644				5	-0.024111	-0.106556	
		10	0.106166	0.017233	E(LU)			6	1.405919	0.693553	
		11	0.125627	0.056547	E(CP)					0.28511973	
		12	0.321416	0.386713	E(LB)						
		E(LU)	0.08941947						0.12469427		
		E(CP)	-0.01136145							0.15012578	
		E(LB)	0.05895232								

TABLE OF WEIGHTS (CONTINUED)

N	M	I	A(N,M,I)	C(N,M,I)	N	M	I	A(N,M,I)	C(N,M,I)
14	7	1	-0.078656	-0.130915	14	12	1	0.008361	-0.065816
		2	-0.069666	-0.132521			2	0.015058	-0.069728
		3	-0.052554	-0.126123			3	0.022076	-0.069962
		4	-0.031776	-0.114051			4	0.029552	-0.067659
		5	-0.006532	-0.096788			5	0.037615	-0.063070
		6	0.023467	-0.074184			6	0.046411	-0.056130
		7	1.214708	0.674581			7	0.056132	-0.046558
		E(LU)	0.2051843*				8	0.067039	-0.033834
		E(CP)	0.08030259				9	0.079506	-0.017101
		E(LB)	0.12547311				10	0.094096	0.005064
							11	0.111723	0.035156
							12	0.432431	0.449638
14	8	1	-0.048365	-0.112041	E(LU)			0.08771669	
		2	-0.039964	-0.114637	E(CP)			-0.005056397	
		3	-0.027495	-0.110509	E(LB)			0.06168210	
		4	-0.011849	-0.101635					
		5	0.006905	-0.088422					
		6	0.029002	-0.070734	14	13	1	0.014760	-0.057849
		7	0.054897	-0.048074			2	0.021453	-0.061764
		8	1.036868	0.646052			3	0.020864	-0.062506
		E(LU)	0.15716466				4	0.034842	-0.061074
		E(CP)	0.05038249				5	0.041933	-0.057693
		E(LB)	0.10683049				6	0.069474	-0.052317
							7	0.057519	-0.044707
							8	0.066569	-0.034426
14	9	1	-0.027030	-0.097117			9	0.076605	-0.020713
		2	-0.019516	-0.100334			10	0.088151	-0.002338
		3	-0.009363	-0.097327			11	0.101914	0.022943
		4	0.002928	-0.091298			12	0.119200	0.059643
		5	0.017368	-0.081103			13	0.299416	0.372795
		6	0.034165	-0.067124	E(LU)			0.08276211	
		7	0.053685	-0.048921	E(CP)			-0.01123278	
		8	0.076476	-0.025720	E(LB)			0.05400148	
		9	0.871267	0.609445					
		E(LU)	0.12719148						
		E(CP)	0.02941694						
		E(LB)	0.09216556		14	14	1	0.019487	-0.050186
							2	0.026238	-0.054008
14	10	1	-0.011580	-0.084931			3	0.032614	-0.055130
		2	-0.004548	-0.085228			4	0.038947	-0.054419
		3	0.004100	-0.087207			5	0.045399	-0.052075
		4	0.014144	-0.082451			6	0.052097	-0.048056
		5	0.025647	-0.074573			7	0.059168	-0.042197
		6	0.038794	-0.063473			8	0.06767	-0.034099
		7	0.053879	-0.048768			9	0.075102	-0.023149
		8	0.071335	-0.029776			10	0.084482	-0.008285
		9	0.091783	-0.005398			11	0.095426	0.012430
		10	0.716445	0.565105			12	0.108942	0.043015
		E(LU)	0.10903536				13	0.127523	0.094166
		E(CP)	0.01430729				14	0.167807	0.272014
		E(LB)	0.08024763		E(LU)			0.07996685	
					E(CP)			-0.01576372	
					E(LB)			0.04665712	
14	11	1	-0.000170	-0.074686					
		2	0.006622	-0.078499	15	2	1	-1.097617	-0.491458
		3	0.014283	-0.078054			2	2.097617	0.491458
		4	0.022800	-0.074680	E(LU)			3.17256460	
		5	0.032273	-0.068624	E(CP)			1.11445612	
		6	0.042866	-0.059816	E(LB)			0.49139327	
		7	0.054817	-0.047926					
		8	0.068463	-0.032355					
		9	0.084290	-0.012126					
		10	0.103025	0.014349					
		11	0.570731	0.512429	E(LU)			1.38015851	
		E(LU)	0.09566494		E(CP)			0.56295169	
		E(CP)	0.00320655		E(LB)			0.32168886	
		E(LB)	0.07027548						

TABLE OF WEIGHTS (CONTINUED)

N	M	I	A(N,M,I)	C(N,M,I)	N	M	I	A(N,M,I)	C(N,M,I)		
15	4	1	-0.329324	-0.241651	15	10	1	-0.019626	-0.086339		
		2	-0.301829	-0.234806			2	-0.013383	-0.089664		
		3	-0.252948	-0.213548			3	-0.005271	-0.088341		
		4	1.884101	0.690005			4	0.004351	-0.083828		
E(LU)			0.74642859				5	0.015475	-0.076474		
E(CP)			0.33084387				6	0.028227	-0.066261		
E(LB)			0.23669248				7	0.042832	-0.052943		
15	5	1	-0.208525	-0.190823			8	0.059624	-0.036054		
		2	-0.191357	-0.188323			9	0.079072	-0.014863		
		3	-0.160491	-0.174645	E(LU)		10	0.808700	0.594768		
		4	-0.119743	-0.153153	E(CP)				0.02177795		
		5	1.680121	0.706944	E(LB)				0.08192516		
E(LU)			0.45754555								
E(CP)			0.20933279		15	11	1	-0.007450	-0.076297		
E(LB)			0.18556433			2	-0.001467	-0.079835			
15	6	1	-0.136498	-0.156597			3	0.005652	-0.079332		
		2	-0.124518	-0.156563			4	0.013759	-0.076068		
		3	-0.103401	-0.147517			5	0.022893	-0.070355		
			-0.075614	-0.132162			6	0.033174	-0.062181		
			-0.041680	-0.111215			7	0.044787	-0.051331		
			1.481712	0.704074			8	0.057997	-0.037396		
E(LU)			0.30614004				9	0.073190	-0.019723		
E(CP)			0.13734100				10	0.090865	0.002701		
E(LB)			0.15135556				11	0.666610	0.549817		
					E(LU)				0.09681113		
					E(CP)				0.000989471		
					E(LB)				0.07212492		
15	7	1	-0.090036	-0.111891			15	12	1	0.001756	-0.067695
		2	-0.080850	-0.133342				2	0.007624	-0.071342	
		3	-0.065446	-0.127335				3	0.014079	-0.071459	
		4	-0.045441	-0.116138				4	0.021133	-0.069178	
		5	-0.021137	-0.100291				5	0.028861	-0.064779	
		6	0.007597	-0.079774				6	0.037374	-0.058256	
		7	1.295312	0.688771				7	0.046827	-0.049425	
E(LU)			0.21929214					8	0.057431	-0.037926	
E(CP)			0.09116039								
E(LB)			0.12679942								
					E(LU)				0.00098946		
					E(CP)				0.00094612		
					E(LB)				0.06376409		
15	8	1	-0.058390	-0.113143			15	13	1	0.008779	-0.060130
		2	-0.050767	-0.115520				2	0.014620	-0.063805	
		3	-0.038897	-0.111607				3	0.020637	-0.064394	
		4	-0.023825	-0.103332				4	0.026961	-0.062900	
		5	-0.005717	-0.091156	E(LU)			5	0.033693	-0.059574	
		6	0.015565	-0.075053	E(CP)				6	0.040939	-0.054417
		7	0.040351	-0.054703	E(LB)						
		8	1.121680	0.664514							
E(LU)			0.16646559								
E(CP)			0.05986446								
E(LB)			0.10825884								
15	9	1	-0.035972	-0.098361							
		2	-0.029235	-0.101322							
		3	-0.019633	-0.098904							
		4	-0.007812	-0.092773							
		5	0.006156	-0.083327							
		6	0.022403	-0.070544							
		7	0.041203	-0.054142							
		8	0.062969	-0.03395							
		9	0.959920	0.632967	E(LU)						
E(LU)			0.13300106		E(CP)				0.08092217		
E(CP)			0.03779810		E(LB)				-0.00585240		
E(LB)			0.09370837						0.05644073		

TABLE OF WEIGHTS (CONTINUED)

N	M	I	A(N,M,I)	C(N,M,I)	N	M	I	A(N,M,I)	C(N,M,I)	
15	14	1	0.014143	-0.053241	16	5	1	-0.223015	-0.191470	
		2	0.020013	-0.056879			2	-0.206788	-0.189099	
		3	0.025750	-0.057827			3	-0.177158	-0.176323	
		4	0.031576	-0.056973			4	-0.138048	-0.156390	
		5	0.037611	-0.054542			5	1.745009	0.713282	
		6	0.043958	-0.050539	E(LU)			0.48908000		
		7	0.050725	-0.044833	E(CP)			0.22342597		
		8	0.058045	-0.037157	E(LB)			0.18654151		
		9	0.066092	-0.027072						
		10	0.075114	-0.013872	16	6	1	-0.148725	-0.157331	
		11	0.085490	0.003612			2	-0.137508	-0.157263	
		12	0.097844	0.027465			3	-0.117232	-0.148785	
		13	0.113340	0.061879			4	-0.090481	-0.134532	
		14	0.260298	0.359980			5	-0.057883	-0.115196	
				0.07689745			6	1.551828	0.713108	
		E(LU)		-0.01102126	E(LU)			0.32746210		
		E(CP)		0.04980248	E(CP)			0.14915808		
		E(LB)			E(LB)			0.15241337		
15	15	1	0.018170	-0.046538						
		2	0.024108	-0.050064	16	7	1	-0.100621	-0.132718	
		3	0.029685	-0.051279			2	-0.092121	-0.134040	
		4	0.035191	-0.050957			3	-0.077354	-0.128381	
		5	0.040762	-0.049293			4	-0.058057	-0.117942	
		6	0.046496	-0.046315			5	-0.034624	-0.103296	
		7	0.052488	-0.041899			6	-0.007020	-0.084506	
		8	0.058844	-0.035827			7	1.369798	0.700883	
		9	0.065696	-0.027731	E(LU)			0.23396225		
		10	0.073230	-0.017008	E(CP)			0.10131710		
		11	0.081725	-0.002653	E(LB)			0.12793461		
		12	0.091651	0.017156						
		13	0.103914	0.046191	16	8	1	-0.067719	-0.114069	
		14	0.120784	0.094483			2	-0.060754	-0.116260	
		15	0.157255	0.261738			3	-0.049415	-0.112545	
		E(LU)		0.0747775			4	0.034868	-0.104798	
		E(CP)		-0.01488220			5	-0.017357	-0.093508	
		E(LB)		0.04337628			6	0.03178	-0.078726	
							7	0.026873	-0.060251	
16	2	1	-1.132243	-0.492005			8	1.199963	0.680158	
		2	2.132243	0.492005	E(LU)			0.17650200		
		E(LU)		3.32404220	E(CP)			0.06874770		
		E(CP)		1.14801534	E(LB)			0.10947376		
		E(LB)		0.49194784						
16	3	1	-0.581757	-0.326035	16	9	1	-0.044303	-0.099396	
		2	-0.533457	-0.311694			2	-0.038218	-0.102138	
		3	2.115214	0.637730			3	-0.029094	-0.099811	
		E(LU)		1.45938438			4	-0.017697	-0.094037	
		E(CP)		0.58582769			5	-0.004166	-0.085242	
		E(LB)		0.32245028			6	0.011570	-0.073467	
							7	0.029712	-0.058535	
16	4	1	-0.347172	-0.242220			8	0.050576	-0.040084	
		2	-0.321026	-0.235794	E(LU)			9	1.041619	0.652711
		3	-0.274186	-0.215984	E(CP)			0.13966768		
		4	1.942384	0.693998	E(LB)			0.04566615		
		E(LU)		0.79453328				0.09501012		
		E(CP)		0.34828173						
		E(LB)		0.23757701						

TABLE OF WEIGHTS (CONTINUED)

N	M	I	A(N,M,I)	C(N,M,I)	N	M	I	A(N,M,I)	C(N,M,I)
16	10	1	-0.027135	-0.087496	16	14	1	0.008992	-0.055209
		2	-0.021550	-0.090585			2	0.014141	-0.058750
		3	-0.013895	-0.089277			3	0.019370	-0.059563
		4	-0.004646	-0.084992			4	0.024804	-0.058635
		5	0.006132	-0.078105			5	0.030525	-0.056268
		6	0.018515	-0.068653			6	0.036615	-0.052317
		7	0.032675	-0.056482			7	0.043164	-0.046878
		8	0.048869	-0.041268			8	0.050284	-0.039699
		9	0.067459	-0.022503			9	0.057124	-0.030467
		10	0.893576	0.619360			10	0.066884	-0.018695
E(LU)			0.11534960				11	0.076854	-0.003625
E(CP)			0.02881067				12	0.088469	0.015969
E(LB)			0.08332716				13	0.102433	0.042224
							14	0.379341	0.421953
16	11	1	-0.014263	-0.077587	E(LU)			0.07514429	
		2	-0.008950	-0.080895	E(CP)			-0.00637294	
		3	-0.002286	-0.080349	E(LB)			0.05199709	
		4	0.005469	-0.077213					
		5	0.014303	-0.071820	16	15	1	0.013547	-0.049291
		6	0.024297	-0.064207			2	0.018743	-0.052670
		7	0.035593	-0.054237			3	0.023778	-0.053739
		8	0.040404	-0.041625			4	0.02884	-0.053290
		9	0.063020	-0.025917			5	0.034060	-0.051538
		10	0.079847	-0.005432			6	0.039489	-0.048520
		11	0.754566	0.580293			7	0.045218	-0.044164
E(LU)			0.09897866				8	0.051338	-0.038307
E(CP)			0.01622073				9	0.057965	-0.030678
E(LB)			0.07364497				10	0.065253	-0.020850
							11	0.073425	-0.008153
16	12	1	-0.004450	-0.069172			12	0.082818	0.008503
		2	0.000732	-0.072584			13	0.03994	0.031075
		3	0.006721	-0.072615			14	0.107995	0.063476
		4	0.013424	-0.070383			15	0.263520	0.348149
		5	0.020868	-0.066184	E(LU)			0.07182155	
		6	0.029134	-0.060054	E(CP)			-0.01076262	
		7	0.038344	-0.051876	E(LB)			0.04619787	
		8	0.048668	-0.041398					
		9	0.060342	-0.028216	16	16	1	0.017016	-0.043375
		10	0.073692	-0.011716			2	0.022284	-0.046633
		11	0.089173	0.009035			3	0.027208	-0.047890
		12	0.623351	0.535164			4	0.032046	-0.047839
E(LU)			0.08784015				5	0.036912	-0.046675
E(CP)			0.00665801				6	0.041887	-0.044432
E(LB)			0.06543511				7	0.047042	-0.041053
							8	0.052455	-0.036402
16	13	1	0.003118	-0.061843			9	0.058216	-0.030249
		2	0.008256	-0.065297			10	0.064444	-0.022230
		3	0.013789	-0.065770			11	0.071304	-0.011772
		4	0.019747	-0.064259			12	0.079051	0.002079
		5	0.026189	-0.061031			13	0.088111	0.021046
		6	0.033196	-0.056120			14	0.099315	0.048675
		7	0.040872	-0.049427			15	0.114733	0.094419
		8	0.049357	-0.040731			16	0.147977	0.252333
		9	0.058836	-0.029675	E(LU)			0.06987019	
		10	0.069568	-0.015710	E(CP)			-0.01409012	
		11	0.081920	0.002010	E(LB)			0.04052374	
		12	0.096438	0.024833					
		13	0.498713	0.483018	17	2	1	-1.164659	-0.492486
E(LU)			0.08025299				2	2.164659	0.492486
E(CP)			-0.00069037		E(LU)			3.47015408	
E(LB)			0.05831799		E(CP)			1.17949167	
					E(LB)			0.49243526	

TABLE OF WEIGHTS (CONTINUED)

N	M	I	A(N,M,I)	C(N,M,I)	N	M	I	A(N,M,I)	C(N,M,I)	
17	3	1	-0.603668	-0.326486	17	9	1	-0.052096	-0.100271	
		2	-0.557497	-0.313014			2	-0.046565	-0.102825	
		3	2.161166	0.639500			3	-0.037862	-0.100587	
E(LU)			1.53642388				4	-0.026851	-0.095136	
E(CP)			0.60729095				5	-0.013728	-0.086910	
E(LB)			0.32311812				6	0.001531	-0.075995	
							7	0.019069	-0.062288	
17	4	1	-0.362861	-0.242716			8	0.039129	-0.045535	
		2	-0.338922	-0.236662			9	1.117373	0.669546	
		3	-0.293934	-0.218114	E(LU)			0.14699387		
		4	1.996717	0.697492	E(CP)			0.05307401		
E(LU)			0.84174810		E(LB)				0.09612512	
E(CP)			0.36462724							
E(LB)			0.23835098		17	10	1	-0.034167	-0.088465	
							2	-0.029139	-0.091350	
17	5	1	-0.236557	-0.192031			3	-0.021881	-0.090064	
		2	-0.221164	-0.169778			4	-0.012965	-0.085992	
		3	-0.192661	-0.177793			5	-0.002507	-0.079521	
		4	-0.155037	-0.159206			6	0.009531	-0.070728	
		5	1.805419	0.718809			7	0.023273	-0.059520	
E(LU)			0.52028442				8	0.038922	-0.045671	
E(CP)			0.23663986				9	0.056761	-0.028822	
E(LB)			0.18739415				10	0.972172	0.640135	
					E(LU)			0.12022174		
17	6	1	-0.160149	-0.157965	E(CP)			0.03544569		
		2	-0.149601	-0.157871	E(LB)			0.08451762		
		3	-0.130090	-0.149896						
		4	-0.104290	-0.136581	17	11	1	-0.020654	-0.078673	
		5	-0.072907	-0.118639			2	-0.015906	-0.081761	
		6	1.617037	0.720952			3	-0.009632	-0.081188	
E(LU)			0.34893506				4	-0.002186	-0.078180	
E(CP)			0.16024410				5	0.006378	-0.073083	
E(LB)			0.15333326				6	0.016104	-0.065964	
							7	0.027102	-0.056744	
17	7	1	-0.110512	-0.133428			8	0.039540	-0.045224	
		2	-0.102606	-0.134640			9	0.053648	-0.031078	
		3	-0.088415	-0.129294			10	0.069744	-0.013827	
		4	-0.069771	-0.119517	E(LU)			11	0.835861	0.605723
		5	-0.047139	-0.105901	E(CP)				0.10195092	
		6	-0.020560	-0.088568	E(LB)				0.022220540	
		7	1.439003	0.711349					0.07492279	
E(LU)			0.24902198							
E(CP)			0.11085361		17	12	1	-0.010286	-0.070375	
E(LB)			0.12891783				2	-0.005683	-0.073577	
							3	-0.000086	-0.073546	
17	8	1	-0.076441	-0.114859			4	0.006316	-0.071375	
		2	-0.070039	-0.116891			5	0.013511	-0.067372	
		3	-0.059173	-0.113357			6	0.021553	-0.061602	
		4	-0.045116	-0.106076			7	0.030535	-0.053996	
		5	-0.028154	-0.095554			8	0.140597	-0.044377	
		6	-0.008307	-0.081890			9	0.051928	-0.032455	
		7	0.014595	-0.064968			10	0.064785	-0.017797	
		8	1.272528	0.693595			11	0.079517	0.000228	
E(LU)			0.18708688				12	0.707314	0.566244	
E(CP)			0.07709833		E(LU)			0.08930564		
E(LB)			0.11052085		E(CP)			0.01208216		
					E(LB)				0.06681358	

TABLE OF WEIGHTS (CONTINUED)

N	M	I	A(N,M,I)	C(N,M,I)	N	M	I	A(N,M,I)	C(N,M,I)	
17	13	1	-0.002231	-0.063202	17	16	1	0.012979	-0.045870	
		2	0.002318	-0.066454			2	0.017617	-0.049609	
		3	0.007448	-0.066839			3	0.022076	-0.050145	
		4	0.013101	-0.065335			4	0.026538	-0.049982	
		5	0.019298	-0.062220			5	0.031091	-0.048727	
		6	0.026098	-0.057556			6	0.035799	-0.046430	
		7	0.033584	-0.051282			7	0.040724	-0.043057	
		8	0.041872	-0.043242			8	0.045932	-0.038508	
		9	0.051113	-0.033181			9	0.051504	-0.032609	
		10	0.061516	-0.020708			10	0.057542	-0.025090	
		11	0.073364	-0.005250			11	0.064186	-0.015545	
		12	0.087058	0.014056			12	0.071635	-0.003341	
		13	0.585461	0.521211			13	0.080193	0.012555	
E(LU)			0.08049558				14	0.090373	0.033974	
E(CP)			0.00423893				15	0.103110	0.064588	
E(LB)			0.05983608				16	0.248699	0.337194	
				E(LU)				0.06738336		
17	14	1	0.004088	-0.056878	E(CP)			-0.01047916		
		2	0.008636	-0.060131	E(LB)				0.04307100	
		3	0.013446	-0.060836						
		4	0.018560	-0.059871	17	17	1	0.015998	-0.040607	
		5	0.024028	-0.057487			2	0.020706	-0.043624	
		6	0.029909	-0.053742			3	0.025089	-0.044891	
		7	0.036278	-0.048586			4	0.029378	-0.045031	
		8	0.043231	-0.041881			5	0.033671	-0.044229	
		9	0.050892	-0.033402			6	0.038035	-0.042531	
		10	0.059426	-0.022749			7	0.042527	-0.039913	
		11	0.069060	-0.009558			8	0.047204	-0.036289	
		12	0.080119	0.00712			9	0.052133	-0.031512	
		13	0.093083	0.028459			10	0.057392	-0.025352	
		14	0.469244	0.469601			11	0.063089	-0.017458	
E(LU)			0.07436842				12	0.069375	-0.007282	
E(CP)			-0.00189289				13	0.076482	0.006082	
E(LB)			0.05369960				14	0.084803	0.024262	
				E(LU)				15	0.095098	0.050618
17	15	1	0.009066	-0.051176					0.109270	0.094076
		2	0.013648	-0.054390					0.139752	0.243681
		3	0.018244	-0.055341	E(LU)				0.06572241	
		4	0.022974	-0.054815	E(CP)				-0.01337530	
		5	0.027908	-0.053042	E(LB)				0.03802109	
		6	0.031111	-0.050075						
		7	0.038648	-0.045871	18	2	1	-1.195128	-0.492912	
		8	0.044600	-0.040314			2	2.195128	0.492912	
		9	0.051065	-0.033203	E(LU)				3.61129585	
		10	0.058176	-0.024231	E(CP)				1.20912723	
		11	0.066111	-0.012936	E(LB)				0.49286703	
		12	0.075128	0.001394						
		13	0.085616	0.019905	18	3	1	-0.624252	-0.326884	
		14	0.098200	0.044587			2	-0.580008	-0.314183	
		15	0.357506	0.409507			3	2.204260	0.641066	
E(LU)			0.07016498		E(LU)				1.61137253	
E(CP)			-0.00670775		E(CP)				0.62748837	
E(LB)			0.04818440		E(LB)				0.32370865	
18	4	1	-0.379529	-0.243153						
		2	-0.355679	-0.237429						
		3	-0.312382	-0.215992						
		4	2.047590	0.700574						
				E(LU)					0.88805128	
				E(CP)					0.38000703	
				E(LB)					0.23903395	

TABLE OF WEIGHTS (CONTINUED)

N	M	I	A(N,M,I)	C(N,M,I)	N	M	I	A(N,M,I)	C(N,M,I)	
18	5	1	-0.249266	-0.192523	18	10	1	-0.040776	-0.089291	
		2	-0.234618	-0.190376			2	-0.036223	-0.091997	
		3	-0.207148	-0.179091			3	-0.029314	-0.090739	
		4	-0.170883	-0.161679			4	-0.020701	-0.086863	
		5	1.861914	0.723670			5	-0.010540	-0.080764	
E(LU)			0.55118001				6	0.001172	-0.072544	
E(CP)			0.24907530				7	0.014523	-0.062157	
E(LB)			0.18814472				8	0.029671	-0.049465	
							9	0.046841	-0.034147	
16	6	1	-0.170868	-0.158518	10	1	1.045347	0.657947		
		2	-0.160910	-0.158405			0.12567798			
		3	-0.142100	-0.150876	E(LU)			0.04172006		
		4	-0.117175	-0.138383	E(CP)				0.08554362	
		5	-0.086906	-0.121647	E(LB)					
		6	1.677960	0.727829	18	11	1	-0.026669	-0.079582	
E(LU)			0.37044855				2	-0.022402	-0.082484	
E(CP)			0.17068152				3	-0.016466	-0.081896	
E(LB)			0.15414076				4	-0.009294	-0.079012	
							5	-0.000979	-0.074183	
18	7	1	-0.119793	-0.134044			6	0.008496	-0.067503	
		2	-0.112406	-0.135163			7	0.019212	-0.058930	
		3	-0.098738	-0.130098			8	0.031300	-0.048324	
		4	-0.080698	-0.120906			9	0.044947	-0.035451	
		5	-0.058807	-0.108183			10	0.060404	-0.019962	
		6	-0.033165	-0.092095			11	0.913459	0.627325	
		7	1.503605	0.720486	E(LU)			0.10556433		
E(LU)			0.26434202		E(CP)			0.02787638		
E(CP)			0.11983820		E(LB)				0.07601539	
E(LB)			0.12977806							
18	8	1	-0.084626	-0.115541	18	12	1	-0.015793	-0.071378	
		2	-0.078711	-0.117434			2	-0.011677	-0.074393	
		3	-0.062272	-0.114068			3	-0.006416	-0.074315	
		4	-0.054656	-0.107202			4	-0.002078	-0.072211	
		5	-0.038217	-0.097349			5	0.006695	-0.068395	
		6	-0.019006	-0.084645			6	0.014529	-0.062952	
		7	0.003084	-0.069031			7	0.023297	-0.055848	
		8	1.340405	0.705270			8	0.033110	-0.046959	
E(LU)			0.19807869				9	0.044122	-0.036073	
E(CP)			0.08497296				10	0.056540	-0.022877	
E(LB)			0.11143330				11	0.070637	-0.006924	
							12	0.785235	0.592326	
					E(LU)			0.09145851		
18	9	1	-0.059414	-0.101022	E(CP)			0.01723593		
		2	-0.054359	-0.103411	E(LB)			0.06798899		
		3	-0.046030	-0.101260						
		4	-0.035375	-0.096099	18	13	1	-0.007289	-0.064317	
		5	-0.022631	-0.088374			2	-0.003238	-0.067387	
		6	-0.007819	-0.078203			3	0.001550	-0.067701	
		7	0.009161	-0.065532			4	0.006940	-0.066218	
		8	0.028495	-0.050186			5	0.012925	-0.063222	
		9	1.187973	0.684067			6	0.019540	-0.058792	
E(LU)			0.15482946				7	0.026851	-0.052898	
E(CP)			0.06006815				8	0.034951	-0.045430	
E(LB)			0.09709201				9	0.043969	-0.036200	
					E(LU)			10	0.054072	-0.024926
					E(CP)			11	0.065486	-0.011201
					E(LB)			12	0.070516	0.055561
							13	0.685728	0.552731	
								0.05146655		
								0.00893995		
								0.06110111		

TABLE OF WEIGHTS (CONTINUED)

N	M	I	A(N,M,I)	C(N,M,I)	N	M	I	A(N,M,I)	C(N,M,I)
18	14	1	-0.000568	-0.058133	18	17	1	0.012444	-0.042879
		2	0.003471	-0.061213			2	0.016611	-0.045800
		3	0.007930	-0.061830			3	0.020593	-0.046965
		4	0.012775	-0.060849			4	0.024555	-0.047008
		5	0.018027	-0.058527			5	0.028573	-0.046121
		6	0.023730	-0.054936			6	0.032702	-0.044362
		7	0.029942	-0.050053			7	0.036930	-0.041722
		8	0.036744	-0.043781			8	0.041487	-0.038137
		9	0.044239	-0.035952			9	0.046252	-0.033494
		10	0.052564	-0.026314			10	0.051355	-0.027618
		11	0.061904	-0.014497			11	0.056889	-0.020248
		12	0.072509	0.003034			12	0.062980	-0.010994
		13	0.084730	0.018080			13	0.069810	0.000742
		14	0.552004	0.507970			14	0.077655	0.615937
E(LU)			0.07436294				15	0.086979	0.036313
E(CP)			0.00240300				16	0.098636	0.065331
E(LB)			0.05508562				17	0.235490	0.327023
					E(LU)				0.06346845
18	15	1	0.004780	-0.052617	E(CP)				-0.01018489
		2	0.008843	-0.055674	E(LB)				0.04033369
		3	0.013074	-0.056526					
		4	0.017522	-0.055953	18	18	1	0.015092	-0.038165
		5	0.022232	-0.054191			2	0.019328	-0.040965
		6	0.027249	-0.051307			3	0.023258	-0.042221
		7	0.032630	-0.047281			4	0.027089	-0.042497
		8	0.038443	-0.042029			5	0.030909	-0.041963
		9	0.044772	-0.035403			6	0.034773	-0.040676
		10	0.051728	-0.027176			7	0.038128	-0.038627
		11	0.059460	-0.017018			8	0.042820	-0.035765
		12	0.068169	-0.004442			9	0.047095	-0.031992
		13	0.078145	0.011289			10	0.051612	-0.027160
		14	0.089813	0.031340			11	0.056443	-0.021041
		15	0.443142	0.456986			12	0.061685	-0.013300
E(LU)			0.06933298				13	0.067477	-0.003410
E(CP)			-0.00278409				14	0.074032	0.009488
E(LB)			0.04973648				15	0.081713	0.026940
							16	0.091221	0.052132
18	16	1	0.009048	-0.047594			17	0.104314	0.093529
		2	0.013157	-0.050597			18	0.132411	0.235693
		3	0.017235	-0.051629	E(LU)				0.06204005
		4	0.021397	-0.051393	E(CP)				-0.01272745
		5	0.025706	-0.050102	E(LB)				0.03580789
		6	0.030212	-0.047820					
		7	0.034966	-0.044532	19	2	1	-1.223869	-0.493292
		8	0.040027	-0.040165			2	2.223669	0.493292
		9	0.045465	-0.034587	E(LU)				3.74782267
		10	0.051368	-0.027599	E(CP)				1.23712437
		11	0.057055	-0.018906	E(LB)				0.49325215
		12	0.061067	-0.008069					
		13	0.073294	0.005581	19	3	1	-0.643657	-0.327238
		14	0.082827	0.023119			2	-0.601169	-0.315224
		15	0.094248	0.046408			3	2.244827	0.642462
		16	0.338109	0.397887	E(LU)				1.68432765
E(LU)			0.06582537		E(CP)				0.64655945
E(CP)			-0.00691185		E(LB)				0.32423438
E(LB)			0.04487895						
					19	4	1	-0.394294	-0.243540
						2	-0.371431	-0.238113	
						3	-0.329685	-0.221662	
						4	2.095409	0.703314	
					E(LU)				0.93343886
					E(CP)				0.39452713
					E(LB)				0.23964110

TABLE OF WEIGHTS (CONTINUED)

N	M	I	A(N,M,I)	C(N,M,I)	N	M	I	A(N,M,I)	C(N,M,I)
19	5	1	-0.261237	-0.192958	19	10	1	-0.047007	-0.090004
		2	-0.247259	-0.190909			2	-0.042865	-0.092551
		3	-0.220739	-0.180245			3	-0.036265	-0.091324
		4	-0.185724	-0.163869			4	-0.027929	-0.087629
		5	1.914959	0.727980			5	-0.018045	-0.081863
E(LU)			0.58171310				6	-0.006641	-0.074147
E(CP)			0.26081700				7	0.006343	-0.064468
E(LB)			0.18861059				8	0.021029	-0.052718
							9	0.037595	-0.038703
19	6	1	-0.180964	-0.159004			10	1.117786	0.673407
		2	-0.171530	-0.158877	E(LU)			0.13159684	
		3	-0.153365	-0.151748	E(CP)			0.04766707	
		4	-0.129250	-0.139981	E(LB)			0.08643819	
		5	-0.100003	-0.124297					
		6	1.735111	0.733908	19	11	1	-0.032345	-0.080360
E(LU)			0.39192137				2	-0.028492	-0.083097
E(CP)			0.18053993				3	-0.022852	-0.082502
E(LB)			0.15435543				4	-0.015928	-0.079736
							5	-0.007843	-0.075152
19	7	1	-0.128533	-0.134583			6	0.001395	-0.068861
		2	-0.121602	-0.135622			7	0.011842	-0.06C851
		3	-0.108414	-0.130811			8	0.023603	-0.051025
		4	-0.090935	-0.122136			9	0.036827	-0.039209
		5	-0.069730	-0.110797			10	0.051716	-0.025147
		6	-0.044949	-0.095185			11	0.982076	0.645940
		7	1.564162	0.728535	E(LU)			0.10969257	
E(LU)			0.27982455		E(CP)			0.03326000	
E(CP)			0.12832890		E(LB)			0.07696225	
E(LB)			0.13053726						
					19	12	1	-0.020995	-0.072230
19	8	1	-0.092336	-0.116135			2	-0.017298	-0.075078
		2	-0.086846	-0.117908			3	-0.012331	-0.074965
		3	-0.076795	-0.114696			4	-0.006425	-0.072929
		4	-0.063593	-0.108201			5	0.000344	-0.069288
		5	-0.047637	-0.098937			6	0.007984	-0.064141
		6	-0.029016	-0.087065			7	0.016548	-0.057480
		7	-0.007670	-0.072570			8	0.026124	-0.049218
		8	1.403893	0.715513			9	0.036839	-0.039200
E(LU)			0.20936888				10	0.048859	-0.027194
E(CP)			0.09242024				11	0.062404	-0.012872
E(LB)			0.11223593				12	0.857947	0.614595
					E(LU)			0.09416748	
19	9	1	-0.066309	-0.101674	E(CP)			0.02213853	
		2	-0.061667	-0.103918	E(LB)			0.06899532	
		3	-0.053675	-0.101850					
		4	-0.043347	-0.096952	19	13	1	-0.012077	-0.065253
		5	-0.030960	-0.089671			2	-0.008453	-0.068158
		6	-0.016565	-0.080147			3	-0.003960	-0.068416
		7	-0.000103	-0.068365			4	0.001201	-0.066962
		8	0.018570	-0.054204			5	0.006996	-0.064084
		9	1.254056	0.696782			6	0.013442	-0.056872
E(LU)			0.16305851				7	0.020588	-0.054320
E(CP)			0.06668914				8	0.028511	-0.047351
E(LB)			0.09793914				9	0.037316	-0.038827
							10	0.047141	-0.028538
							11	0.058169	-0.016185
							12	0.070640	-0.001353
							13	0.740487	0.579318
					E(LU)			0.08302831	
					E(CP)			0.01342381	
					E(LB)			0.06217738	

TABLE OF WEIGHTS (CONTINUED)

N	M	I	A(N,M,I)	C(N,M,I)	N	M	I	A(N,M,I)	C(N,M,I)
19	14	1	-0.004989	-0.059169	19	17	1	0.008968	-0.044464
		2	-0.001384	-0.062091			2	0.012677	-0.047270
		3	0.002773	-0.062636			3	0.016326	-0.048344
		4	0.007387	-0.061652			4	0.020023	-0.048319
		5	0.012453	-0.059399			5	0.023825	-0.047390
		6	0.017997	-0.055961			6	0.027772	-0.045626
		7	0.024066	-0.051334			7	0.031106	-0.043028
		8	0.030726	-0.045450			8	0.036272	-0.039552
		9	0.038064	-0.038185			9	0.040920	-0.035112
		10	0.046194	-0.029351			10	0.045913	-0.029573
		11	0.055267	-0.018676			11	0.051331	-0.022740
		12	0.065482	-0.005781			12	0.057280	-0.014330
		13	0.077109	0.009882			13	0.063906	-0.003928
		14	0.628854	0.539802			14	0.071419	0.009098
E(LU)			C.07498023				15	0.080136	0.025759
E(CP)			0.00651543				16	0.090563	0.047806
E(LB)			0.05624730				17	0.320763	0.387016
					E(LU)			0.06200679	
					E(CP)			-0.00702291	
					E(LB)				0.04198714
19	15	1	0.000692	-0.053779			19	18	1
		2	0.004313	-0.056686				2	0.011941
		3	0.008234	-0.057456				3	-0.040244
		4	0.012444	-0.056855				2	0.015709
		5	0.016963	-0.055121				3	-0.042966
		6	0.021823	-0.052332				4	0.019289
		7	0.027068	-0.048486				5	-0.044136
		8	0.032757	-0.043523				6	0.022835
		9	0.038961	-0.037334				5	-0.044327
		10	0.045774	-0.029749				6	0.026412
		11	0.053320	-0.020523				7	-0.043716
		12	0.061762	-0.009310				8	0.030068
		13	0.071323	0.004394				7	-0.042366
		14	0.082316	0.021334				8	0.032841
		15	0.522250	0.495426				8	-0.040281
E(LU)			0.06915784				9	0.037772	
E(CP)			0.00099208				10	-0.037423	
E(LB)			0.05100764				11	0.041903	
							10	-0.033716	
							11	0.046286	
							12	-0.029044	
							11	0.050984	
							12	-0.023232	
							12	0.056983	
							13	-0.016030	
							13	0.061695	
							14	-0.007067	
							14	0.067989	
							15	0.004227	
							15	0.075216	
							16	0.018774	
							16	0.083802	
							17	0.038205	
							17	0.094526	
							18	0.065788	
					F(LU)				
					E(CP)				
					E(LB)				
								0.317554	
								0.05998848	
								-0.00988868	
								0.03791809	
19	16	1	0.005271	-0.043924					
		2	0.008929	-0.051792					
		3	0.012687	-0.052735					
		4	0.016601	-0.052449					
		5	0.020708	-0.051151					
		6	0.025048	-0.048913					
		7	0.029663	-0.045735					
		8	0.034603	-0.041566					
		9	0.039929	-0.036308					
		10	0.045717	-0.029809					
		11	0.052068	-0.021870					
		12	0.059114	-0.012148					
		13	0.067036	-0.000151					
		14	0.076094	0.014738					
		15	0.086669	0.033642					
		16	0.419861	0.445119					
E(LU)			0.06496979						
E(CP)			-0.00344791						
E(LB)			0.04630055						

TABLE OF WEIGHTS (CONTINUED)

N	M	I	A(N,M,I)	C(N,M,I)	N	M	I	A(N,M,I)	C(N,M,I)
19	19	1	0.014282	-0.035995	20	7	1	-0.136790	-0.135060
		2	0.918115	-0.038600			2	-0.130264	-0.136029
		3	0.021661	-0.039833			3	-0.117518	-0.131448
		4	0.025107	-0.040204			4	-0.100561	-0.123220
		5	0.028531	-0.039873			5	-0.079995	-0.111990
		6	0.031980	-0.038897			6	-0.056007	-0.097918
		7	0.035494	-0.037282			7	1.621135	0.735681
		8	0.039109	-0.034997	E(LU)			0.29539488	
		9	0.042861	-0.031977	E(CP)			0.13637533	
		10	0.046794	-0.028121	E(LB)			0.13121241	
		11	0.050958	-0.023280					
		12	0.055419	-0.017234	20	8	1	-0.099621	-0.116659
		13	0.060267	-0.009660			2	-0.094504	-0.118326
		14	0.065629	-0.000055			3	-0.084808	-0.115255
		15	0.071704	0.012400			4	-0.071993	-0.109093
		16	0.078826	0.079177			5	-0.056488	-0.109352
		17	0.087648	0.053305			6	-0.038416	-0.089210
		18	0.099799	0.092832			7	-0.017755	-0.075681
		19	0.125817	0.228292			8	1.463535	0.724575
		E(LU)	0.05874886		E(LU)			0.22087332	
		E(CP)	-0.01213794		E(CP)			0.09940206	
		E(LB)	0.03383684		E(LB)			0.11294771	
20	2	1	-1.251068	-0.493634	20	9	1	-0.072826	-0.102246
		2	2.251068	0.493634			2	-0.068544	-0.104362
		E(LU)	3.88005370				3	-0.060858	-0.102371
		E(CP)	1.26365389				4	-0.050834	-0.097711
		E(LB)	0.49359782				5	-0.038781	-0.090828
							6	-0.024779	-0.081874
20	3	1	-0.662014	-0.327555			7	-0.008798	-0.070863
		2	-0.621129	-0.316157			8	0.009270	-0.057714
		3	2.263164	0.643713			9	1.316151	0.707969
		E(LU)	1.75538518		E(LU)			0.17159045	
		E(CP)	0.66462201		E(CP)			0.07297238	
		E(LB)	0.32470597		E(LB)			0.09868793	
20	4	1	-0.408252	-0.243885	20	10	1	-0.052900	-0.090626
		2	-0.386289	-0.238726			2	-0.049115	-0.093031
		3	-0.345972	-0.223154			3	-0.042792	-0.091837
		4	2.140513	0.705766			4	-0.034710	-0.088309
		E(LU)	0.97791855				5	-0.025087	-0.082842
		E(CP)	0.40827717				6	-0.013973	-0.075573
		E(LB)	0.24018443				7	-0.001335	-0.066511
							8	0.012921	-0.055584
20	5	1	-0.272551	-0.193344			9	0.028939	-0.042651
		2	-0.259179	-0.191385			10	1.178052	0.686964
		3	-0.233536	-0.181278	E(LU)			0.13788300	
		4	-0.199675	-0.165821	E(CP)			0.05331635	
		5	1.964941	0.731828	E(LB)			0.08722579	
		E(LU)	0.61184794						
		E(CP)	0.27193675		20	11	1	-0.037716	-0.081036
		E(LB)	0.18940540				2	-0.034222	-0.083625
							3	-0.028845	-0.083028
20	6	1	-0.190502	-0.159435			4	-0.022146	-0.080373
		2	-0.181539	-0.159298			5	-0.014276	-0.076014
		3	-0.163969	-0.152528			6	-0.005262	-0.070070
		4	-0.140605	-0.141408			7	0.004930	-0.062554
		5	-0.112303	-0.126651			8	0.016382	-0.053398
		6	1.788917	0.739321			9	0.029216	-0.042476
		E(LU)	0.41329354				10	0.043593	-0.029594
		E(CP)	0.18987852				11	1.048347	0.662168
		E(LB)	0.15549251	E(LU)				0.11423656	
				E(CP)				0.03838053	
				E(LB)				0.07779186	

TABLE OF WEIGHTS (CONTINUED)

N	M	I	A(N,M,I)	C(N,M,I)	N	M	I	A(N,M,I)	C(N,M,I)
20	12	1	-0.025922	-0.072964	20	15	1	-0.003203	-0.054744
		2	-0.022589	-0.075662			2	0.001035	-0.057513
		3	-0.017879	-0.075522			3	0.003690	-0.051213
		4	-0.012183	-0.073554			4	0.007695	-0.057596
		5	-0.005600	-0.070076			5	0.012048	-0.055899
		6	0.001858	-0.065197			6	0.016769	-0.053209
		7	0.010227	-0.058928			7	0.021892	-0.049537
		8	0.019578	-0.051213			8	0.027467	-0.044842
		9	0.030012	-0.041931			9	0.033552	-0.039043
		10	0.041668	-0.030912			10	0.040230	-0.032016
		11	0.054724	-0.017911			11	0.047602	-0.023580
		12	0.926107	0.633868			12	0.055804	-0.013436
E(LU)			0.09732994				13	0.065012	-0.001280
E(CP)			0.02680890				14	0.075467	0.013416
E(LB)			0.06987174				15	0.595940	0.527466
				E(LU)				0.06951916	
20	13	1	-0.016619	-0.066052	E(LU)				
		2	-0.013364	-0.068809	E(CP)			0.00461910	
		3	-0.009129	-0.069021	E(LB)			0.05207861	
		4	-0.004170	-0.067601	20	16	1	0.001656	-0.050002
		5	0.001453	-0.064835			2	0.004926	-0.052742
		6	0.007742	-0.060825			3	0.008410	-0.053608
		7	0.014732	-0.055581			4	0.012111	-0.053287
		8	0.022485	-0.049051			5	0.016048	-0.051997
		9	0.031087	-0.041132			6	0.020247	-0.049816
		10	0.040654	-0.031666			7	0.024742	-0.046757
		11	0.051333	-0.020429			8	0.029575	-0.042785
		12	0.063321	-0.007116			9	0.034801	-0.037825
		13	0.810474	0.602120			10	0.040482	-0.031763
E(LU)			0.08507430				11	0.046707	-0.024432
E(C.)			0.01770390				12	0.053585	-0.015601
E(LB)			0.06310742				13	0.061262	-0.004939
				E(LU)			14	0.069938	0.008023
20	14	1	-0.009191	-0.060043			15	0.079893	0.023984
		2	-0.005961	-0.062821			16	0.495616	0.483548
		3	-0.002065	-0.063307	E(LU)			0.06467887	
		4	0.002348	-0.062329	E(CP)			-0.00010333	
		5	0.007248	-0.060148	E(LB)			0.04747114	
		6	0.012649	-0.056856					
		7	0.018585	-0.052465	20	17	1	0.005617	-0.045695
		8	0.025109	-0.046929			2	0.008931	-0.048385
		9	0.032297	-0.040154			3	0.012297	-0.049380
		10	0.040241	-0.031999			4	0.015773	-0.049304
		11	0.049069	-0.022261			5	0.019394	-0.048357
		12	0.058941	-0.010659			6	0.023192	-0.046613
		13	0.070069	0.003196			7	0.027201	-0.044083
		14	0.700660	0.566775			8	0.031459	-0.040736
E(LU)			0.07610847				9	0.036010	-0.036510
E(CP)			0.01045130				10	0.040910	-0.031298
E(LB)			0.05724068				11	0.046228	-0.024954
				E(LU)			12	0.052055	-0.017265
				E(CP)			13	0.058509	-0.007934
				E(LB)			14	0.065756	0.003474
							15	0.074029	0.017606
							16	0.083671	0.035466
							17	0.398968	0.433947
								0.06114864	
								-0.00394307	
								0.04329477	

TABLE OF WEIGHTS (CONTINUED)

N	M	I	A(N,M,I)	C(N,M,I)	N	M	I	A(N,M,I)	C(N,M,I)
20	18	1	0.008847	-0.041706	20	20	1	0.013553	-0.034055
		2	0.012215	-0.044331			2	0.017039	-0.036484
		3	0.015502	-0.045422			3	0.020257	-0.037686
		4	0.018813	-0.045550			4	0.023376	-0.038123
		5	0.022197	-0.044896			5	0.026464	-0.037945
		6	0.025690	-0.043529			6	0.029565	-0.037211
		7	0.029324	-0.041460			7	0.032711	-0.035932
		8	0.033133	-0.038646			8	0.035932	-0.034091
		9	0.037162	-0.035086			9	0.039258	-0.031646
		10	0.041450	-0.030632			10	0.042720	-0.028527
		11	0.046055	-0.025168			11	0.046357	-0.024632
		12	0.051050	-0.018506			12	0.050215	-0.019814
		13	0.056532	-0.010374			13	0.054354	-0.013260
		14	0.062634	-0.000381			14	0.058856	-0.006460
		15	0.069547	0.012071			15	0.063842	0.002864
		16	0.077558	0.027938			16	0.069496	0.014902
		17	0.087131	0.048871			17	0.076128	0.031052
		18	0.305157	0.376826			18	0.084346	0.054203
		E(LU)	0.6 0.1867				19	0.095649	0.092028
		E(CP)	-0.00706723				20	0.119862	0.221415
		E(LB)	0.03943688		E(LU)			0.05578958	
					E(CP)			-0.01159947	
					E(LB)			0.03207039	
20	19	1	0.011469	-0.037905					
		2	0.014895	-0.040446					
		3	0.018135	-0.041607	21	2	1	-1.276880	-0.493942
		4	0.021329	-0.041903			2	2.276880	0.493942
		5	0.024538	-0.041503	E(LU)			4.00827646	
		6	0.027802	-0.040467	E(CP)			1.28886132	
		7	0.031153	-0.038810	E(LB)			0.49390979	
		8	0.034624	-0.036509					
		9	0.038247	-0.035514	21	3	1	-0.679427	-0.327841
		10	0.042061	-0.029746			2	-0.6 0.0016	-0.316999
		11	0.046112	-0.025085			3	2.319443	0.644841
		12	0.050458	-0.019364	E(LU)			1.82463798	
		13	0.055176	-0.012340	E(CP)			0.68177635	
		14	0.060372	-0.003540	E(LB)			0.32513088	
		15	0.066198	0.007217					
		16	0.272887	0.021167	21	4	1	-0.421487	-0.244196
		17	0.080830	0.039737			2	-0.400349	-0.239279
		18	0.090746	0.066024			3	-0.361352	-0.224498
		19	0.212971	0.308714			4	2.183188	0.707973
		E(LU)	0.05687410		E(LU)			1.02150585	
		E(CP)	-0.00959610		E(CP)			0.42133361	
		E(LB)	0.03577112		E(LB)			0.24067351	
					21	5	1	-0.283275	-0.193691
						2	-0.270454	-0.191814	
						3	-0.245624	-0.182209	
						4	-0.212831	-0.167572	
						5	2.012185	0.735285	
					E(LU)			0.64156176	
					E(CP)			0.28249590	
					E(LB)			0.18993997	
					21	6	1	-0.199541	-0.159820
						2	-0.191002	-0.159675	
						3	-0.173984	-0.153231	
						4	-0.151319	-0.142690	
						5	-0.123892	-0.128756	
						6	1.839738	0.744172	
					E(LU)			0.43452074	
					E(CP)			0.19874861	
					E(LB)			0.15606403	

TABLE OF WEIGHTS (CONTINUED)

N	M	I	A(N,M,I)	C(N,M,I)	N	M	I	A(N,M,I)	C(N,M,I)	
21	7	1	-0.144615	-0.135485	21	12	1	-0.030601	-0.073604	
	2	-0.138450	-0.136392			2	-0.027584	-0.076167		
	3	-0.126112	-0.132021			3	-0.023103	-0.076006		
	4	-0.109643	-0.124225			4	-0.017596	-0.074104		
	5	-0.089672	-0.113595			5	-0.011187	-0.070777		
	6	-0.066419	-0.100351			6	-0.003901	-0.066142		
E(LU)	7	1.674911	0.742070			7	0.004282	-0.060223		
E(CP)		0.31099565				8	0.013418	-0.052983		
E(LB)		0.14402019				9	0.023589	-0.044337		
		0.13181685				10	0.034909	-0.034153		
21	8	1	-0.106524	-0.117124			11	0.047525	-0.022243	
	2	-0.101739	-0.118696		E(LU)	12	0.990248	0.650738		
	3	-0.092368	-0.115755		E(CP)		0.10086432			
	4	-0.079914	-0.109895		E(LB)		0.03126495			
	5	-0.064832	-0.101621				0.07064304			
	6	-0.047274	-0.091123		21	13	1	-0.020936	-0.066744	
	7	-0.027245	-0.078439			2	-0.018002	-0.069367		
E(LU)	8	1.519896	0.73..652			3	-0.013994	-0.069541		
E(CP)		0.23252621				4	-0.009216	-0.069156		
E(LB)		0.10619473				5	-0.003750	-0.055499		
		0.11358345				6	0.002392	-0.061675		
21	9	1	-0.079003	-0.102752			7	0.009234	-0.056708	
	2	-0.075039	-0.104752			8	0.016823	-0.050566		
	3	-0.067630	-0.102836			9	0.025231	-0.043172		
	4	-0.057890	-0.098393			10	0.034555	-0.034404		
	5	-0.046151	-0.091865			11	0.044917	-0.024094		
	6	-0.032519	-0.083417			12	0.056476	-0.012009		
	7	-0.016987	-0.073081	E(LU)		13	0.076270	0.621934		
	8	0.000523	-0.060807	E(CP)			0.08752028			
E(LU)	9	1.374696	0.717905	E(LB)			0.02179399			
E(CP)		0.18035373					0.06392100			
E(LB)		0.07894880			21	14	1	-0.013190	-0.060794	
		0.09935486				2	-0.010287	-0.063440		
21	10	1	-0.058485	-0.091174			3	-0.005618	-0.063875	
	2	-0.055015	0.03453			4	-0.002385	-0.062909		
	3	-0.048942	-0.092291			5	0.002367	-0.060800		
	4	-0.041036	-0.088916			6	0.007636	-0.057647		
	5	-0.031718	-0.083721			7	0.013446	-0.053473		
	6	-0.020880	-0.076849			8	0.019842	-0.048247		
	7	-0.016567	-0.068330			9	0.026883	-0.041903		
	8	0.005230	-0.058118			10	0.034651	-0.034330		
	9	0.020804	-0.046107			11	0.043251	-0.025373		
E(LU)	10	1.238610	0.698958			12	0.052814	-0.014822		
E(CP)		0.14446082				13	0.063513	-0.002388		
E(LB)		0.05869415		E(LU)		14	0.768077	0.590001		
		0.08792500		E(CP)			0.07766021			
				E(LB)			0.01421994			
21	11	1	-0.042812	-0.081628				0.05810297		
	2	-0.039631	-0.084084							
	3	-0.034490	-0.083419							
	4	-0.027998	.080939							
	5	-0.020328	-0.076784							
	6	-0.011527	-0.071153							
	7	-0.001577	-0.064073							
	8	0.009585	-0.055502							
	9	0.022055	-0.045346							
	10	0.035968	-0.033457							
	11	1.110755	0.676455							
E(LU)		0.11911746								
E(CP)		0.04325992								
E(LB)		0.07852549								

TABLE OF WEIGHTS (CONTINUED)

N	M	I	A(N,M,I)	C(N,M,I)	N	M	I	A(N,M,I)	C(N,M,I)
21	15	1	-C.006919	-0.055563	21	18	1	0.005853	-0.042848
		2	-0.004012	-0.058205			2	0.000874	-0.045374
		3	-0.000589	-0.058845			3	0.011911	-0.046394
		4	0.003237	-0.058219			4	0.015024	-0.046474
		5	0.007443	-0.056566			5	0.018245	-0.045796
		6	0.012039	-0.053974			6	0.021603	-0.044433
		7	0.01707	-0.050466			7	0.02517	-0.042403
		8	0.021516	-0.046017			8	0.028836	-0.049694
		9	0.02137	-0.040565			9	0.032780	-0.036255
		10	0.03135	-0.034010			10	0.036985	-0.032027
		11	0.041242	-0.026215			11	0.041512	-0.026894
		12	0.050225	-0.016982			12	0.046418	-0.020718
		13	0.059124	-0.006049			13	0.051789	-0.013292
		14	0.069130	0.006947			14	0.057729	-0.004339
		15	0.664991	0.554729			15	0.064392	0.006557
E(LU)			0.07032505				16	0.071987	0.020003
E(CP)			0.00810102				17	0.080826	0.036967
E(LB)			0.05299863				18	0.380111	0.423414
					E(LU)				0.05777143
21	16	1	-0.001802	-0.050903	E(CP)				-0.00431152
		2	0.001131	-0.053522	E(LB)				0.04064434
		3	0.004378	-0.054323					
		4	0.007896	-0.053977	21	19	1	0.008698	-0.039258
		5	0.011684	-0.052704			2	0.011772	-0.041717
		6	0.015759	-0.050587			3	0.014753	-0.042808
		7	0.020147	-0.047646			4	0.017739	-0.043048
		8	0.024883	-0.043862			5	0.020774	-0.042605
		9	0.030017	-0.039172			6	0.023891	-0.041546
		10	0.035594	-0.033501			7	0.027116	-0.039889
		11	0.041700	-0.026708			8	0.030478	-0.037622
		12	0.048420	-0.018625			9	0.034006	-0.034708
		13	0.055879	-0.009004			10	0.037735	-0.031080
		14	0.064233	0.002489			11	0.041797	-0.026648
		15	0.073691	0.016331			12	0.045971	-0.021282
		16	0.566382	0.515715			13	0.050597	-0.014797
E(LU)			0.06485329				14	0.055671	-0.006936
E(CP)			0.00311876				15	0.061314	0.002673
E(LB)			0.04846207				16	0.067704	0.014599
							17	0.075101	0.029744
21	17	1	C.002397	-0.046698			18	0.083931	0.049671
		2	0.005370	-0.049278			19	0.291040	0.367257
		3	0.008493	-0.050203	E(LU)				0.05559063
		4	0.011778	-0.050089	E(CP)				-0.00706342
		5	0.015245	-0.049137	E(LB)				0.03717178
		6	0.018916	-0.047426					
		7	0.022818	-0.044972					
		8	0.026981	-0.041760					
		9	0.031445	-0.037741					
		10	0.036263	-0.032831					
		11	0.041487	-0.026922					
		12	0.047201	-0.019846					
		13	0.053501	-0.011386					
		14	0.060520	-0.001230					
		15	0.068439	0.011065					
		16	0.077509	0.026154					
		17	0.471636	0.472299					
E(LU)			0.06077952						
E(CP)			-0.00096075						
E(LB)			0.04437683						

TABLE OF WEIGHTS (CONTINUED)

N	M	I	A(N,M,I)	C(N,M,I)	N	M	I	A(N,M,I)	C(N,M,I)	
21	20	1	0.011028	-0.035816	22	4	1	-0.434070	-0.244476	
		2	0.014157	-0.038193			2	-0.413490	-0.239780	
		3	0.017105	-0.039333			3	-0.375918	-0.225713	
		4	0.020000	-0.039706			4	2.223678	0.709969	
		5	0.022898	-0.039466	E(LU)			1.06422125		
		6	0.025833	-0.038676	E(CP)			0.43376212		
		7	0.028833	-0.037352	E(LB)			0.24111609		
		8	0.031923	-0.035486						
		9	0.035133	-0.033042	22	5	1	-0.293467	-0.194003	
		10	0.038489	-0.029966			2	-0.281150	-0.192202	
		11	0.042026	-0.026176			3	-0.257076	-0.183051	
		12	0.045787	-0.021555			4	-0.225276	-0.169152	
		13	0.049824	-0.015938	E(LU)		5	2.056969	0.738407	
		14	0.054209	-0.009097	E(CP)			0.67084108		
		15	0.059038	-0.000691	E(LB)			0.29254724		
		16	0.064453	0.009794				0.19042304		
		17	0.070670	0.023194						
		18	0.078048	0.040976	22	6	1	-0.208130	-0.160166	
		19	0.087254	0.066087			2	-0.199975	-0.160015	
		20	0.203293	0.300441			3	-0.183470	-0.153867	
		E(LU)	0.05407008				4	-0.161458	-0.143848	
		E(CP)	-0.00931060				5	-0.134845	-0.130649	
		E(LB)	0.03385072				6	1.887878	0.748545	
	21	1	0.012894	-0.032310	E(LU)			0.45557038		
		2	0.016080	-0.034581	E(CP)			0.20719220		
		3	0.019015	-0.035746	E(LB)			0.15657969		
		4	0.021851	-0.036228	22	7	1	-0.152049	-0.135866	
		5	0.024653	-0.036168			2	-0.146209	-0.136718	
		6	0.027458	-0.035622			3	-0.134250	-0.132539	
		7	0.030295	-0.034606			4	-0.118236	-0.125119	
		8	0.033186	-0.031114	E(LU)		5	-0.098823	-0.115041	
		9	0.036159	-0.031116	E(CP)			6	-0.076253	-0.102533
		10	0.039235	-0.028564	E(LB)			7	1.725817	0.747815
		11	0.042446	-0.025388				0.32658258		
		12	0.045824	-0.021484				0.15130047		
		13	0.049414	-0.016709				0.13236123		
		14	0.053270	-0.010860						
		15	0.057470	-0.003637	22	8	1	-0.113082	-0.117539	
		16	0.062124	0.005419			2	-0.108593	-0.119026	
		17	0.067404	0.017060			3	-0.099523	-0.116206	
		18	0.073603	0.032626			4	-0.087407	-0.110619	
		19	0.081287	0.054878			5	-0.072723	-0.102765	
		20	0.091876	0.091146			6	-0.055645	-0.092840	
		21	0.114456	0.215004			7	-0.036204	-0.080900	
		E(LU)	0.05311439				8	1.513176	0.739897	
		E(CP)	-0.01110585					0.24427569		
		E(LB)	0.03047836		E(LU)			0.11258985		
	22	2	1	-1.301440	-0.494222	E(CP)			0.11415483	
		2	2.301440	0.494222	E(LB)					
		E(LU)	4.13275081		22	9	1	-0.084872	-0.103202	
		E(CP)	1.31287156				2	-0.081190	-0.105100	
		E(LB)	0.49419277				3	-0.074036	-0.103253	
							4	-0.064360	-0.099008	
	22	3	1	-0.695987	-0.328100					
		2	-0.657336	-0.317763				5	-0.053119	-0.092802
		3	2.35223	0.645863				6	-0.039835	-0.084805
		E(LU)	1.89217469					7	-0.024723	-0.075066
		E(CP)	0.69810867					8	-0.007729	-0.063556
		E(LB)	0.32551588					9	1.43063	0.726792
					E(LU)			0.18029138		
					E(CP)			0.08464553		
					E(LB)			0.09995287		

TABLE OF WEIGHTS (CONTINUED)

N	M	I	A(N,M,I)	C(N,M,I)	N	M	I	A(N,M,I)	C(N,M,I)
22	10	1	-0.063797	-0.091660	22	14	1	-0.017003	-0.061447
		2	-0.060601	-0.093825			2	-0.014385	-0.063972
		3	-0.054757	-0.092695			3	-0.010918	-0.064365
		4	-0.047129	-0.089463			4	-0.006845	-0.063413
		5	-0.037983	-0.084513			5	-0.002229	-0.061375
		6	-0.027405	-0.077998			6	0.002917	-0.058353
		7	-0.015399	-0.069960			7	0.008610	-0.054776
		8	-0.001917	-0.060373			8	0.014879	-0.049432
		9	0.013133	-0.049161			9	0.021782	-0.043466
		10	1.295854	0.709648			10	0.029381	-0.036397
			E(LU)	0.15126968			11	0.037767	-0.028103
			E(CP)	0.06382371			12	0.047049	-0.018422
			E(LB)	0.08855022			13	0.057369	-0.007137
							14	0.831624	0.610259
22	11	1	-0.047658	-0.082152	E(LU)			0.07956563	
		2	-0.044752	-0.084487	E(CP)			0.01783144	
		3	-0.039824	-0.083898	E(LB)			0.05886035	
		4	-0.033522	-0.081446					
		5	-0.026041	-0.077478	22	12	1	-0.010467	-0.056269
		6	-0.017442	-0.072129			2	-0.007849	-0.058795
		7	-0.007722	-0.065437			3	-0.004630	-0.059383
		8	0.003165	-0.057379			4	-0.000964	-0.058755
		9	0.015297	-0.047887			5	0.003111	-0.057145
		10	0.028784	-0.036846			6	0.007593	-0.054649
		11	1.169717	0.689139			7	0.012499	-0.051296
			E(LU)	0.12427189			8	0.017862	-0.047069
			E(CP)	0.04791797			9	0.023724	-0.041928
			E(LB)	0.07917935			10	0.030145	-0.035792
							11	0.037196	-0.028555
22	12	1	-0.035052	-0.074167					
		2	-0.032313	-0.076608	22	16	1	0.005110	-0.051672
		3	-0.028036	-0.076431			2	-0.002471	-0.054179
		4	-0.022704	-0.076593			3	0.000569	-0.054921
		5	-0.016456	-0.071406	E(LU)		4	0.003924	-0.054559
		6	-0.009333	-0.066992	E(CP)		5	0.007582	-0.053308
		7	-0.001327	-0.061386	E(LB)		6	0.011543	-0.051259
		8	0.007603	-0.054568			7	0.015838	-0.048429
		9	0.017525	-0.046475			8	0.020484	-0.044819
		10	0.028533	-0.037005	22	16	1	-0.005110	-0.051672
		11	0.040749	-0.026013			2	-0.002471	-0.054179
		12	1.050810	0.665643			3	0.000569	-0.054921
			E(LU)	0.10470500	E(LU)		4	0.003924	-0.054559
			E(CP)	0.03552320	E(CP)		5	0.007582	-0.053308
			E(LB)	0.07132781	E(LB)		6	0.011543	-0.051259
							7	0.015838	-0.048429
							8	0.020484	-0.044819
22	13	1	-0.025047	-0.067350					
		2	-0.022395	-0.069850	22	16	1	-0.005110	-0.051672
		3	-0.018588	-0.069993			2	-0.002471	-0.054179
		4	-0.013974	-0.068645			3	0.000569	-0.054921
		5	-0.008653	-0.065089	E(LU)		4	0.003924	-0.054559
		6	-0.002649	-0.062438	E(CP)		5	0.007582	-0.053308
		7	0.004050	-0.051227	E(LB)		6	0.011543	-0.051259
		8	0.011483	-0.051924			7	0.015838	-0.048429
		9	0.019706	-0.044839			8	0.020484	-0.044819
		10	0.028801	-0.036622	22	16	1	-0.005110	-0.051672
		11	0.038870	-0.027293			2	-0.002471	-0.054179
		12	0.050045	-0.016224			3	0.000569	-0.054921
		13	6.938350	0.639340			4	0.003924	-0.054559
			E(LU)	0.09029856	E(LU)		5	0.007582	-0.053308
			E(CP)	0.02570744	E(CP)		6	0.011543	-0.051259
			E(LB)	0.06463988	E(LB)		7	0.015838	-0.048429
							8	0.020484	-0.044819

TABLE OF WEIGHTS (CONTINUED)

N	M	I	A(N,M,I)	C(N,M,I)	N	M	I	A(N,M,I)	C(N,M,I)
22	17	1	-0.000692	-0.047541	22	19	1	0.006009	-0.040322
		2	0.001982	-0.050015			2	0.008777	-0.042695
		3	0.004893	-0.050879			3	0.011534	-0.043723
		4	0.008014	-0.050736			4	0.014342	-0.043917
		5	0.011345	-0.049789			5	0.017230	-0.043447
		6	0.014906	-0.048115			6	0.020225	-0.042380
		7	0.018711	-0.045743			7	0.023341	-0.040750
		8	0.022792	-0.042661			8	0.026624	-0.038526
		9	0.027167	-0.038846			9	0.030059	-0.035724
		10	0.031923	-0.034195			10	0.033736	-0.032232
		11	0.037042	-0.028684			11	0.037624	-0.028048
		12	0.042658	-0.022124			12	0.041834	-0.023C01
		13	0.048810	-0.014389			13	0.046370	-0.017006
		14	0.055631	-0.005227			14	0.051344	-0.0C9632
		15	0.063253	0.005668			15	0.056833	-0.001233
		16	0.071871	0.018749			16	0.062987	0.C09193
		17	0.539692	0.504527			17	0.069992	0.022017
E(LU)			0.06081663				18	0.078134	0.038155
E(CP)			0.00192009				19	0.363007	0.413471
E(LB)			0.04529672		E(LU)			0.05476281	
					E(CP)			-0.00458357	
					E(LB)				0.03829068
22	18	1	0.002969	-0.043785	22	20	1	0.008533	-0.037073
		2	0.005687	-0.046214			2	0.011352	-0.039379
		3	0.008507	-0.047171			3	0.014069	-0.040459
		4	0.011449	-0.047212			4	0.016778	-0.04C780
		5	0.014531	-0.046521			5	0.019519	-0.04C500
		6	0.017772	-0.045174			6	0.022321	-0.039681
		7	0.021193	-0.043196			7	0.025204	-0.038351
		8	0.024827	-0.040573			8	0.028200	-0.036496
		9	0.028687	-0.037286			9	0.031317	-0.034104
		10	0.032827	-0.033268			10	0.034600	-0.031120
		11	0.037279	-0.028441			11	0.036064	-0.027481
		12	0.042106	-0.022691			12	0.041759	-0.023097
		13	0.047371	-0.015865			13	0.045722	-0.017840
		14	0.053169	-0.007753			14	0.050022	-0.011535
		15	0.059619	0.001940			15	0.054736	-0.003933
		16	0.066884	0.013632			16	0.059977	0.005317
		17	0.075192	0.027940			17	0.065907	0.016757
		18	0.449933	0.461640			18	0.072766	0.031243
E(LU)			0.05735061				19	0.080947	0.050259
E(CP)			-0.00163612				20	0.278209	0.358253
E(LB)			0.04164798		E(LU)			0.05286705	
					E(CP)			-0.00702486	
					E(LB)				0.03514712

TABLE OF WEIGHTS (CONTINUED)

N	M	I	A(N,M,I)	C(N,M,I)	N	M	I	A(N,M,I)	C(N,M,I)
22	21	1	0.010614	-0.033940	23	4	1	-0.446061	-0.244730
		2	0.013486	-0.036167			2	-0.426381	-0.240237
		3	0.016181	-0.037280			3	-0.389748	-0.226817
		4	0.018819	-0.037707			4	2.262191	0.711785
		5	0.021451	-0.037592	E(LU)			1.10608938	
		6	0.024107	-0.036993	E(CP)			0.44561957	
		7	0.026810	-0.035935	E(LB)				0.24151852
		8	0.029588	-0.034409					
		9	0.032449	-0.032401	23	5	1	-0.303177	-0.194285
		10	0.035435	-0.029863			2	-0.291322	-0.192554
		11	0.038552	-0.026747			3	-0.267953	-0.183817
		12	0.041849	-0.022960			4	-0.237079	-0.170584
		13	0.045351	-0.018398			5	2.099531	0.741241
		14	0.049118	-0.012895	E(LU)			0.69967926	
		15	0.053206	-0.006235	E(CP)			0.30213653	
		16	0.057712	0.001909	E(LB)				0.19086173
		17	0.062764	0.012027					
		18	0.078562	0.024916	23	6	1	-0.216311	-0.160479
		19	0.075443	0.041976			2	-0.208505	-0.160324
		20	0.084022	0.065013			3	-0.192480	-0.154445
		21	0.194480	0.292681			4	-0.171078	-0.144898
		E(LU)	0.05153187				5	-0.145224	-0.132362
		E(CP)	-0.00903424				6	1.933598	0.752508
		E(LB)	0.03212313		E(LU)			0.47641869	
					E(CP)				0.21524910
					E(LB)				0.15704731
22	22	1	0.01	-0.030733					
		2	0.01	-0.032859					
		3	0.01	-0.033986	23	7	1	-0.159128	-0.136209
		4	0.020551	-0.034499			2	-0.153582	-0.137013
		5	0.023056	-0.034529			3	-0.141975	-0.133009
		6	0.025607	-0.034130			4	-0.126391	-0.125931
		7	0.028178	-0.033325			5	-0.107499	-0.116350
		8	0.030794	-0.032106			6	-0.085566	-0.104499
		9	0.033464	-0.030463			7	1.774142	0.753011
		10	0.036226	-0.028354	E(LU)			0.34212138	
		11	0.039082	-0.025735	E(CP)			0.15824839	
		12	0.042076	-0.022528	E(LB)				0.13285412
		13	0.045226	-0.018638					
		14	0.048580	-0.013922	23	8	1	-0.119329	-0.117912
		15	0.052185	-0.008184			2	-0.115104	-0.119324
		16	0.056116	-0.001137			3	-0.106313	-0.116615
		17	0.060475	0.007660			4	-0.094514	-0.111278
		18	0.065424	0.018928			5	-0.080205	-0.103803
		19	0.071237	0.033950			6	-0.063578	-0.094391
		20	0.078445	0.055370			7	-0.044683	-0.083112
		21	0.088381	0.090709			8	1.623725	0.746435
		22	0.109526	0.209011	E(LU)			0.25608069	
		E(LU)	0.05068421		E(CP)			0.11869505	
		E(CP)	-0.01065184		E(LB)				0.11467125
		E(LB)	0.02903621						
23	2	1	-1.324862	-0.494478					
		2	2.324862	0.494478	23	9	1	-0.090463	-0.103606
		E(LU)	4.25371176				2	-0.087031	-0.105411
		E(CP)	1.33579271				3	-0.080117	-0.103629
		E(LB)	0.49445062				4	-0.076117	-0.099566
							5	-0.059113	-0.093651
							6	-0.046768	-0.086060
							7	-0.032050	-0.076051
23	3	1	-0.711775	-0.328336			8	-0.015537	-0.066015
		2	-0.674982	-0.318458			9	1.482569	0.734790
		3	2.386757	0.646794	E(LU)			0.19835768	
		E(LU)	1.95807953		E(CP)			0.09008641	
		E(CP)	0.71369343		E(LB)				0.10049225
		E(LB)	0.32586633						

TABLE OF WEIGHTS (CONTINUED)

N	M	I	A(N,M,I)	C(N,M,I)	N	M	I	A(N,M,I)	C(N,M,I)
23	10	1	-0.068856	-0.092095	23	14	1	-0.020644	-0.062022
		2	-0.065905	-0.094156			2	-0.013278	-0.064436
		3	-0.060269	-0.093058			3	-0.014991	-0.064792
		4	-0.052846	-0.089957			4	-0.011061	-0.063857
		5	-0.043918	-0.085232			5	-0.006570	-0.061888
		6	-0.033587	-0.079038			6	-0.001537	-0.058966
		7	-0.021873	-0.071429			7	0.004039	-0.055193
		8	-0.008741	-0.062395			8	0.010191	-0.050500
		9	0.005880	-0.051880			9	0.016959	-0.04870
		10	1.350115	0.719241			10	0.024395	-0.038243
E(LU)			0.15826056				11	0.032581	-0.030518
E(CP)			0.06872565				12	0.041605	-0.021572
E(LB)			0.08911283				13	0.051586	-0.011236
23	11	1	-0.052275	-0.082619	E(LU)		14	0.891725	0.628112
		2	-0.049614	-0.084845	E(CP)			0.08176810	
		3	-0.044879	-0.084262	E(LB)			0.02129585	
		4	-0.038754	-0.081902				0.05953202	
		5	-0.031451	-0.078106	23	15	1	-0.013858	-0.056886
		6	-0.023044	-0.073012			2	-0.011496	-0.059304
		7	-0.013543	-0.066668			3	-0.009457	-0.059848
		8	-0.002916	-0.059066			4	-0.004935	-0.059221
		9	0.008899	-0.050154			5	-0.000978	-0.057655
		10	0.021994	-0.039847			6	0.003395	-0.055253
		11	1.225582	0.700481			7	0.008206	-0.052040
E(LU)			0.12964842				8	0.013472	-0.048017
E(CP)			0.05237239				9	0.019220	-0.043159
E(LB)			0.07976613				10	0.025528	-0.037385
23	12	1	-0.039296	-0.074667	E(LU)		11	0.032425	-0.030636
		2	-0.036802	-0.076996	E(CP)		12	0.040015	-0.022775
		3	-0.032710	-0.076807	E(LB)		13	0.048387	-0.013657
		4	-0.027537	-0.075031			14	0.057669	-0.003074
		5	-0.021461	-0.071973	23	16	1	-0.008277	-0.052337
		6	-0.014473	-0.067761	E(LU)		2	-0.005899	-0.054740
		7	-0.006638	-0.062438	E(CP)		3	-0.003041	-0.055433
		8	0.002097	-0.055995	E(LB)		4	0.000172	-0.055058
		9	0.011784	-0.048387			5	0.003709	-0.053835
		10	0.022502	-0.039535			6	0.007575	-0.051846
		11	0.034352	-0.029328			7	0.011777	-0.049129
		12	1.108163	0.678918			8	0.016329	-0.045688
E(LU)			0.10879863				9	0.021298	-0.041465
E(CP)			0.03959874				10	0.026669	-0.036455
E(LB)			0.07194033				11	0.032560	-0.030526
23	13	1	-0.028970	-0.067886			12	0.038985	-0.023615
		2	-0.026565	-0.070274			13	0.046066	-0.015549
		3	-0.022939	-0.070390			14	0.053887	-0.006157
		4	-0.018475	-0.069079			15	0.02596	0.004820
		5	-0.013288	-0.066620			16	0.695593	0.567014
		6	-0.007415	-0.063126	E(LU)			0.06630856	
		7	-0.000851	-0.058638	E(CP)			0.00920619	
		8	0.006430	-0.053149	E(LB)			0.05C06475	
		9	0.014477	-0.046619					
		10	0.023356	-0.038975					
		11	0.033154	-0.030114					
		12	0.043981	-0.019898					
		13	0.997106	0.654769					
E(LU)			0.09335412						
E(CP)			0.02945680						
E(LB)			0.06528043						

TABLE OF WEIGHTS (CONTINUED)

N	M	I	A(N,M,I)	C(N,M,I)	N	M	I	A(N,M,I)	C(N,M,I)	
23	17	1	-0.003655	-0.048263	23	19	1	0.003411	-0.041199	
		2	-0.001244	-0.050639			2	0.005909	-0.043487	
		3	0.001481	-0.051447			3	0.008471	-0.044457	
		4	0.004455	-0.051283			4	0.011123	-0.044615	
		5	0.007669	-0.050345			5	0.013887	-0.044125	
		6	0.011133	-0.048710			6	0.016780	-0.043660	
		7	0.014831	-0.046438			7	0.019798	-0.041470	
		8	0.018871	-0.043448			8	0.022996	-0.039317	
		9	0.023152	-0.039831			9	0.026380	-0.036600	
		10	0.027817	-0.035444			10	0.030001	-0.033248	
		11	0.032865	-0.030257			11	0.033825	-0.029295	
		12	0.038384	-0.024144			12	0.037942	-0.024577	
		13	0.044389	-0.017027			13	0.042427	-0.018980	
		14	0.051034	-0.008672			14	0.047315	-0.012379	
		15	0.058398	0.001120			15	0.052660	-0.004606	
		16	0.066644	0.012681			16	0.058612	0.004662	
		17	0.603776	0.532147			17	0.055310	0.015808	
E(LU)			0.06119601				18	0.072957	0.029414	
E(CP)			0.00470017				19	0.430194	0.451531	
E(LB)			0.04609331		E(LU)			0.05430916		
					E(CP)				-0.00217056	
					E(LB)				0.03922450	
23	18	1	0.000194	-0.044575	23	20	1	0.006104	-0.038066	
		2	0.002646	-0.046912			2	0.008651	-0.040298	
		3	0.005275	-0.047812			3	0.011168	-0.041321	
		4	0.008068	-0.047822			4	0.013716	-0.041599	
		5	0.011028	-0.047126			5	0.016325	-0.041290	
		6	0.014162	-0.045809			6	0.019011	-0.04C466	
		7	0.017515	-0.043866			7	0.021809	-0.039131	
		8	0.021048	-0.041362			8	0.024700	-0.037336	
		9	0.024872	-0.038183			9	0.027785	-0.034966	
		10	0.028875	-0.034430			10	0.030958	-0.032134	
		11	0.033363	-0.029780			11	0.034420	-0.028603	
		12	0.038034	-0.024480			12	0.037984	-0.024527	
		13	0.043231	-0.018136			13	0.041940	-0.019546	
		14	0.048884	-0.010732			14	0.046153	-0.013730	
		15	0.055157	-0.001925			15	0.050775	-0.006799	
		16	0.062143	0.008368			16	0.055861	0.001462	
		17	0.070C35	0.020767			17	0.061571	0.011459	
		18	0.515472	0.493874			18	0.068058	0.023716	
E(LU)			0.05728653		E(CP)			19	0.075590	0.039106
E(CP)			0.00095448		E(LB)			20	0.347421	0.404070
E(LB)			0.04250454		E(LU)				0.05206387	
					E(CP)					-0.0C478196
					E(LB)					0.03618730

TABLE OF WEIGHTS (CONTINUED)

N	M	I	A(N,M,I)	C(N,M,I)	N	M	I	A(N,M,I)	C(N,M,I)
23	21	1	0.008356	0.35111	23	23	1	0.011749	-0.029300
		2	0.010952	-0.037277			2	0.014443	-0.031296
		3	0.013461	-0.038337			3	0.016915	-0.032383
		4	0.015912	-0.03818			4	0.019296	-0.032915
		5	0.018403	-0.038563			5	0.021637	-0.033014
		6	0.020936	-0.037940			6	0.023968	-0.032735
		7	0.023539	-0.036861			7	0.026314	-0.032093
		8	0.026213	-0.035349			8	0.028683	-0.031103
		9	0.029021	-0.033345			9	0.031120	-0.029730
		10	0.031907	-0.030890			10	0.033589	-0.027985
		11	0.034969	-0.027882			11	0.036174	-0.025797
		12	0.038215	-0.024224			12	0.038830	-0.023139
		13	0.041650	-0.019928			13	0.041635	-0.019922
		14	0.045352	-0.014781			14	0.044584	-0.016060
		15	0.049362	-0.00853			15	0.047728	-0.011412
		16	0.053758	-0.001297			16	0.051110	-0.005790
		17	0.058642	0.007615			17	0.054801	0.001083
		18	0.064166	0.018608			18	0.058897	0.009633
		19	0.070550	0.032491			19	0.063548	0.020550
		20	0.078160	0.050676			20	0.069018	0.035063
		21	0.266495	0.349764			21	0.075300	0.055713
E(LU)			0.05040338				22	0.085149	0.089235
E(CP)			-0.00696129				23	0.105012	0.203397
E(LB)			0.03332701		E(LU)			0.04846684	
					E(CP)				-0.01023295
					E(LB)				0.02772378
23	22	1	0.010228	-0.032246					
		2	0.012873	-0.034337					
		3	0.015348	-0.035418					
		4	0.017763	-0.035883					
		5	0.020166	-0.035864					
		6	0.022582	-0.035420					
		7	0.025037	-0.034566					
		8	0.027534	-0.033327					
		9	0.030133	-0.031642					
		10	0.032777	-0.029557					
		11	0.035580	-0.026947					
		12	0.038475	-0.023825					
		13	0.041565	-0.020057					
		14	0.044637	-0.015569					
		15	0.048365	-0.010179					
		16	0.052108	-0.003701					
		17	0.056406	0.004192					
		18	0.061135	0.013968					
		19	0.066561	0.026384					
		20	0.073001	0.042777					
		21	0.081024	0.065832					
		22	0.186420	0.285386					
E(LU)			0.04922310		E(LU)				
E(CP)			-0.00876815		E(CP)				
E(LB)			0.03056093		E(LB)				
					24	5	1	-0.312447	-0.194542
						2	-0.301019	-0.192877	
						3	-0.278309	-0.184517	
						4	-0.248301	-0.171890	
						5	2.140076	0.743825	
					E(LU)			0.72807462	
					E(CP)			0.31130369	
					E(LB)			0.19126190	

TABLE OF WEIGHTS (CONTINUED)

N	M	I	A(N,M,I)	C(N,M,I)	N	M	I	A(N,M,I)	C(N,M,I)
24	6	1	-0.224126	-0.160763	24	11	1	-0.056685	-0.083038
		2	-0.216634	-0.160605			2	-0.054241	-0.085164
		3	-0.201057	-0.154973			3	-0.049681	-0.084589
		4	-0.180228	-0.145857			4	-0.043721	-0.082316
		5	-0.155085	-0.133918			5	-0.036586	-0.078677
		6	1.977123	0.756116			6	-0.028363	-0.073816
		E(LU)	0.49704860				7	-0.019070	-0.067786
		E(CP)	0.22295192				8	-0.008690	-0.060589
		E(LB)	0.15747334				9	0.002829	-0.052190
							10	0.015559	-0.042523
24	7	1	-0.165886	-0.136519			11	1.278649	0.710688
		2	-0.160606	-0.137280	E(LU)			0.13520496	
		3	-0.149328	-0.133438	E(CP)			0.05663907	
		4	-0.134146	-0.126672	E(LB)			0.08029586	
		5	-0.115746	-0.117541					
		6	-0.094409	-0.106282	24	12	1	-0.043350	-0.075114
		7	1.820121	0.757733			2	-0.041075	-0.077341
		E(LU)	0.35758552				3	-0.037150	-0.077143
		E(CP)	0.16489218				4	-0.032125	-0.075425
		E(LB)	0.13330255				5	-0.026171	-0.072488
							6	-0.019351	-0.068461
24	8	1	-0.125290	-0.118250			7	-0.011678	-0.063393
		2	-0.121304	-0.119593			8	-0.003130	-0.057285
		3	-0.112772	-0.116987			9	0.006334	-0.050108
		4	-0.101272	-0.111878			10	0.016780	-0.041798
		5	-0.087317	-0.104747			11	0.028293	-0.032267
		6	-0.071114	-0.095799			12	1.162621	0.690824
		7	-0.052731	-0.085111	E(LU)			0.11310142	
		8	1.671800	0.752364	E(CP)			0.04350525	
		E(LU)	0.26790847		E(LB)			0.07249181	
		E(CP)	0.12453462						
		E(LB)	0.11514035		24	13	1	-0.032719	-0.068363
							2	-0.030535	-0.070648
24	9	1	-0.095798	-0.103970			3	-0.027071	-0.070743
		2	-0.092592	-0.105691			4	-0.022744	-0.069468
		3	-0.085890	-0.103970			5	-0.017683	-0.067099
		4	-0.076896	-0.100075			6	-0.011934	-0.063752
		5	-0.066000	-0.094425			7	-0.005499	-0.059470
		6	-0.053356	-0.087200			8	0.001635	-0.054260
		7	-0.039009	-0.078467			9	0.009515	-0.048088
		8	-0.022943	-0.068229			10	0.018189	-0.040903
		9	1.532484	0.742027			11	0.027735	-0.032622
		E(LU)	0.20751570				12	0.038242	-0.023135
		E(CP)	0.09529249				13	1.052869	0.668551
		E(LB)	0.10098133		E(LU)			0.09664182	
					E(CP)			0.03305372	
24	10	1	-0.073685	-0.092486	E(LB)			0.06585529	
		2	-0.070954	-0.094454					
		3	-0.065509	-0.093387					
		4	-0.058278	-0.090406					
		5	-0.049557	-0.085886					
		6	-0.039461	-0.079984					
		7	-0.028021	-0.072761					
		8	-0.015218	-0.064218					
		9	-0.000998	-0.054317					
		10	1.401679	0.727899					
		E(LU)	0.16539357						
		E(CP)	0.07341826						
		E(LB)	0.08962194						

TABLE OF WEIGHTS (CONTINUED)

N	M	I	A(N,M,I)	C(N,M,I)	N	M	I	A(N,M,I)	C(N,M,I)
24	14	1	-0.024127	-0.062531	24	17	1	-0.006499	-0.048891
		2	-0.021983	-0.064844			2	-0.004321	-0.051174
		3	-0.018857	-0.065168			3	-0.001761	-0.051934
		4	-0.015060	-0.064253			4	0.001076	-0.051760
		5	-0.010682	-0.062346			5	0.004211	-0.050811
		6	-0.005761	-0.059561			6	0.007533	-0.049264
		7	-0.000290	-0.055934			7	0.011242	-0.046993
		8	0.005750	-0.051466			8	0.015072	-0.044237
		9	0.012378	-0.046144			9	0.019386	-0.040701
		10	0.019668	-0.039899			10	0.023957	-0.036555
		11	0.027663	-0.032671			11	0.028939	-0.031656
		12	0.036447	-0.024354			12	0.034306	-0.025980
		13	0.046122	-0.014814			13	0.04020	-0.019361
		14	0.948731	0.643985			14	0.04670	-0.011667
E(LU)			0.08422122		E(LU)		15	0.053823	-0.302782
E(CP)			0.02462280		E(CP)		16	0.061755	0.007593
E(LB)			0.06013250		E(LB)		17	0.664373	0.556173
24	15	1	-0.017105	-0.057431	E(LU)			0.06186649	
		2	-0.014969	-0.059749	E(CP)			0.00738246	
		3	-0.012092	-0.060254	E(LB)			0.04679261	
		4	-0.008696	-0.059630					
		5	-0.004850	-0.058110	24	18	1	-0.002475	-0.045255
		6	-0.000583	-0.055800			2	-0.000259	-0.047504
		7	0.004161	-0.052701			3	0.002201	-0.048354
		8	0.009290	-0.048895			4	0.004666	-0.048336
		9	0.014974	-0.044259			5	0.007700	-0.047659
		10	0.021148	-0.038824			6	0.010794	-0.046318
		11	0.027900	-0.032498			7	0.014016	-0.044487
		12	0.035313	-0.025177			8	0.017417	-0.042119
		13	0.043457	-0.016750			9	0.021386	-0.038895
		14	0.052436	-0.007059			10	0.025182	-0.035448
		15	0.849616	0.617138			11	0.029642	-0.031020
E(LU)			0.07475231		E(LU)		12	0.034054	-0.026209
E(CP)			0.01774484		E(CP)		13	0.039415	-0.020075
E(LB)			0.05513653		E(LB)		14	0.044838	-0.013352
24	16	1	-0.011313	-0.052921	E(LU)		15	0.050958	-0.005370
		2	-0.009163	-0.055227	E(CP)		16	0.057699	0.003929
		3	-0.006469	-0.055875	E(LB)		17	0.065252	0.014885
		4	-0.003385	-0.055494	E(LU)		18	0.577315	0.521587
		5	0.000046	-0.054297	E(CP)			0.05752515	
		6	0.003828	-0.052365	E(LB)			0.00346018	
		7	0.007921	-0.04971				0.04324895	
		8	0.012411	-0.046465					
		9	0.017303	-0.042445					
		10	0.022558	-0.037723					
		11	0.028368	-0.032133					
		12	0.034638	-0.025703					
		13	0.041559	-0.018228					
		14	0.049152	-0.009617					
		15	0.057555	0.000342					
		16	0.754990	0.587928					
E(LU)			0.06747956						
E(CP)			0.01208139						
E(LB)			0.05072627						

TABLE OF WEIGHTS (CONTINUED)

N	M	I	A(N,M,I)	C(N,M,I)	N	M	I	A(N,M,I)	C(N,M,I)
24	19	1	0.000905	-0.041941	24	21	1	0.006154	-0.036040
		2	0.003164	-0.044148			2	0.008506	-0.038142
		3	0.005555	-0.045066			3	0.010815	-0.039151
		4	0.008071	-0.045193			4	0.013140	-0.039493
		5	0.010734	-0.044684			5	0.015514	-0.039306
		6	0.013521	-0.043644			6	0.017945	-0.038667
		7	0.016435	-0.042115			7	0.020429	-0.037625
		8	0.019637	-0.039942			8	0.023099	-0.036040
		9	0.022803	-0.037505			9	0.025743	-0.034203
		10	0.026719	-0.033941			10	0.028697	-0.031687
		11	0.029997	-0.030672			11	0.031580	-0.028925
		12	0.034402	-0.025868			12	0.034836	-0.025342
		13	0.038730	-0.020747			13	0.038156	-0.021392
		14	0.043507	-0.014657			14	0.041933	-0.016415
		15	0.048732	-0.007553			15	0.045799	-0.010844
		16	0.054520	0.000812			16	0.050108	-0.004137
		17	0.060958	0.010675			17	0.054842	0.003809
		18	0.068216	0.022447			18	0.060165	0.013408
		19	0.493393	0.48374			19	0.066188	0.025170
E(LU)			0.05417052				20	0.073197	0.036844
E(CP)			0.00017117				21	0.333154	0.395179
E(LB)			0.04002428		E(LU)			0.04962788	
					E(CP)				-0.00492314
					E(LB)				0.03429681
24	20	1	0.003753	-0.038888	24	22	1	0.008175	-0.033339
		2	0.006057	-0.041046			2	0.010574	-0.035378
		3	0.008399	-0.042017			3	0.012864	-0.036413
		4	0.010808	-0.042259			4	0.015129	-0.036835
		5	0.013294	-0.041940			5	0.017403	-0.036782
		6	0.015900	-0.041093			6	0.019717	-0.036300
		7	0.018611	-0.039782			7	0.022047	-0.035464
		8	0.021436	-0.038014			8	0.024510	-0.034155
		9	0.024426	-0.035765			9	0.026977	-0.032554
		10	0.027521	-0.033081			10	0.029650	-0.030414
		11	0.031146	-0.029441			11	0.032257	-0.028021
		12	0.034308	-0.025968			12	0.035139	-0.024936
		13	0.038424	-0.021075			13	0.038322	-0.021171
		14	0.042551	-0.015682			14	0.041338	-0.017209
		15	0.047082	-0.009322			15	0.044935	-0.011998
		16	0.052019	-0.001870			16	0.048628	-0.006114
		17	0.057545	0.007016			17	0.052763	0.001032
		18	0.063743	0.017651			18	0.057327	0.009615
		19	0.070809	0.030651			19	0.062480	0.020215
		20	0.412170	0.441924			20	0.068458	0.033512
E(LU)			0.05159088		E(LU)			0.04816352	
E(CP)			-0.00259469		E(CP)				-0.00687983
E(LB)			0.03705876		E(LB)				0.031682??
							21	0.075549	0.050964
							22	0.255757	0.341745

TABLE OF WEIGHTS (CONTINUED)

N	M	I	A(N,M,I)	C(N,M,I)	N	M	I	A(N,M,I)	C(N,M,I)
24	23	1	0.009865	-0.030709	25	3	1	-0.741297	-0.328748
		2	0.012311	-0.032676			2	-0.706762	-0.319677
		3	0.014593	-0.033724			3	2.448059	0.648426
		4	0.016814	-0.034214	E(LU)			2.08530608	
		5	0.019018	-0.034270	E(CP)			0.74287178	
		6	0.021232	-0.033942	E(LB)				0.32648069
		7	0.023451	-0.033279					
		8	0.025757	-0.032215	25	4	1	-0.468472	-0.245175
		9	0.028049	-0.030887			2	-0.450043	-0.24037
10			0.030536	-0.029034			3	-0.415470	-0.228150
11			0.032941	-0.026957			4	2.333986	0.714962
12			0.035565	-0.024275	E(LU)			1.18738033	
13			0.038329	-0.021160	E(CP)			0.46781327	
14			0.041191	-0.017439	E(LB)				0.24222296
15			0.044281	-0.013016					
16			0.047572	-0.007758	25	5	1	-0.321316	-0.194777
17			0.051172	-0.001443			2	-0.310282	-0.193172
18			0.055132	0.006201			3	-0.288191	-0.185159
19			0.059561	0.015675			4	-0.258993	-0.173084
20			0.064672	0.027621			5	2.178782	0.746191
21			0.070703	0.043424	E(LU)			0.75602911	
22			0.078235	0.065561	E(CP)			0.32008373	
23			0.179020	0.278512	E(LB)				0.19162842
E(LU)			0.04711383						
E(CP)			-0.00851289		25	6	1	-0.231589	-0.161021
E(LB)			0.02914162				2	-0.224397	-0.160862
							3	-0.209240	-0.155458
24	24	1	0.011248	-0.027993			4	-0.188950	-0.146734
		2	0.013739	-0.029871			5	-0.164473	0.135339
		3	0.016021	-0.030917			6	2.018650	0.759414
		4	0.018216	-0.031460	E(LU)			0.51744818	
		5	0.020370	-0.031614	E(CP)			0.23032985	
		6	0.022514	-0.031424	E(LB)				0.15786311
		7	0.024647	-0.030730					
		8	0.026838	-0.030091	25	7	1	-0.172349	-0.136802
		9	0.029015	-0.028489			2	-0.167311	-0.137524
10			0.031329	-0.027477			3	-0.156342	-0.133831
11			0.033589	-0.025584			4	-0.141540	-0.127351
12			0.035989	-0.023440			5	-0.123602	-0.118629
13			0.038543	-0.020740			6	-0.102823	-0.107905
14			0.041131	-0.017557			7	1.863966	0.762043
15			0.043928	-0.013710	E(LU)			0.37295445	
16			0.046862	-0.009153	E(CP)			0.17125667	
17			0.050054	-0.003639	E(LB)				0.13371230
18			0.053531	0.003055					
		19	0.057386	0.011390	25	3	1	-0.130991	-0.118557
		20	0.061783	0.021945			2	-0.127221	-0.119837
		21	0.066927	0.036007			3	-0.118931	-0.117327
		22	0.073331	0.055932			4	-0.107714	-0.112428
		23	0.082153	0.088238			5	-0.054093	-0.105611
		24	0.100863	0.198122			6	-0.078289	-0.097082
E(LU)			0.04643549				7	-0.060385	-0.086925
E(CP)			-0.00984533				8	1.717625	0.757767
E(LB)			0.02652435		E(LU)			0.27973288	
					E(CP)				0.13012998
25	2	1	-1.368683	-0.494926	E(LB)				0.11556839
		2	2.368683	0.494926					
E(LU)			4.48592812						
E(CP)			1.37873247						
E(LB)			0.49690321						

TABLE OF WEIGHTS (CONTINUED)

N	M	I	A(N,M,I)	C(N,M,I)	N	M	I	A(N,M,I)	C(N,M,I)
25	9	1	-C.10C902	-0.104300	25	13	1	-0.036308	-0.068792
		2	-C.097898	-0.105944			2	-0.034320	-0.070982
		3	-0.091397	-0.104281			3	-0.031004	-0.071058
		4	-0.082624	-0.100540			4	-0.026804	-0.069819
		5	-0.071979	-0.095134			5	-0.021861	-0.067534
		6	-C.059629	-0.088240			6	-0.016228	-0.064321
		7	-0.045632	-0.079936			7	-0.009922	-0.060231
		8	-0.029985	-0.070233			8	-0.002924	-0.055270
		9	1.58C04	0.748609			9	0.004794	-0.049420
E(LU)			0.21673546				10	0.013273	-0.042642
E(CP)			0.10028244				11	0.022584	-0.034867
E(LB)			0.10142692				12	0.032798	-0.026010
							13	1.105923	0.680946
25	10	1	-C.078304	-0.092840	E(LU)			0.10012423	
		2	-0.075769	-0.094722	E(CP)			0.03650889	
		3	-0.070501	-0.093684	E(LB)			0.06637441	
		4	-0.063450	-0.090817					
		5	-0.054925	-0.086485	25	14	1	-0.027463	-0.062987
		6	-0.045053	-0.080848			2	-0.025518	-0.065206
		7	-0.033874	-0.073973			3	-0.022537	-0.065502
		8	-0.021382	-0.065870			4	-0.018860	-0.064606
		9	-0.007535	-0.056515			5	-0.014588	-0.062761
		10	1.450793	0.735755			6	-0.009771	-0.060083
E(LU)			0.17263602				7	-0.004406	-0.056611
E(CP)			0.07791785				8	0.001530	-0.052347
E(LB)			0.09008494				9	0.008022	-0.047302
25	11	1	-0.060903	-0.083415			10	0.015177	-0.041393
		2	-0.058654	-0.085451			11	0.022982	-0.034605
		3	-0.054256	-0.084885			12	0.031548	-0.026830
		4	-0.048449	-0.082692			13	0.040941	-0.017971
		5	-0.041474	-0.079199	E(LU)			0.08682651	
		6	-0.033425	-0.074550	E(CP)			0.02782135	
		7	-0.024332	-0.068804	E(LB)			0.06067302	
		8	-0.014184	-0.061972					
		9	-0.002945	-0.054030	25	15	1	-0.020217	-0.057916
		10	0.009446	-0.044927			2	-0.018283	-0.060172
		11	1.329176	0.719926			3	-0.015551	-0.060613
E(LU)			0.14090683				4	-0.012269	-0.059993
E(CP)			0.06073226				5	-0.008537	-0.058526
E(LB)			0.08077665				6	-0.004338	-0.056280
25	12	1	-0.047230	-0.075517			7	0.000300	-0.053317
		2	-0.045150	-0.077650			8	0.005319	-0.049695
		3	-0.041377	-0.077446			9	0.012966	-0.045241
		4	-0.036489	-0.075783			10	0.015954	-0.040149
		5	-0.030670	-0.072958			11	0.023615	-0.034163
		6	-0.023991	-0.069100			12	0.030844	-0.027321
		7	-0.016473	-0.064265			13	0.038774	-0.019488
		8	-0.008104	-0.058459			14	0.047483	-0.010542
		9	0.001149	-0.051664	E(LU)			0.07673648	
		10	0.011340	-0.043833	E(CP)			0.02071714	
		11	0.022540	-0.034894	E(LB)			0.05570065	
		12	1.214454	0.701568					
E(LU)			0.11757719						
E(CP)			0.04725515						
E(LB)			0.07299117						

TABLE OF WEIGHTS (CONTINUED)

N	M	I	A(N,M,I)	C(N,M,I)	N	M	I	A(N,M,I)	C(N,M,I)
25	16	1	-0.014226	-0.053437	25	19	1	-0.001511	-0.042582
		2	-0.012280	-0.055655			2	0.000536	-0.044712
		3	-0.009730	-0.056262			3	0.002777	-0.045580
		4	-0.006767	-0.055881			4	0.005148	-0.045706
		5	-0.003416	-0.054698			5	0.007784	-0.045118
		6	0.000228	-0.052868			6	0.010293	-0.044292
		7	0.004311	-0.050319			7	0.013648	-0.042297
		8	0.006740	-0.047138			8	0.016012	-0.040961
		9	0.013383	-0.043435			9	0.019203	-0.038460
		10	0.018781	-0.038783			10	0.024225	-0.034053
		11	0.024316	-0.033639			11	0.026723	-0.031592
		12	0.030527	-0.027559			12	0.030579	-0.027487
		13	0.037271	-0.020612			13	0.034843	-0.022690
		14	0.044668	-0.012645			14	0.040233	-0.016383
		15	0.052795	-0.003537			15	0.045011	-0.010159
		16	0.811399	0.606468			16	0.050657	-0.002512
E(LU)			0.06888924				17	0.056882	0.006342
E(CP)			0.01485185				18	0.063787	0.016770
E(LB)			0.05131672				19	0.553170	0.511471
25	17	1	-0.009232	-0.049443	E(LU)			0.05430050	
		2	-0.007260	-0.051640	E(CP)			0.00244102	
		3	-0.004848	-0.052357	E(LB)			0.04072222	
		4	-0.002117	-0.052162					
		5	0.000879	-0.051264	25	20	1	0.001479	-0.039587
		6	0.004177	-0.049710			2	0.003569	-0.041673
		7	0.007815	-0.047517			3	0.005756	-0.042596
		8	0.011434	-0.044984			4	0.008031	-0.042816
		9	0.015921	-0.041405			5	0.010448	-0.042449
		10	0.020253	-0.037606			6	0.013025	-0.041554
		11	0.025191	-0.032939			7	0.015402	-0.040560
		12	0.030451	-0.027620			8	0.018347	-0.038621
		13	0.036231	-0.021444			9	0.021346	-0.036313
		14	0.042593	-0.014304			10	0.024325	-0.033953
		15	0.049500	-0.006173			11	0.028185	-0.030127
		16	0.057147	0.003248			12	0.030435	-0.027632
		17	0.721867	0.577320			13	0.035676	-0.021855
E(LU)			0.06278626				14	0.036707	-0.017912
E(CP)			0.00997094				15	0.043784	-0.011387
E(LB)			0.04741317				16	0.048355	-0.004818
25	18	1	-0.005043	-0.045848			17	0.053791	0.003245
		2	-0.003036	-0.048015			18	0.059696	0.012672
		3	-0.000726	-0.048819	E(LU)		19	0.066471	0.023804
		4	0.001824	-0.048779	E(CP)		20	0.473171	0.474112
		5	0.004483	-0.048170	E(LB)			0.0513934	
		6	0.007751	-0.046642				-0.00046792	
		7	0.010435	-0.045269				0.03780750	
		8	0.014601	-0.042266					
		9	0.017272	-0.040246					
		10	0.022055	-0.036060					
		11	0.026242	-0.032037					
		12	0.030231	-0.027809					
		13	0.035679	-0.021917					
		14	0.041032	-0.015644					
		15	0.047011	-0.008309					
		16	0.053506	0.000123					
		17	0.060779	0.009946					
		18	0.635905	0.545761					
E(LU)			0.05802293						
E(CP)			0.00588284						
E(LB)			0.04390460						

TABLE OF WEIGHTS (CONTINUED)

N	M	I	A(N,M,I)	C(N,M,I)	N	M	I	A(N,M,I)	C(N,M,I)
25	21	1	0.004015	-0.036813	25	23	1	0.007991	-0.01733
		2	0.006150	-0.038850			2	0.010217	-0.033654
		3	0.008301	-0.039812			3	0.012332	-0.034661
		4	0.010494	-0.040124			4	0.014413	-0.035114
		5	0.012767	-0.039913			5	0.016307	-0.035132
		6	0.015083	-0.039304			6	0.018615	-0.034796
		7	0.017547	-0.038195			7	0.020791	-0.034037
		8	0.019926	-0.036894			8	0.022797	-0.033205
		9	0.023362	-0.034198			9	0.025487	-0.031417
		10	0.024924	-0.033298			10	0.027226	-0.030315
		11	0.028334	-0.029964			11	0.030451	-0.027371
		12	0.032751	-0.025098			12	0.032439	-0.025277
		13	0.033983	-0.023707			13	0.034975	-0.022600
		14	0.038804	-0.017806			14	0.038427	-0.018207
		15	0.042477	-0.012817			15	0.040862	-0.014907
		16	0.046778	-0.006543			16	0.044536	-0.009371
		17	0.051285	0.000504			17	0.047835	-0.003905
		18	0.056394	0.009060			18	0.051722	0.003109
		19	0.062243	0.019180			19	0.056077	0.011315
		20	0.068693	0.031758			20	0.060755	0.021679
		21	0.395689	0.432743			21	0.06631	0.034261
E(LU)			0.04914458		E(LU)				
E(CP)			-0.00293163						
E(LB)			0.03511308						
25	22	1	0.006168	-0.034211	E(CP)				
		2	0.008348	-0.036193	E(LB)				
		3	0.010476	-0.037183		25	24	1	-0.00678580
		4	0.012607	-0.037570			2	0.011794	0.05018924
		5	0.014776	-0.037485			3	0.013905	-0.032175
		6	0.017026	-0.036955			4	0.015953	-0.032683
		7	0.019221	-0.036171			5	0.017988	-0.032792
		8	0.021340	-0.035185			6	0.020022	-0.032574
		9	0.024679	-0.032515			7	0.022074	-0.032010
		10	0.025895	-0.032125			8	0.024017	-0.031278
		11	0.030229	-0.027673			9	0.026504	-0.029812
		12	0.031117	-0.027074			10	0.028155	-0.028849
		13	0.035583	-0.021713			11	0.031096	-0.026352
		14	0.038063	-0.018702			12	0.032808	-0.024695
		15	0.041779	-0.013661			13	0.035503	-0.021765
		16	0.045324	-0.008299			14	0.038100	-0.018724
		17	0.049433	-0.001734			15	0.040722	-0.015128
		18	0.053748	0.005862			16	0.043591	-0.010706
		19	0.058821	0.015944			17	0.046790	-0.005556
		20	0.064336	0.026491			18	0.050125	0.000586
		21	0.071016	0.040325			19	0.053932	0.007926
		22	0.320015	0.386798			20	0.057987	0.017243
E(LU)			0.04741691				21	0.062967	0.028582
E(CP)			-0.00501984				22	0.068493	0.043984
E(LB)			0.03258909				23	0.075661	0.055216
							24	0.172188	0.272031
					E(LU)				0.04517886
					E(CP)				-0.00826855
					E(LB)				0.02784672

TABLE OF WEIGHTS (CONTINUED)

N	M	I	A(N,M,I)	C(N,M,I)	N	M	I	A(N,M,I)	C(N,M,I)
25	25	1	0.010788	-0.026796					
		2	0.013098	-0.028566					
		3	0.015213	-0.029573					
		4	0.017239	-0.030122					
		5	0.019234	-0.030313					
		6	0.021211	-0.030205					
		7	0.023185	-0.029800					
		8	0.025057	-0.029207					
		9	0.027393	-0.028041					
		10	0.029004	-0.027158					
		11	0.021672	-0.025206					
		12	0.033363	-0.023590					
		13	0.035757	-0.021260					
		14	0.038198	-0.018529					
		15	0.040571	-0.015429					
		16	0.043268	-0.011548					
		17	0.046011	-0.007108					
		18	0.048983	-0.001688					
		19	0.052348	0.004773					
		20	0.055864	0.013016					
		21	0.060199	0.023073					
		22	0.064907	0.036847					
		23	0.071049	0.056035					
		24	0.079353	0.087235					
		25	0.097036	0.193159					
E(LU)			-0.00009232						
E(CP)			"0.00948561						
E(LB)			0.02542407						

APPENDIX D

CRAMER-RAO EFFICIENCIES OF BEST LINEAR INVARIANT ESTIMATES OF PARAMETERS OF THE EXTREME-VALUE DISTRIBUTION

INTRODUCTION AND SUMMARY

The Weibull distribution, since it was empirically derived by W. Weibull [12] in 1939, has been shown in innumerable situations to provide an appropriate model for survival populations associated with life testing. This distribution, which had been derived earlier by Von Mises and Fisher and Tippett (see Gumbel [3]) using extreme-value considerations, is also known as the Fisher-Tippett type III distribution or the third asymptotic distribution of smallest values. This explains why the Weibull model is often applicable when the cause of failure is characterized by a weakest-link or severest-flaw phenomenon.

When there is no threshold below which a failure cannot occur, the following two-parameter form of the Weibull distribution may apply:

$$F_{\delta,b}(t) \begin{cases} = 1 - \exp[-(t/\delta)^{1/b}], & t \geq 0 \\ = 0 & \text{otherwise} . \end{cases}$$

Here $\delta > 0$ is a scale parameter and $b > 0$ determines the shape of the distribution. The location parameter present in the three-parameter form (when a lower failure threshold does exist) is assumed to be zero.

This two-parameter Weibull distribution can also be useful in providing a model for populations which are not of the survival type. A recent example is a study of the thrust build-up curves for a large rocket

engine. It was found that at any specified time from engine start the observed thrust levels for the specified engine system over many runs could be very well described by means of the two-parameter Weibull. It is not clear at this time why this distribution provides such a good model for the thrust build-up process.

If any random variable T has the Weibull distribution with parameters δ and b , then $X = \log T$ has the (first) extreme-value distribution of smallest values, with

$$P(X \leq x) = P_{u,b}(x) = 1 - \exp(-\exp(-(x-u)/b)), \quad b > 0.$$

The parameter b is a scale parameter of this distribution and $u = \log \delta$ is the mode, a location parameter. For any estimation problem, an analysis in terms of X rather than T will be more fruitful.

One of the difficulties encountered in dealing with the two-parameter Weibull or extreme-value distribution has been the fact that "good" estimates of the parameters are not easily obtained. The maximum-likelihood estimates are obtained only with considerable effort (iteratively), and the mean squared errors of these estimates are not known except in the asymptotic case. Furthermore, since the minimally sufficient statistic for either the Weibull or extreme-value distribution consists of all the available extreme-value observations (see [10]), the dimension of the sufficient statistic is equal to the number of observations made.

Therefore, the result of Rao [11], which guarantees that maximum-likelihood estimates are the minimum-variance estimates of their expected values (when the number of sufficient statistics is equal to the number of parameters to be estimated), is not applicable when more than two observations are made. Hence one cannot claim optimality properties for the maximum-likelihood estimates of the two Weibull parameters when the number of observations is greater than two, but not large enough for asymptotic theory to apply.

A method in widespread use for Weibull parameter estimation employs a graphical plot which is based on fitting a linear model by approximating the method of least squares. The Weibull plot is of unquestionable value in finding outliers or in determining whether the sample data indicate that the population is of the prescribed type. With respect to the problem of estimation, however, graphical procedures which involve visually fitting the least-squares line will obviously be inferior to analytical procedures which yield true Gauss-Markov least-squares estimates.

The least-squares or best linear unbiased estimates which, for limited sample sizes, can be found relatively easily for certain functions of the two extreme-value parameters, once appropriate weights (or coefficients) have been found, enjoy all the usual asymptotic properties of consistency, efficiency, and normality provided by the maximum-likelihood

estimates (see Blom [1]). Furthermore, if the weights for obtaining these estimates are available, the covariance matrices of the estimates are available as well. A recent result given in [9] allows one to calculate as simple functions of the least-squares estimates and their covariance matrices, linear estimates which have smallest expected loss among all linear estimates with expected loss invariant under transformations of location and scale. Here loss is defined to be squared error divided by the square of the extreme-value scale parameter. These estimates are uniformly better than the best linear unbiased (BLU) estimates and are, in fact, the unique admissible minimax linear estimates. They, of course, also have the asymptotic properties mentioned above plus the property of asymptotic unbiasedness.

Calculation of the weights for obtaining the best linear unbiased estimates (based on the results of Lieblein [7]), and from these the best linear invariant estimates of the two extreme-value parameters, has been completed for censored samples up to size 25. These calculated weights, along with the variances and covariances of the estimates, appear in [10]¹.

¹Although the calculations were performed for sample size n ranging from 2 through 25 (an extension of tables of Lieblein [8] giving values for n ranging from 2 through 6) the results given in [10] are through n equal to 20 only.

In the present report expressions are derived for Cramer-Rao bounds for the expected squared error of regular invariant estimates of extreme-value location and scale parameters. The bounds are calculated and compared with the mean squared error of the best linear invariant estimates of the two extreme-value parameters and, in addition, similar comparisons are made for certain percentiles of the distribution, for censored samples up to size 25.

All of the estimation procedures considered above, along with all but the numerical results given below, are applicable to the general case in which any selection of observations is censored from a size n sample. In the following, however, it is assumed that only the largest $n-r$, $2 \leq r \leq n$, observations are censored. This assumption corresponds to the situation in life testing in which testing is terminated at the time of the r^{th} failure. Termination of a life test in this manner (by failure number) is called Type II censoring to distinguish it from the type of censoring (Type I) wherein testing is stopped at a specified time after the initiation of the test.

EFFICIENCIES OF BEST LINEAR INVARIANT ESTIMATES OF
PARAMETERS OF THE EXTREME-VALUE DISTRIBUTION

Assume a population having the extreme-value distribution of smallest values given by

$$F_{u,b}(x) = 1 - \exp\{-\exp((x-u)/b)\}, \quad b > 0. \quad (1)$$

The function $R_{u,b}(x) = 1 - F_{u,b}(x) = \exp(-\exp((x-u)/b))$ gives the proportion of the population lying to the right of the point x . Assume a specified value R for $R_{u,b}(x)$ and let x_R be the point defined by $R = \exp(-\exp((x_R-u)/b))$. Then $x_R = u + b \log \log(1/R)$ is the percentile above which $100R\%$ of the population lies. If $R = 1/e$, then $x_R = u$. In a life-testing situation $R(x)$ is the proportion of the population surviving at age time x , so that if a reliability or survival proportion R is specified, the corresponding x_R is the logarithm of the time at which $100R\%$ of the population will have survived.

Let a size n sample be chosen from the population with distribution (1) and let an estimate of x_R be based on $X_{(1,n)} \leq X_{(2,n)} \dots \leq X_{(r,n)}$, the first r , $2 \leq r \leq n$, of the n ordered observations. In [10] there is considered the class of linear estimates of u , b , and x_R with expected loss invariant under location and scalar transformations, where loss is defined as squared error divided by b^2 . It is shown that

the best (minimum-expected-loss) estimates in this class are linear functions of the BLU estimates of u and b . Let u^* with variance Ab^2 and b^* with variance Cb^2 be the BLU estimates of u and b , respectively, and let Bb^2 be the covariance of the two estimates. The BLU estimate of $x_R = u+b \log \log(1/R)$ is $\tilde{x}_R^* = u^* + b^* \log \log(1/R)$, with variance $Q_R b^2 = [A+2B \log \log(1/R) + C(\log \log(1/R))^2]b^2$. The best linear invariant, BLI, estimate of x_R is $\tilde{x}_R = \tilde{u} + \tilde{b} [B/(1+C)] + [b^*/(1+C)] \log \log(1/R) = \tilde{u} + \tilde{b} \log \log(1/R)$. The expected losses for \tilde{u} and \tilde{b} are $\tilde{A}b^2 = [A-B^2/(1+C)]b^2$ and $\tilde{C}b^2 = [C/(1+C)]b^2$, respectively, with $E(\tilde{u}\tilde{b} - ub) = \tilde{B}b^2 = [B/(1+C)]b^2$. For \tilde{x}_R , the expected loss is thus $\tilde{Q}_R b^2 = [\tilde{A} + 2\tilde{B} \log \log(1/R) + \tilde{C}(\log \log(1/R))^2]b^2$ or $\tilde{Q}_R b^2 = [A + 2B \log \log(1/R) + C(\log \log(1/R))^2 - [(B+C \log \log(1/R))^2/(1+C)]]b^2$, clearly uniformly less than $Q_R b^2$. One may then inquire as to the efficiency of this estimate with respect to any nonlinear estimate which could be obtained.

Since the expected value of \tilde{x}_R is equal to $u+b \log \log(1/R) - [(B+C \log \log(1/R))/(1+C)]b$, this estimate is, in general, biased. Cramér-Rao bounds for the variance of unbiased estimates, therefore constitute for each r and n an incorrect standard with which to compare the mean squared error (MSE) of estimates with this given bias.

The variance $nQ_R^0 b^2 = n [A^0 + 2B^0 \log \log(1/R) + C^0 (\log \log(1/R))^2] b^2$ of an efficient estimate of $\sqrt{n}x_R$ based on $x_{(1,n)}, x_{(2,n)}, \dots, x_{(r,n)}$ depends upon r and n through $p = r/n$ only. The expression giving the appropriate lower bounds for the mean squared error of biased estimates of x_R as a function of A^0, B^0 , and C^0 and any given bias is derived in Appendix D.2.

This expression for estimates of x_R with bias $-[(E+C \log \log(1/R))/(1+C)]b$ is

$$\begin{aligned} & A^0 - \frac{2B(R^0)(1+C) - B^2(1+C^0)}{(1+C)^2} + \\ & \frac{2[B^0(1+C) + B(C-C^0)]\log \log(1/R)}{(1+C)^2} + \frac{C^0 + C^2}{(1+C)^2} (\log \log(1/R))^2 b^2 \\ & \equiv [\tilde{A}^0 + 2\tilde{B}^0 \log \log(1/R) + \tilde{C}^0 (\log \log(1/R))^2] b^2. \end{aligned}$$

This preliminary result is not, however, particularly meaningful as a lower bound, since other good invariant estimates which are nonlinear and have bias different from that specified may exist. A more meaningful lower bound would be one for the MSE of invariant estimates of x_R , a natural analogue to the classical bound Q_R^0 which provides the standard with which one may compare the variances of unbiased estimates of this parameter. Expressions giving the lower bounds for the MSE of invariant estimates of general location and scale parameters are therefore derived in Appendix D.1 and applied to the location parameter x_R .

(see footnote, p. 149) and the scale parameter b . These bounds for x_R and t are

$$\begin{aligned}\tilde{Q}_R^{0,b^2} &= \left\{ A^0 + 2B^0 \log \log (1/R) + C^0 (\log \log(1/R))^2 \right. \\ &\quad \left. - (B^0 + C^0 \log \log (1/R))^2 / (1+C^0) \right\} b^2 \\ &= \left\{ \tilde{A}^0 + 2\tilde{B}^0 \log \log(1/R) + \tilde{C}^0 (\log \log(1/R))^2 \right\} b^2 \\ \text{and } & [C^0/(1+C^0)] b^2 = \tilde{C}^0 b^2,\end{aligned}$$

respectively.

Table D.I gives values for \tilde{Q}_R^0 and \tilde{Q}_R^0 , with $R = .90$ and $R = .95$, and $\tilde{A}, \tilde{B}, \tilde{C}, \tilde{A}^0, \tilde{B}^0$, and \tilde{C}^0 for $2 \leq n \leq 25$, $2 \leq r \leq n$. Table D.II gives values for $A, B, C, A^0, B^0, C^0, Q_R^0$, and \tilde{Q}_R^0 for the same values of R, r , and n so comparisons can be made among the various sets of expected losses. The values for A, B , and C are obtained from [10] as are the expressions for A^0, B^0 , and C^0 . The Cramér-Rao efficiency of \tilde{x}_R for any combination of R, r , and n (and with b considered a nuisance parameter) is simply \tilde{Q}_R^0 divided by \tilde{Q}_R^0 . Cramér-Rao efficiencies for $\tilde{u}(\tilde{x}_R)$ with $R = 1/e$ and b a nuisance parameter will be given by \tilde{A}^0/\tilde{A} . Efficiencies for \tilde{b} with x_R a nuisance parameter will be given by \tilde{C}^0/\tilde{C} . The values of the efficiencies of $\tilde{Q}_{.90}$ for $2 \leq n \leq 18$, $2 \leq r \leq n$ appear in Table D.III.

It can be seen from Table D.III that for $n \leq 18$ the Cramer-Rao efficiencies of $\bar{Q}_{.90}$ are greater than .86 when r is greater than 2. When r is equal to 2 $(\bar{x}_{(1,n)}, \bar{x}_{(2,n)})$ is a complete sufficient statistic for x_R and b , as is shown in [10]. The estimates \bar{x}_R^* and \bar{b}^* , therefore, are the unique (with probability 1) uniformly minimum-variance unbiased estimates. It can be further inferred on the basis of the results of Appendix D.1 that, for $r = 2$, \bar{x}_R^* and \bar{b}^* are best in the class of all invariant estimates of x_R and b respectively, so that all the bounds given in Table D.I, as well as in Table D.II, are unrealistically low for r equal to 2 at least.

From Table D.I it can be observed that, for $r \geq 8$, all of the values given for expected loss indicate that the corresponding estimates have efficiencies of at least .84 with respect to their lower bounds.

A comparison of Table D.I and Table D.II shows that the discrepancy between the MSE of the BLI estimates and that of the BLU estimates is most pronounced when n is small and/or when there is extensive censoring and when a specified R is large.

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APPENDIX D.1

CRAMER-RAO LOWER BOUNDS FOR INVARIANT ESTIMATES
OF LOCATION AND SCALE PARAMETERS

Let Y_1, Y_2, \dots, Y_r be the first r order statistics of a size n random sample chosen from a population with density $f_{\mu, \sigma}(x)$, where (μ, σ) is a location-scale parameter¹ with $\sigma > 0$. Let the joint density of Y_1, Y_2, \dots, Y_r be $h_{\mu, \sigma}(y_1, y_2, \dots, y_r)$, let $p = r/n$, and let $\hat{\mu}$ and $\hat{\sigma}$ be the maximum-likelihood estimates, based on Y_1, Y_2, \dots, Y_r , of μ and σ , respectively.

It is assumed that the regularity conditions given in [4] are satisfied so that the concentration ellipse of the joint distribution of any pair of regular unbiased estimates of $\sqrt{n}\hat{\mu}$ and $\sqrt{n}\hat{\sigma}$ (where the definition of regular estimation is given in Appendix B with $\theta = (\mu, \sigma)$) contains the fixed ellipse specified by the asymptotic variances and covariances of $\sqrt{n}\hat{\mu}$ and $\sqrt{n}\hat{\sigma}$. Thus, the variance of any regular unbiased estimate

¹Here, if a density $f(x|\theta)$ with respect to Lebesgue measure exists, $\theta = (\theta_1, \theta_2)$ is a location-scale parameter if and only if $f(x|\theta) = \frac{1}{\theta_2} g(\frac{x-\theta_1}{\theta_2})$ for some function g . If $f(x|\theta)$ exists and (θ_1, θ_2) is a location-scale parameter, then for c a known constant, $(\theta_1 + c\theta_2, c\theta_2) = (\theta'_1, \theta'_2)$ is a location-scale parameter, since $f(x|\theta'_1, \theta'_2) = \frac{c}{\theta'_2} g(\frac{x-\theta'_1 + \theta'_2}{\theta'_2/c}) = \frac{1}{\theta'_2} \eta(\frac{x-\theta'_1}{\theta'_2})$ for some η .

of $\sqrt{n}\hat{\mu}$, where σ is considered a nuisance parameter, is greater than or equal to $n\alpha^0\sigma^2$, the asymptotic variance of $\sqrt{n}\hat{\mu}$, and likewise, the variance of any regular unbiased estimate of $\sqrt{n}\sigma$ is greater than or equal to $n\gamma^0\sigma^2$, the asymptotic variance of $\sqrt{n}\hat{\sigma}$ (see Cramer').

The variances $n\alpha^0\sigma^2$ and $n\gamma^0\sigma^2$ depend upon r and n through $p = r/n$ only, but α^0 and γ^0 are functions of both r and n .

Let loss be defined as squared error divided by σ^2 and consider estimates of $\varphi = \lambda\mu + m\sigma$ (λ and m known constants) with expected loss invariant under transformations of location and scale. Such an estimate has expected loss (risk) independent of μ and σ for all μ and σ . It is desired to find an expression giving a lower bound for the risk of any regular invariant estimate $\bar{\varphi}$ of φ when $\lambda = 1$, $m = 0$ or $m = 1$, $\lambda = 0$.

The requirement of invariant risk prescribes a particular form for $\bar{\varphi}$. Let $R(\varphi, \bar{\varphi})$ represent the expected loss of $\bar{\varphi}$ in the general case in which $\varphi = \lambda\mu + m\sigma$. $R(\varphi, \bar{\varphi})$ is independent of μ and σ for all values of μ and σ and is equal to

$$V(\bar{\varphi})/\sigma^2 + [E(\bar{\varphi} - \varphi)]^2/\sigma^2,$$

where $V(\bar{\varphi})$ is the variance of $\bar{\varphi}$ and $E(\bar{\varphi} - \varphi)$ is the bias of this estimate. Both terms are greater than or equal to zero so that each must be independent of μ and σ for all $\underline{\theta} = (\mu, \sigma)$. Thus, since

$E(\bar{\varphi}-\varphi)$ is equal to $E[\bar{\varphi}-k\mu-k\sigma]$, $\bar{\varphi}$ must be equal to $k\mu^* + k\sigma^*$, where μ^* and σ^* are regular unbiased estimates of μ and σ , respectively, and k is independent of μ and σ for all θ . The risk of $\bar{\varphi}$ is therefore of the form

$$\frac{1}{\sigma^2} \left\{ k^2 V(\mu^*) + 2kC(\mu^*, \sigma^*) + k^2 V(\sigma^*) \right. \\ \left. + [E(k\mu^* + k\sigma^* - k\mu - k\sigma)]^2 \right\},$$

where $V(\mu^*)$ is the variance of μ^* , $V(\sigma^*)$ is the variance of σ^* , and $C(\mu^*, \sigma^*)$ is the covariance of μ^* and σ^* . Furthermore,

$$\frac{1}{\sigma^2} V(\bar{\varphi}) = \frac{1}{\sigma^2} [k^2 V(\mu^*) + 2kC(\mu^*, \sigma^*) + k^2 V(\sigma^*)]$$

is independent of μ and σ for all θ . Therefore, $V(\mu^*)$, $C(\mu^*, \sigma^*)$, and $V(\sigma^*)$ are of the form $\alpha\sigma^2$, $\beta\sigma^2$, and $\gamma\sigma^2$, respectively, with α and γ positive, and for all μ and σ , either (1) α , β , and γ are all independent of μ and σ , (2) α is independent of μ and σ and $2kC(\mu, \sigma) = -k^2\gamma(\mu, \sigma)$, (3) γ is independent of μ and σ and $2kC(\mu, \sigma) = -k^2\alpha(\mu, \sigma)$ or (4) β is independent of μ and σ and $k^2\alpha(\mu, \sigma) = -k^2\gamma(\mu, \sigma)$. The estimate $\bar{\varphi}$ cannot, of course, be invariant if $V(\bar{\varphi}) = 0$ unless $\bar{\varphi} = k\mu + k\sigma$ for all μ and σ .

One may now make use of the fact that the correlation coefficient of μ^* and σ^* is less than or equal to 1, which implies that $\beta^2 \leq \alpha\gamma$

and hence that $V(\tilde{\varphi})/\sigma^2 \leq \ell^2\alpha + |2\ell k\sqrt{\alpha\gamma}| + k^2\gamma$. Then, since $V(\tilde{\varphi})/\sigma^2$, ℓ , and k are independent of μ and σ for all θ , if α is a constant, so is γ . Conversely, if γ is a constant, so is α . Also, $\ell^2\alpha > 0$ cannot be identically equal to $-k^2\gamma < 0$. Therefore α , β , and γ are all independent of μ and σ for all values of the parameters.

If $R(\varphi, \tilde{\varphi})$ is then minimized with respect to k , and the k which yields the minimum value for $R(\varphi, \tilde{\varphi})$ is substituted into the expression for $\tilde{\varphi}$, the resulting expression defines the best estimate $\tilde{\varphi}$ of φ among invariant estimates based on a given μ^* and σ^* . Since the minimizing k is equal to $(m-\ell\beta)/(1+\gamma)$, $\tilde{\varphi}$ is equal to $\ell\mu^* + [(m-\ell\beta)/(1+\gamma)]\sigma^*$ and $R(\varphi, \tilde{\varphi})$, the expected loss of $\tilde{\varphi}$, is equal to $\ell^2\alpha + 2\ell m\beta + m^2\gamma - (m\gamma + \ell\beta)^2/(1+\gamma)$.

The change in $R(\varphi, \tilde{\varphi})$ induced by changes in α , β , and γ , corresponding to changes in μ^* and σ^* , is now considered. Since $R(\varphi, \tilde{\varphi})$ cannot be negative, it is clearly smallest when α , β , and γ are all zero. Moreover, $\partial R(\varphi, \tilde{\varphi})/\partial\alpha$ is equal to $\ell^2 \geq 0$ and $\partial R(\varphi, \tilde{\varphi})/\partial\gamma$ is equal to $(m-\ell\beta)^2/(1+\gamma)^2 \geq 0$ so that $R(\varphi, \tilde{\varphi})$ is monotonically non-decreasing in both α and γ for fixed β . It can be shown, too, that for $m = 1$, $\ell = 0$ and for $\ell = 1$, $m = 0$, an increase in both α and γ will effect an increase in $R(\varphi, \tilde{\varphi})$, irrespective of any change in β .

Let $m = 1$, $\ell = 0$ so that $\varphi = \sigma$ and $\tilde{\varphi} = \tilde{\sigma}$. Then, since $\partial R(\varphi, \tilde{\varphi})/\partial \beta = 2\ell(m-\ell\beta)/(1+\gamma)$, $R(\sigma, \tilde{\sigma})$ is monotonically increasing in γ , independently of changes in β . $R(\sigma, \tilde{\sigma})$ is also independent of α . Let $m = 0$, $\ell = 1$ so that $\varphi = \mu$ and $\tilde{\varphi} = \tilde{\mu}$. One may now again make use of the fact that $\beta^2 \leq \alpha\gamma$, which implies that $d\beta \leq |(\gamma/2\beta)d\alpha|$ and hence that $|\frac{\partial R}{\partial \beta} d\beta| = |[2\beta/(1+\gamma)]d\beta| \leq [\gamma/(1+\gamma)]|d\alpha|$. Then, $dR(\mu, \tilde{\mu}) \geq d\alpha - [\gamma/(1+\gamma)]|d\alpha| + [\beta^2/(1+\gamma)^2]d\gamma$ or $dR(\mu, \tilde{\mu}) \geq [1-\gamma/(1+\gamma)]d\alpha + [\beta^2/(1+\gamma)^2]d\gamma > 0$ for $d\alpha > 0$ and $d\gamma > 0$. Thus, an increase in both σ and γ induces an increase in $R(\mu, \tilde{\mu})$. Therefore, the expected squared error of $\tilde{\mu}$, any regular invariant estimate of μ , is greater than or equal to $[\sigma^0 - \beta^0/(1+\gamma^0)]\sigma^2$ (where $n\beta^0$ is the asymptotic covariance of $\sqrt{n}\hat{\mu}$ and $\sqrt{n}\hat{\sigma}$), and the mean squared deviation of $\tilde{\sigma}$, any regular invariant estimate of σ , is greater than or equal to $[\gamma^0/(1+\gamma^0)]\sigma^2$, since $\gamma \geq \gamma^0$ and $\alpha \geq \alpha^0$.

In order to apply this result to the parameters of the extreme-value distribution, we let μ be the location parameter x_R (see footnote, p. 12) and σ be the scale parameter b . All regularity conditions are satisfied, and the asymptotic variance of the maximum-likelihood estimate of $\sqrt{n}x_R$ (corresponding to $n\sigma\sigma^2$) is $n[A^0 + 2B^0 \log \log(1/R) + C^0 (\log \log(1/R))^2]b^2$. Likewise, $n[B^0 + C^0 \log \log(1/R)]b^2$ corresponds to $n\beta^0\sigma^2$ and nC^0b^2 corresponds to $n\gamma^0\sigma^2$. Therefore, the expected squared deviations of any regular

Invariant estimates of x_R and of b are less than or equal to

$$\begin{aligned}\tilde{Q}_R^{0,b} &= \left\{ A^0 + 2B^0 \log \log(1/k) + C^0 (\log \log(1/R))^2 \right. \\ &\quad \left. - (B^0 + C^0 \log \log(1/R))^2 / (1+C^0) \right\} b^2 \\ &= \left\{ \tilde{A}^0 + 2\tilde{B}^0 \log \log(1/R) + \tilde{C}^0 (\log \log(1/R))^2 \right\} b^2\end{aligned}$$

and $[C^0/(1+C^0)]b^2 = \tilde{C}^0 b^2$, respectively.

APPENDIX D.2

CRAMER-RAO LOWER BOUNDS FOR ESTIMATES WITH GIVEN BIAS WHEN A NUISANCE PARAMETER IS PRESENT AND THE SAMPLE IS CENSORED

Let Y_1, Y_2, \dots, Y_r be the first r order statistics of a size n random sample chosen from a population with density $f_{\theta}(x)$, where $\theta = (\theta_1, \theta_2)$, and let the joint density of Y_1, Y_2, \dots, Y_r be given by $h_{\theta}(y_1, y_2, \dots, y_r)$. Suppose that all regularity conditions for $f_{\theta}(x)$ are satisfied (see Halperin [4]) so that the maximum-likelihood estimates $\hat{\theta}_1$ and $\hat{\theta}_2$ of θ_1 and θ_2 , respectively, based on Y_1, Y_2, \dots, Y_r , converge in probability to the true values as $n \rightarrow \infty$ with $p = r/n$ fixed. Moreover, the concentration ellipse of the joint asymptotic distribution of $\hat{\theta}_1$ and $\hat{\theta}_2$ lies wholly within the concentration ellipse of any pair of regular unbiased estimates of θ_1 and θ_2 . Under the same conditions, the asymptotic covariance matrix of the maximum-likelihood estimates of $\sqrt{n}\theta_1$ and $\sqrt{n}\theta_2$ is D^{-1} where

$$D = \{d_{i,j}\} = \lim_{\substack{n \rightarrow \infty \\ p \text{ fixed}}} \{\lambda_{i,j}/n\},$$

and

$$\lambda_{i,j} = -E \left[\frac{\partial^2 \log h_{\theta}(y_1, y_2, \dots, y_r)}{\partial \theta_i \partial \theta_j} \right].$$

Regular estimation of θ_1 and θ_2 is defined as in Halperin [4] and Cramér [2]. It is supposed that y_1, y_2, \dots, y_r can be transformed to new variables $\lambda_1, \lambda_2, \dots, \lambda_{r-2}, \bar{\theta}_1, \bar{\theta}_2$ such that

$$h_{\theta}(y_1, y_2, \dots, y_r) \prod_{i=1}^r dy_i \\ = g_{\theta}(\bar{\theta}_1, \bar{\theta}_2) q_{\theta}(\lambda_1, \lambda_2, \dots, \lambda_{r-2} \mid \bar{\theta}_1, \bar{\theta}_2) \prod_{i=1}^{r-2} d\lambda_i d\bar{\theta}_1 d\bar{\theta}_2,$$

where $g_{\theta}(\bar{\theta}_1, \bar{\theta}_2)$ is the joint density function of $\bar{\theta}_1$ and $\bar{\theta}_2$ and $q_{\theta}(\lambda_1, \lambda_2, \dots, \lambda_{r-2} \mid \bar{\theta}_1, \bar{\theta}_2)$ is the conditional density of $\lambda_1, \lambda_2, \dots, \lambda_{r-2}$ given $\bar{\theta}_1$ and $\bar{\theta}_2$. If $\frac{\partial h}{\partial \theta_j}$, $\frac{\partial g}{\partial \theta_j}$, and $\frac{\partial q}{\partial \theta_j}$ exist for every θ_j and if

$\frac{\partial h}{\partial \theta_j} < H_0(y_1, y_2, \dots, y_r), \frac{\partial g}{\partial \theta_j} < G_0(\bar{\theta}_1, \bar{\theta}_2), \frac{\partial q}{\partial \theta_j} < M_0(\lambda_1, \lambda_2, \dots, \lambda_{r-2}, \bar{\theta}_1, \bar{\theta}_2),$
 $j = 1, 2$, where H_0 , $\bar{\theta}_1 G_0$, $\bar{\theta}_2 G_0$, and G_0 ; and M_0 are integrable over the whole space of (y_1, y_2, \dots, y_r) ; $\bar{\theta}_1, \bar{\theta}_2$; and $\bar{\theta}_1, \bar{\theta}_2, \lambda_1, \lambda_2, \dots, \lambda_{r-2}$, respectively, then $\bar{\theta}_1$ and $\bar{\theta}_2$ will be called regular joint estimates of θ_1 and θ_2 .

The variance of any regular unbiased estimate of θ_1 is greater than or equal to $\frac{1}{n} d_{1,1}^{-1}$, the asymptotic variance of $\sqrt{n}\hat{\theta}_1$ (see Cramér, p. 494).

Furthermore, since a reparameterization of $f_{\theta}(x)$ may give $\theta = (\eta(\theta_1, \theta_2), \theta_2)$, the variance of any regular unbiased estimate of

$\eta(\theta_1, \theta_2)$, η nonsingular, is less than that of $\sqrt{n}\eta(\hat{\theta}_1, \hat{\theta}_2)$ for $n \rightarrow \infty$.

It can now be shown that the following is true of the mean squared error (MSE) of $\bar{\theta}_1$, any regular estimate of θ_1 . If $\bar{\theta}_1$ is a regular estimate of θ_1 and the bias of $\bar{\theta}_1$ is $k_1\theta_1$, with k_1 independent of θ , then $MSE(\bar{\theta}_1) \geq \frac{1}{n}(1+k_1)^2 d_{1,1}^{-1} + (k_1 e_1)^2$.

If the bias of $\bar{\theta}_1$ is $k_2\theta_2$, with k_2 independent of θ , then

$$MSE(\bar{\theta}_1) \geq \frac{1}{n}(d_{1,1}^{-1} + 2k_2 d_{1,2}^{-1} + k_2^2 d_{2,2}^{-1}) + (k_2 \theta_2)^2.$$

Proof:

If $\bar{\theta}_1$ has bias $k_1\theta_1$, then $E(\bar{\theta}_1) = \theta_1 + k_1\theta_1 = (1+k_1)\theta_1$. If a re-parameterization is made so that $\theta = ((1+k_1)\theta_1, \theta_2)$, then, since $h_{\theta_1, \theta_2}(y_1, y_2, \dots, y_r) = h_{(1+k_1)\theta_1, \theta_2}(y_1, y_2, \dots, y_r)$, $\sqrt{n}\bar{\theta}_1$ is by definition a regular unbiased estimate of $\sqrt{n}(1+k_1)\theta_1$ with variance greater than or equal to the variance of the maximum-likelihood estimate of $\sqrt{n}(1+k_1)\theta_1$ as $n \rightarrow \infty$, p fixed.

If $\bar{\theta}_1$ has bias $k_2\theta_2$, then $E(\bar{\theta}_1) = \theta_1 + k_2\theta_2$ and $\sqrt{n}\bar{\theta}_1$ is a regular unbiased estimate of $\sqrt{n}(\theta_1 + k_2\theta_2)$ with variance greater than or equal to the maximum-likelihood estimate of this parametric function of θ_1 and θ_2 as $n \rightarrow \infty$, p fixed. Then since the maximum-likelihood estimate of $c_1\theta_1 + c_2\theta_2$ is $c_1\hat{\theta}_1 + c_2\hat{\theta}_2$, with variance $c_1^2 \text{Var}(\hat{\theta}_1) + 2c_1c_2 \text{Cov}(\hat{\theta}_1, \hat{\theta}_2) + c_2^2 \text{Var}(\hat{\theta}_2)$, $MSE(\bar{\theta}_1) \geq \frac{1}{n}(1+k_1)^2 d_{1,1}^{-1} + (k_1 e_1)^2$

when $E(\bar{\theta}_1) = (1+k_1)\theta_1$, and $MSE(\bar{\theta}_1) \geq \frac{1}{n}(d_{1,1}^{-1} + 2k_2 d_{1,2}^{-1} + k_2^2 d_{2,2}^{-1}) + (k_2\theta_2)^2$
when $E(\bar{\theta}_1) = \theta_1 + k_2\theta_2$.

It should be noted that this result agrees with one concerning more general forms of bias, which could be fairly directly derived for the uncensored case on the basis of a lemma of Hodges appearing in [6]. If this derivation is made for the case of a single unknown parameter ($\theta = \theta_1$, with $E(\bar{\theta}_1) = \theta + \text{bias}$ as it is in [5] for a Gaussian distribution with unknown σ , the bound obtained is larger than that given by Cramér in [2] for the single-parameter case.

For the problem considered in this paper all regularity conditions are satisfied. The parameter point $\theta = (\theta_1, \theta_2)$ is given by $\theta_1 = x_R = u + b \log \log(1/R)$ and $\theta_2 = b$, and the prescribed bias is $[-(B+C \log \log(1/R)/(1+C)) b \equiv k_2 b]$, with k_2 a function of R, r , and n .

The covariance matrix $\frac{1}{n}D^{-1}$ for joint efficient estimates of x_R and b is

$$\begin{bmatrix} [A^0 + 2B^0 \log \log(1/k) + C^0 \log^2 \log(1/R)]b^2 & [B^0 + C^0 \log \log(1/R)]b^2 \\ [B^0 + C^0 \log \log(1/R)]b^2 & C^0 b^2 \end{bmatrix}$$

Thus, the Cramér-Rao lower bound for mean squared error of estimates

of x_R with bias $k_2 b$, is

$$\left\{ A^0 - \frac{2BB^0(1+C)-B^2(1+C^0)}{(1+C)^2} + \right.$$
$$\left. \frac{2[B^0(1+C)+B(C-C^0)]\log\log(1/R)}{(1+C)^2} + \frac{(C^0+C^2)(\log\log(1/R))^2}{(1+C)^2} \right\} b^2$$

Likewise, the corresponding bound for estimates of $b(\theta_1=b, \theta_2=x_R)$ with bias $[-C/(1+C)]b = k_1 b$ is $[(C^0+C^2)/(1+C)^2]b^2$.

Table D.I - Factors for Calculating Cramér-Rao Efficiencies of BLI Estimates of a Scale Parameter
 and $100(1-R)$ Percent Points of the Extreme-Value Distribution, $R = e^{-1}$, .90, .99,
 Where $\frac{1-R}{n}$ of the Size n Ordered Sample is Censored From Above, $2 \leq n \leq 25$, $2 \leq r \leq n$

n	r	\tilde{A}	\tilde{A}^0	\tilde{B}	\tilde{B}^0	\tilde{C}	\tilde{C}^0	\tilde{Q}	\tilde{Q}^0	$\tilde{\alpha}_{.90}$	$\tilde{\alpha}_{.99}$	$\tilde{\alpha}^0_{.90}$	$\tilde{\alpha}^0_{.99}$
2	2	0.657130	0.541667	0.037574	-0.098554	0.419839	0.233107	2.593897	2.165725	~ 1.1166	6.381769		
3	2	0.795461	0.510573	0.257510	0.054913	0.450055	0.285418	1.915628	1.703733	7.950090	6.045004		
3	3	0.4c2407	0.363452	-0.019422	-0.071238	0.256346	0.169498	1.783475	1.537773	5.996531	6.5114505		
4	2	1.014778	0.589262	0.413509	0.163705	0.464388	0.300232	1.505415	1.372892	7.037457	5.434456		
3	3	0.423151	0.333607	0.084776	0.007460	0.281729	0.203175	1.468327	1.328941	5.604971	4.504433		
4	4	0.292477	0.273587	-0.024312	-0.055778	0.183862	0.131931	1.351007	1.192743	4.443778	3.578594		
5	2	1.249210	0.698349	0.531791	0.247140	0.472308	0.307934	1.238599	1.145458	6.332866	4.90881		
3	3	0.490293	0.356132	0.166129	0.070080	0.294192	0.215413	1.212423	1.131607	5.187363	4.259817		
4	4	0.290628	0.250441	0.030763	-0.008114	0.202419	0.155572	1.17251	1.080758	4.291067	3.640222		
5	5	0.230605	0.219377	-0.029135	-0.045832	0.147843	0.108405	1.084913	0.974634	3.521210	2.915063		
6	2	1.481024	0.816546	0.631490	0.314617	0.47731	0.312700	1.056183	0.984097	5.772317	4.519131		
3	3	0.575395	0.399459	0.232697	0.121273	0.301733	0.222413	1.056108	0.979975	4.819592	3.902427		
4	4	0.315521	0.256166	0.087351	0.032039	0.212423	0.165465	1.021624	0.954972	4.071425	3.4146726		
5	5	0.223513	0.201595	0.006880	-0.014225	0.15905	0.126963	0.974138	0.980722	3.462147	3.017064		
6	6	0.190304	0.183111	-0.027716	-0.038896	0.116577	0.092009	0.905408	0.824072	2.912221	2.487806		
7	2	1.704680	0.936056	0.713666	0.371176	0.480823	0.3115950	0.927623	0.865509	5.313623	4.207061		
3	3	0.667587	0.452168	0.269854	0.164384	0.306813	0.227011	0.921279	0.852136	4.572628	3.743849		
4	4	0.243402	0.275604	0.122678	0.066457	0.218847	0.172496	0.909847	0.850044	3.956465	3.344355		
5	5	0.233167	0.201413	0.042126	0.013809	0.164973	0.134916	0.879020	0.822600	3.336558	2.929802		
6	6	0.182699	0.169194	-0.001301	-0.016396	0.127606	0.105382	0.834770	0.761725	2.894708	2.571217		
7	7	0.162191	0.157140	-0.025789	-0.033783	0.098365	0.079907	0.776397	0.713852	2.480999	2.148902		
8	2	1.916115	1.053689	0.784533	0.419816	0.483377	0.319312	0.835533	0.776196	4.929591	3.927166		
3	3	0.761587	0.509725	0.337341	0.201542	0.310477	0.230278	0.816007	0.768871	4.229463	3.578477		
4	4	0.398C56	0.302514	0.159281	0.096310	0.223358	0.176631	0.812293	0.763516	3.659187	3.141464		
5	5	0.251921	0.210552	0.071292	0.038447	0.170378	0.140089	0.793878	0.746945	3.201659	2.921310		
6	6	0.185598	0.164819	0.022472	0.004152	0.134224	0.113074	0.754590	0.720759	2.819615	2.521431		
7	7	0.155051	0.146009	-0.005413	-0.016979	0.107264	0.091458	0.727116	0.685586	2.483909	2.217605		
8	8	0.141360	0.137624	-0.023866	-0.029859	0.085017	0.070624	0.679311	0.629666	2.160004	1.906837		
9	2	2.122722	1.168113	0.846804	0.462458	0.485330	0.320106	0.769266	0.707781	4.602115	3.6117256		

Table D.I (continued)

n	r	λ	\tilde{A}	\tilde{B}	\tilde{B}^0	\tilde{C}	\tilde{C}^0	\tilde{Q}	\tilde{Q}^0	Q	Q^0
3	0.856217	0.568929	0.379959	0.234151	0.313246	0.732774	0.732451	0.693619	0.889204	3.319422	3.007596
4	0.446256	0.333664	0.191609	0.122602	0.226713	0.173667	0.731980	0.691703	0.480962	3.007596	3.007596
5	0.276050	0.225294	0.097154	0.060297	0.174294	0.143739	0.721440	0.691829	0.070514	2.712254	2.712254
6	0.195796	0.171019	0.043783	0.022614	0.138801	0.117496	0.701653	0.664759	0.730209	2.449346	2.449346
7	0.155472	0.142875	0.011395	-0.0011303	0.112788	0.097192	0.675362	0.640431	0.437388	2.209473	2.209473
8	0.134568	0.128541	-0.020969	-0.016845	0.092364	0.080125	0.643529	0.610124	0.172946	1.979495	1.979495
9	0.125295	0.122421	-0.022094	-0.026751	0.074324	0.063273	0.603659	0.563247	1.911954	1.707493	1.707493
10	2	2.317441	1.274815	0.902322	0.500402	0.486871	0.321517	0.721920	0.654849	4.318679	3.478710
11	2	0.949C76	0.628545	0.417951	0.263181	0.315415	0.234626	0.665298	0.63219	3.778412	3.17226
12	2	0.456157	0.367223	0.220478	0.146098	0.229309	0.161987	0.645139	0.631462	3.320224	2.874511
13	2	0.303445	0.243550	0.120331	0.079870	0.177275	0.146480	0.659619	0.625873	2.947760	2.608416
14	2	0.209738	0.179442	0.062298	0.039269	0.142198	0.120708	0.646313	0.613982	2.639246	2.372440
15	2	0.160661	0.144537	0.027627	0.013021	0.116706	0.107917	0.627333	0.596994	2.376135	2.160218
16	2	0.134036	0.125239	0.004750	-0.004510	0.097049	0.084935	0.604125	0.575665	2.144009	1.964016
17	2	0.119657	0.114879	-0.010439	-0.016385	0.081004	0.071240	0.576856	0.549392	1.929854	1.773149
18	2	0.112522	0.110444	-0.024229	-0.027509	0.066793	0.057309	0.543073	0.509513	1.714628	1.5458612
19	2	2.503400	1.385672	0.952399	0.534571	0.488120	0.322655	0.688620	0.613693	4.077337	3.295294
20	2	1.C29956	0.687812	0.452207	0.289327	0.317159	0.236149	0.610433	0.581526	3.023166	3.023166
21	2	0.546820	0.402057	0.245536	0.167212	0.231380	0.181928	0.608972	0.580457	3.174938	2.753762
22	2	0.328228	0.264051	0.141299	0.097568	0.179627	0.149622	0.606576	0.577570	2.833985	2.511448
23	2	0.226409	0.190689	0.087450	0.054395	0.144934	0.123168	0.597787	0.569612	2.551136	2.296637
24	2	0.169457	0.149433	0.042460	0.026121	0.119670	0.103752	0.583381	0.557298	2.317788	2.104655
25	2	0.136694	0.125541	0.017512	0.006912	0.100438	0.08873	0.566558	0.541461	2.100976	1.929932
26	2	0.118C94	0.111660	0.000594	-0.006435	0.985031	0.075198	0.546077	0.5227451	1.912100	1.766389
27	2	0.107564	0.1C186	-0.011097	-0.015782	0.072072	0.064295	0.522494	0.499503	1.734804	1.605419
28	2	0.102120	0.10C270	-0.019102	-0.022142	0.060304	0.052372	0.493479	0.465144	1.5533971	1.412241
29	2	2.681270	1.488744	0.997998	0.565642	0.489152	0.323593	0.666682	0.581665	3.850507	3.132364
30	2	1.128571	0.746274	0.483337	0.313099	0.318594	0.237396	0.566382	0.539313	3.423147	2.989310
31	2	0.557480	0.437675	0.270268	0.186462	0.230702	0.185125	0.561389	0.5369C6	3.043061	2.643942
32	2	0.363386	0.285989	0.160426	0.113712	0.181531	0.150346	0.560657	0.535674	2.72878	2.421471
33	2	0.244901	0.203966	0.096640	0.068224	0.146945	0.125121	0.555128	0.531442	2.467467	2.221921
34	2	0.175679	0.156593	0.056C79	0.038150	0.122006	0.105955	0.545139	0.521463	2.245549	2.047843
35	2	0.141866	0.128363	0.029301	0.017474	0.103043	0.097879	0.531A15	0.509488	2.052822	1.889820
36	2	0.119300	0.111217	0.010873	0.002816	0.087994	0.078335	0.515978	0.494975	1.881316	1.742441
37	2	0.105732	0.100852	-0.002108	-0.007594	0.075575	0.067727	0.497941	0.478014	1.724395	1.6n1928
38	2	0.097752	0.094840	-0.011349	-0.015130	0.064873	0.059229	0.477356	0.457815	1.574960	1.456240
39	2	0.093484	0.091952	-0.017855	-0.020386	0.054954	0.049218	0.452143	0.4278H6	1.420669	1.299863
40	2	2.851697	1.588181	1.039851	0.594124	0.490018	0.324379	0.653132	0.556893	3.654220	2.986373
41	2	2.214809	0.803682	0.511988	0.334886	0.319794	0.239437	0.529969	0.503031	3.271636	2.768285
42	2	0.647783	0.473311	0.292046	0.204114	0.16567	0.520808	0.499452	0.422805	2.922805	2.543413

Table D.I (continued)

n	r	\tilde{A}	\tilde{B}	\tilde{C}	\tilde{D}	\tilde{Q}^0							
5	0.394596	0.308826	0.177997	0.178515	0.183107	0.151765	0.520760	0.493979	0.520760	0.493979	0.520760	0.493979	0.520760
6	0.264610	0.216375	0.111099	0.090946	0.166678	0.126713	0.517508	0.495757	0.517508	0.495757	0.517508	0.495757	0.517508
7	0.1651673	0.165371	0.068667	0.049250	0.123901	0.107735	0.510365	0.489755	0.510365	0.489755	0.510365	0.489755	0.510365
8	0.148850	0.130111	0.040225	0.07262	0.105124	0.042774	0.500174	0.480133	0.500174	0.480133	0.500174	0.480133	0.500174
9	0.1227503	0.12771	0.020463	0.011565	0.090302	0.080581	0.487707	0.468795	0.487707	0.468795	0.487707	0.468795	0.487707
10	0.1066718	0.105000	0.006357	0.000136	0.078198	0.070331	0.473422	0.455568	0.473422	0.455568	0.473422	0.455568	0.473422
11	0.095836	0.092025	-0.003882	-0.008278	0.067951	0.061433	0.457474	0.440387	0.457474	0.440387	0.457474	0.440387	0.457474
12	0.085619	0.076197	0.07262	-0.011361	0.058952	0.053371	0.439298	0.42477	0.439298	0.42477	0.439298	0.42477	0.439298
13	0.066197	0.084968	-0.016749	-0.018889	0.050470	0.044674	0.417168	0.396155	0.417168	0.396155	0.417168	0.396155	0.417168
14	2	3.015280	1.684168	1.078521	0.620412	0.490757	0.325048	0.646410	0.537950	0.646410	0.537950	0.646410	0.537950
	3	1.258650	0.859960	0.5396401	0.354989	0.320813	0.239318	0.500162	0.474133	0.500162	0.474133	0.500162	0.474133
	4	0.697482	0.508931	0.312161	0.220407	0.235672	0.197613	0.496007	0.467042	0.496007	0.467042	0.496007	0.467042
	5	0.426096	0.332201	0.194239	0.142200	0.184433	0.152955	0.485874	0.466785	0.485874	0.466785	0.485874	0.466785
	6	0.265120	0.233805	0.124694	0.092716	0.150126	0.128039	0.484164	0.454922	0.484164	0.454922	0.484164	0.454922
	7	0.205184	0.175323	0.080303	0.059542	0.125473	0.109193	0.479179	0.450339	0.479179	0.450339	0.479179	0.450339
	8	0.157165	0.139010	0.052982	0.036365	0.106830	0.094389	0.471417	0.453411	0.471417	0.453411	0.471417	0.453411
	9	0.127191	0.115813	0.029417	0.019650	0.092166	0.082373	0.461534	0.443897	0.461534	0.443897	0.461534	0.443897
	10	0.106035	0.100758	0.014307	0.007404	0.080248	0.072349	0.450028	0.43822	0.450028	0.43822	0.450028	0.43822
	11	0.095665	0.090956	0.003201	-0.001762	0.070275	0.063731	0.437146	0.421794	0.437146	0.421794	0.437146	0.421794
	12	0.087717	0.084666	-0.005064	-0.093659	0.061682	0.056179	0.422676	0.408139	0.422676	0.408139	0.422676	0.408139
	13	0.082762	0.080817	-0.011233	-0.013838	0.054011	0.049179	0.406790	0.392149	0.406790	0.392149	0.406790	0.392149
	14	0.0793967	0.078867	-0.015764	-0.017595	0.0466657	0.041616	0.387194	0.368807	0.387194	0.368807	0.387194	0.368807
15	2	3.172565	1.776903	1.114456	0.6444817	0.491393	0.325523	0.645184	0.523758	0.645184	0.523758	0.645184	0.523758
	3	1.380159	0.914668	0.562932	0.373646	0.321689	0.240714	0.475634	0.44958	0.475634	0.44958	0.475634	0.44958
	4	0.746429	0.54285	0.37844	0.215531	0.2366692	0.188508	0.456035	0.438160	0.456035	0.438160	0.456035	0.438160
	5	0.457646	0.355861	0.209333	0.154911	0.185564	0.153967	0.455220	0.438158	0.455220	0.438158	0.455220	0.438158
	6	0.306140	0.249862	0.137341	0.103661	0.151356	0.129160	0.454492	0.437357	0.454492	0.437357	0.454492	0.437357
	7	0.219292	0.186129	0.091160	0.069126	0.126799	0.110423	0.451135	0.434213	0.451135	0.434213	0.451135	0.434213
	8	0.164466	0.146023	0.059864	0.044861	0.108259	0.095731	0.445271	0.426919	0.445271	0.426919	0.445271	0.426919
	9	0.1433001	0.119985	0.037798	0.027277	0.093708	0.081845	0.437475	0.421823	0.437475	0.421823	0.437475	0.421823
	10	0.111219	0.102740	0.021778	0.014237	0.081326	0.073974	0.428088	0.413279	0.428088	0.413279	0.428088	0.413279
	11	0.066811	0.091205	0.003895	0.004404	0.072125	0.065581	0.417529	0.403496	0.417529	0.403496	0.417529	0.403496
	12	0.087233	0.083498	0.007946	-0.003094	0.063764	0.058773	0.405886	0.397530	0.405886	0.397530	0.405886	0.397530
	13	0.080922	0.078435	-0.005852	-0.008842	0.056441	0.051732	0.393087	0.382101	0.393087	0.382101	0.393087	0.382101
	14	0.076897	0.075267	-0.011021	-0.013212	0.049802	0.0456119	0.378709	0.3658645	0.378709	0.3658645	0.378709	0.3658645
	15	0.074578	0.073629	-0.014882	-0.016467	0.043376	0.036950	0.361223	0.344992	0.361223	0.344992	0.361223	0.344992
16	2	3.274042	1.866582	1.146015	0.667589	0.491948	0.326124	0.644429	0.513462	0.644429	0.513462	0.644429	0.513462
	3	1.459384	0.969564	0.585828	0.391049	0.322450	0.240730	0.455667	0.427651	0.455667	0.427651	0.455667	0.427651
	4	0.794533	0.579246	0.348282	0.249640	0.237577	0.183281	0.430136	0.414232	0.430136	0.414232	0.430136	0.414232
	5	0.489080	0.379630	0.223426	0.166774	0.186542	0.154939	0.426174	0.413151	0.426174	0.413151	0.426174	0.413151
	6	0.327462	0.2663338	0.149158	0.113883	0.152613	0.130121	0.427986	0.412732	0.427986	0.412732	0.427986	0.412732

Table D.I (continued)

n	r	λ	A^0	\tilde{B}	B^0	\tilde{C}	C^0	\tilde{Q}	$Q_{.90}$	$\tilde{Q}_{.90}$	$Q_{.99}$	$\tilde{Q}_{.99}$
7	0	233962	0.197559	0.101317	0.078089	0.127935	0.111476	0.425841	0.410632	0.099087	0.838101	1.717763
8	0	176502	0.153801	0.063748	0.052820	0.109474	0.096871	0.421479	0.406641	0.850618	1.408874	1.730071
9	0	139668	0.125027	0.046646	0.034609	0.095010	0.085084	0.415241	0.401021	0.613600	1.509374	1.613600
10	0	115350	0.105673	0.025811	0.020672	0.083327	0.075321	0.407664	0.394070	0.386015	1.508117	1.617414
11	0	958579	0.092471	0.016221	0.010235	0.073645	0.057061	0.398923	0.386015	0.386015	1.31270	1.412942
12	0	807840	0.083414	0.006658	0.002700	0.065435	0.05925	0.389248	0.366982	0.366982	1.249183	1.320694
13	0	680253	0.077227	-0.000690	-0.004038	0.058318	0.053626	0.379691	0.366971	0.366971	1.168996	1.236107
14	0	675244	0.073080	-0.005373	-0.008896	0.051997	0.047921	0.367148	0.355797	0.355797	1.086989	1.149451
15	0	671822	0.071436	-0.010763	-0.012662	0.046198	0.042533	0.354214	0.342818	0.342818	0.986030	0.986030
16	0	69043	0.069043	-0.014090	-0.015466	0.040524	0.036605	0.339505	0.324067	0.324067	0.986030	0.986030
17	2	3.470154	1.951397	1.179497	0.688931	0.497435	0.326564	0.555343	0.506466	0.039086	2.525559	2.379460
18	3	1.536424	1.022943	0.607291	0.407353	0.323118	0.241304	0.439488	0.405612	2.786790	2.216105	2.530904
19	4	0.841748	0.613738	0.364627	0.262858	0.238351	0.193954	0.407704	0.392652	2.305944	2.059385	2.305944
20	5	0.520284	0.403381	0.216640	0.177893	0.187394	0.155594	0.404224	0.390707	2.378645	2.119384	2.119384
21	6	0.348935	0.283079	0.160244	0.123470	0.153333	0.137955	0.404222	0.390549	1.918304	1.791735	1.918304
22	7	0.249022	0.209440	0.110854	0.086502	0.128918	0.112381	0.407959	0.389232	1.957215	1.677088	1.816533
23	8	0.187087	0.142160	0.077098	0.060299	0.110521	0.097948	0.399792	0.386266	1.816533	1.576117	1.677088
24	9	0.146994	0.130765	0.053074	0.04123	0.096125	0.084134	0.394914	0.381855	1.692817	1.491276	1.592620
25	10	0.126222	0.109154	0.035446	0.026742	0.084518	0.076454	0.388700	0.376189	1.483124	1.394857	1.483124
26	11	0.101951	0.094542	0.022205	0.015752	0.074923	0.069296	0.381431	0.369559	1.361966	1.316391	1.361966
27	12	0.089306	0.04187	0.012092	0.007231	0.066819	0.061278	0.373307	0.361278	1.307710	1.239497	1.307710
28	13	0.080496	0.076929	0.004239	0.005556	0.059836	0.055132	0.364436	0.351625	1.228141	1.165777	1.228141
29	14	0.074368	0.071875	-0.001893	-0.004707	0.053700	0.047644	0.354631	0.344662	1.151527	1.094194	1.151527
30	15	0.070165	0.063427	-0.005708	-0.008864	0.048184	0.044620	0.344368	0.342923	1.122495	1.020686	1.122495
31	16	0.067383	0.056192	-0.010479	-0.012128	0.043071	0.039333	0.332655	0.324595	0.929984	0.929984	0.929984
32	17	0.065722	0.064995	-0.013375	-0.014597	0.018021	0.034526	0.318466	0.305636	0.929984	0.929984	0.929984
33	2	3.411296	2.037522	1.2209127	0.790011	0.492867	0.326953	0.665289	0.502189	2.435176	2.104696	2.688413
34	3	1.611373	1.072193	0.627488	0.422688	0.323709	0.241812	0.426524	0.394159	2.167296	2.050161	2.373687
35	4	0.888051	0.647711	0.387007	0.275290	0.239034	0.197552	0.388245	0.370656	2.241014	2.070918	2.070918
36	5	0.551180	0.427027	0.249075	0.188352	0.188145	0.156265	0.382952	0.370656	1.957639	1.91958	1.91958
37	6	0.370449	0.299972	0.170682	0.132493	0.154141	0.131585	0.382849	0.370531	1.908077	1.747755	1.908077
38	7	0.264342	0.221643	0.09426	0.119838	0.112978	0.111371	0.392194	0.369772	1.867619	1.774384	1.867619
39	8	0.158079	0.170961	0.084973	0.0611433	0.07351	0.096967	0.379953	0.367619	1.610988	1.542305	1.610988
40	9	0.154829	0.136990	0.069068	0.047462	0.097092	0.037066	0.376167	0.364193	1.656785	1.552062	1.656785
41	10	0.125678	0.113626	0.041720	0.032483	0.085544	0.077434	0.371113	0.359570	1.453395	1.453395	1.453395
42	11	0.105764	0.097257	0.027976	0.020990	0.076015	0.069346	0.365054	0.340799	1.457694	1.371693	1.457694
43	12	0.091459	0.085645	0.017236	0.012013	0.067999	0.062415	0.358191	0.347658	1.371623	1.295909	1.371623
44	13	0.081467	0.077354	0.008940	0.004940	0.061101	0.056375	0.357655	0.346193	1.292700	1.226875	1.292700
45	14	0.074363	0.071438	0.002403	-0.000685	0.055096	0.051029	0.342510	0.329199	1.217947	1.157459	1.217947
46	15	0.069333	0.067247	-0.002784	-0.005180	0.049736	0.046194	0.333717	0.324497	1.147449	1.092447	1.147449
47	16	0.065825	0.064345	-0.006912	-0.008874	0.044879	0.041735	0.324209	0.315185	1.079117	1.020713	1.079117
48	17	0.063468	0.062434	-0.010185	-0.011629	0.040334	0.037451	0.304429	0.304429	1.010489	0.961910	1.010489

Table R I (continued)

n	r	A	A ⁰	R	B ⁰	C	E ⁰	\bar{A}	\bar{q}^0	\bar{q}^0	\bar{q}^0	\bar{q}^0	\bar{q}^0
18		0.062040	0.061395	-0.012727	-0.013813	0.035818	0.0132670	0.3006670	0.2870709	0.2936881	0.2748274	0.2748274	0.2748274
19	2	3.747823	2.119125	1.237124	0.727969	0.493252	0.327370	0.677759	0.507225	0.601803	2.147771	2.147771	2.147771
3	1.684328	1.122183	0.646559	0.437160	0.324275	0.242263	0.4163C9	0.381498	0.597034	2.226795	2.226795	2.226795	2.226795
4	0.933439	0.681137	0.394527	0.287022	0.239641	0.191080	0.371356	0.356545	2.374907	2.083796	2.083796	2.083796	2.083796
5	0.581713	0.450502	0.267817	0.198274	0.188111	0.154856	0.364011	0.352691	2.177511	1.945069	2.177511	1.945069	2.177511
6	0.391921	0.316930	0.185540	0.141012	0.154855	0.122330	0.163571	0.152616	2.007854	1.819871	2.007854	1.819871	2.007854
7	0.279825	0.234070	0.124329	0.101913	0.130537	0.113867	0.363311	0.352029	1.861508	1.706037	1.861508	1.706037	1.861508
8	0.2C9169	0.18C055	0.092420	0.074019	0.112236	0.099442	0.361790	0.357548	1.734142	1.603441	1.734142	1.603441	1.734142
9	0.163059	0.143649	0.066689	0.053461	0.097939	0.037840	0.359887	0.347869	1.622026	1.510670	1.622026	1.510670	1.622026
10	0.131597	0.116771	0.047667	0.037923	0.064438	0.079283	0.1546706	0.144125	1.522197	1.426040	1.522197	1.426040	1.522197
11	0.109693	0.10C490	0.032661	0.025944	0.076962	0.070253	0.149747	0.132493	1.42318	1.348447	1.42318	1.348447	1.42318
12	0.C94167	0.087661	0.022139	C.016562	0.068995	0.063187	0.3423931	0.334127	1.276543	1.276543	1.276543	1.276543	1.276543
13	0.083028	0.078172	0.013424	0.009123	0.062177	0.0557424	0.337487	0.32A170	1.209619	1.209619	1.209619	1.209619	1.209619
14	0.074580	0.071621	0.006515	0.031348	0.056247	0.052164	0.330501	0.321549	1.295307	1.146419	1.295307	1.146419	1.295307
15	0.C69158	0.666723	0.001692	-0.001630	0.051008	0.047663	0.323071	0.314622	1.396119	1.246119	1.396119	1.246119	1.396119
16	0.C64570	0.632073	-0.003448	-0.005510	0.063001	0.043180	0.314961	0.305673	1.076475	1.027648	1.076475	1.027648	1.076475
17	0.062007	0.060731	-0.007C23	-0.C08647	0.241987	0.039192	0.306244	0.299123	1.015125	0.959646	1.015125	0.959646	1.015125
18	0.055588	0.059082	-0.009889	-0.011163	0.037918	0.035334	0.295518	0.299254	0.953366	0.907059	0.953366	0.907059	0.953366
19	0.0581749	0.059173	-0.012138	-0.013108	0.033837	0.031004	0.264733	0.274179	0.8164962	0.8164962	0.8164962	0.8164962	0.8164962
20	2	3.880054	2.198359	1.263654	0.745922	0.493598	0.327610	0.492338	0.500230	2.683339	2.683339	2.683339	2.683339
3	1.755385	1.171007	0.664622	0.450361	0.324706	0.242667	0.408459	0.370703	2.511807	2.149116	2.511807	2.149116	2.511807
4	0.977919	0.713999	0.409277	0.293128	0.240184	0.191552	0.356707	0.342256	2.364297	2.072664	2.364297	2.072664	2.364297
5	0.611848	0.473760	0.209137	0.207570	0.194045	0.157383	0.171111	0.136555	2.190029	1.904493	2.190029	1.904493	2.190029
6	0.413294	0.338945	0.182879	0.149080	0.155493	0.132975	0.136139	0.335971	1.774758	1.664472	1.774758	1.664472	1.774758
7	0.295395	0.246644	0.13212	0.109075	0.11212	0.114485	0.346085	0.335810	1.817346	1.696472	1.817346	1.696472	1.817346
8	0.22C073	0.189479	0.093492	0.080340	0.112949	0.101012	0.345115	0.324923	1.605738	1.548626	1.605738	1.548626	1.605738
9	0.171590	0.150630	0.072972	0.059153	0.098688	0.088541	0.142932	0.132786	1.594595	1.480055	1.594595	1.480055	1.594595
10	0.137883	C.123496	0.053316	0.043091	0.097226	0.079028	0.339645	0.329765	1.491175	1.390185	1.491175	1.390185	1.491175
11	0.114237	0.174145	0.038381	0.030665	0.077792	0.071044	0.335446	0.325909	1.407307	1.325444	1.407307	1.325444	1.407307
12	0.C57330	0.090131	0.0248C9	0.020875	0.067872	0.054230	0.305111	0.302137	1.329267	1.257095	1.329267	1.257095	1.329267
13	0.C5074	0.079872	0.017704	0.013116	0.062107	-0.058127	0.316216	0.297631	1.193474	1.137474	1.193474	1.137474	1.193474
14	0.C76108	0.072313	0.010451	0.006856	0.057241	0.053140	0.319866	0.309563	1.191265	1.137474	1.191265	1.137474	1.191265
15	0.C65519	0.666732	0.004619	0.001781	0.052079	0.043522	0.312464	0.304435	1.129077	1.077126	1.129077	1.077126	1.129077
16	0.064679	0.626225	-0.002103	-0.002355	0.047471	0.044151	0.305545	0.297942	1.070185	1.022826	1.070185	1.022826	1.070185
17	0.061149	0.C59435	-0.001943	-0.005735	0.043295	0.041524	0.298147	0.270670	1.013603	0.969952	1.013603	0.969952	1.013603
18	0.C58619	0.57509	-0.007047	-0.008495	0.039437	0.036936	0.240141	0.242124	0.922127	0.862456	0.922127	0.862456	0.922127
19	0.056874	0.754074	-G.009596	-0.010730	0.035771	0.033441	0.291214	0.273718	0.841162	0.794273	0.841162	0.794273	0.841162
20	0.0551790	0.015273	-0.011599	-0.012472	0.032070	0.029500	0.270405	0.260797	0.794273	0.741596	0.794273	0.741596	0.794273
21	2	4.CC8276	2.275345	1.268861	0.762972	0.693910	0.327991	0.708699	0.501921	2.194419	2.672178	2.194419	2.672178
3	1.824638	1.718708	0.691776	0.463964	0.325131	0.243031	0.402656	0.3617C7	2.612109	2.093851	2.612109	2.093851	2.612109
4	1.C21506	0.746293	0.421334	0.308669	0.240674	0.191977	0.344003	0.329256	1.968936	1.968936	1.968936	1.968936	1.968936

Table D.I (continued)

n	r	\tilde{A}	\tilde{A}^0	\tilde{B}	\tilde{B}^0	\tilde{C}	\tilde{C}^0	\tilde{Q}	\tilde{Q}^0	\tilde{Q}^{*0}	\tilde{Q}^{*0}	\tilde{Q}^{*0}	\tilde{Q}^{*0}
5	0.441562	0.496771	0.282496	0.213642	0.199940	0.157954	0.332008	0.322030	0.320190	2.061904	1.845949		
6	0.434621	0.350804	0.193748	0.156740	0.156064	0.134619	0.330361	0.321046	1.908510	1.732087			
7	0.310996	0.255309	0.140200	0.115747	0.113617	0.115077	0.330340	0.320949	1.753933	1.629787			
8	0.272526	0.190470	0.106195	0.096377	0.113583	0.107960	0.329776	0.327332	1.659085	1.535369			
9	0.180354	0.157465	0.079469	0.064566	0.093555	0.089165	0.329174	0.319812	1.556487	1.450691			
10	0.144661	0.128926	0.051694	0.048009	0.087925	0.079689	0.325560	0.316367	1.465071	1.373524			
11	0.119117	0.108144	0.041260	0.031563	0.078525	0.071742	0.322281	0.313198	1.382821	1.302801			
12	0.11264	0.092777	0.031265	0.025431	0.070643	0.064760	0.317896	0.309338	1.308121	1.237541			
13	0.087520	0.081773	0.021794	0.016912	0.063921	0.059113	0.313137	0.304922	1.239666	1.176902			
14	0.077660	0.073528	0.014220	0.010386	0.058103	0.051980	0.307902	0.300031	1.176371	1.120130			
15	0.070325	0.067184	0.008101	0.005058	0.052999	0.049425	0.302258	0.294715	1.117117	1.066547			
16	0.064853	0.062510	0.003119	0.000698	0.048462	0.045333	0.296236	0.288995	1.041684	1.015566			
17	0.060780	0.059028	0.002913	0.002913	0.043777	0.041609	0.281835	0.282854	0.966337	0.967529	0.918263		
18	0.057771	0.056462	0.004312	0.005833	0.046644	0.039168	0.281006	0.276225	0.965658	0.970167	0.917182	0.919092	
19	0.055591	0.054618	0.007063	0.008328	0.037172	0.034927	0.275425	0.269550	0.956058	0.956058	0.956058	0.956058	
20	0.054670	0.053359	0.011106	-0.011106	0.010325	0.033851	0.311739	0.267400	0.956058	0.956058	0.956058	0.956058	
21	0.053114	0.052648	-0.011106	-0.011106	0.011815	0.0316478	0.028134	0.257446	0.920256	0.757447	0.757447	0.757447	
22	2	4.132751	2.350272	1.212872	0.779201	0.494493	0.324645	0.72532	0.55562	2.511736	2.175371		
23	2	1.892175	1.265330	0.691069	0.716747	0.325516	0.243640	0.398635	0.254293	2.033556	2.033556		
	3	1.064221	0.78070	0.431762	0.18701	0.241116	0.192161	0.31022	0.317776	2.175829	1.916463		
	4	0.670841	0.519511	0.292547	0.224895	0.190423	0.159283	0.314955	0.305913	2.089334	1.796686		
	5	0.455570	0.367635	0.207197	0.14031	0.155880	0.138830	0.319977	0.307377	1.827282	1.591644		
	6	0.326583	0.272016	0.16300	0.11300	0.11300	0.115534	0.150177	0.307302	1.735519	1.592990		
	7	0.244276	0.208746	0.112560	0.092058	0.114155	0.101218	0.315636	0.314952	1.624089	1.501359		
	8	0.189291	0.165296	0.086464	0.069225	0.099953	0.089723	0.314501	0.305850	1.525668	1.422457		
	9	0.151270	0.134597	0.069824	0.052700	0.088550	0.080276	0.312443	0.303934	1.485010	1.348501		
	10	0.124272	0.112423	0.047918	0.036454	0.079179	0.071363	0.30582	0.301297	1.380556	1.348501		
	11	0.104705	0.096133	0.02892	0.012593	0.071328	0.065625	0.299028	0.280716	1.219206	1.219206		
	12	0.090517	0.074897	0.025707	0.020546	0.064640	0.059806	0.301297	0.294226	1.21652	1.161071		
	13	0.090259	0.084078	0.017831	0.013715	0.058860	0.054714	0.297337	0.294226	1.161071	1.161071		
	14	0.079566	0.074897	0.014424	0.008205	0.053601	0.050208	0.292449	0.294226	1.161071	1.161071		
	15	0.071503	0.066007	0.011444	0.006607	0.038291	0.032804	0.264303	0.264303	1.161071	1.161071		
	16	0.065417	0.052783	0.006220	0.003161	0.049317	0.046175	0.281768	0.281768	1.161071	1.161071		
	17	0.060817	0.058824	0.001920	0.000185	0.045297	0.042524	0.281564	0.281564	1.161071	1.161071		
	18	0.057351	0.055841	0.001634	0.001634	0.043667	0.040634	0.281564	0.281564	1.161071	1.161071		
	19	0.054763	0.052620	0.001725	0.001725	0.041547	0.039147	0.281564	0.281564	1.161071	1.161071		
	20	0.052867	0.050207	0.001725	0.001725	0.040935	0.038200	0.281564	0.281564	1.161071	1.161071		
	21	0.051532	0.050261	0.001366	0.001366	0.032124	0.029034	0.281564	0.281564	1.161071	1.161071		
	22	0.050684	0.050261	0.001366	0.001366	0.029034	0.026902	0.281564	0.281564	1.161071	1.161071		
23	2	4.253712	2.423202	1.335793	0.794692	0.494451	0.323377	0.745637	0.509456	2.427775	2.060704		
	3	1.959040	1.30915	0.73693	0.488055	0.325866	0.261663	0.394172	0.362461	2.287647	1.976643		
	4	1.106080	0.809186	0.45620	0.288697	0.241519	0.192769	0.323560	0.307645	2.117120	1.847013		
	5	0.659679	0.541966	0.302137	0.232633	0.190862	0.158670	0.306394	0.287104	1.958810	1.756552		

Table D.I (continued)

n	x	\tilde{A}	\tilde{A}^0	\tilde{B}	\tilde{B}^0	\tilde{C}	\tilde{C}^0	\tilde{Q}	\tilde{Q}^0	$\tilde{Q} \cdot .99$	$\tilde{Q} \cdot .99$
6	0.476419	0.384356	0.215249	0.170386	0.157047	0.134303	0.307951	0.294922	0.294922	0.919400	1.653264
7	0.342121	0.284731	0.158246	0.128277	0.132854	0.115483	0.307951	0.294746	0.294746	0.975890	1.558907
8	0.256091	0.213536	0.113695	0.097530	0.14671	0.11694	0.302579	0.294574	0.294574	0.973217	1.473217
9	0.198356	0.12477	0.097086	0.074651	0.100492	0.090225	0.301811	0.293905	0.293905	1.195351	1.195351
10	0.159261	0.140465	0.068726	0.057182	0.089113	0.080805	0.300226	0.292315	0.292315	1.374328	1.374328
11	0.129648	0.116933	0.052372	0.043562	0.079766	0.072919	0.297842	0.297842	0.297842	1.259222	1.259222
12	0.108799	0.099546	0.039599	0.032764	0.071940	0.066210	0.294897	0.297393	0.297393	1.199204	1.199204
13	0.C93354	0.086522	0.029457	0.024082	0.065280	0.060421	0.291367	0.284115	0.284115	1.143550	1.143550
14	0.C81768	0.076663	0.021206	0.017023	0.059532	0.055164	0.287400	0.291419	0.291419	1.145620	1.145620
15	0.C72995	0.069146	0.014656	0.011228	0.054507	0.050496	0.293064	0.276155	0.276155	1.091605	1.091605
16	0.066309	0.063383	0.079206	0.066436	0.05065	0.045907	0.278409	0.271963	0.271963	1.041048	0.996794
17	0.061196	0.058962	0.047002	0.027449	0.046093	0.043109	0.273465	0.267265	0.267265	0.921151	0.952910
18	0.C57287	0.055575	0.C01954	0.049984	0.042505	0.047028	0.268240	0.262262	0.262262	0.910758	0.910758
19	0.C543C9	0.052997	-0.002171	-0.003676	0.039225	0.037003	0.262717	0.25626	0.25626	0.94123	0.969839
20	0.052064	0.051059	-0.004782	-0.006016	0.036187	0.034177	0.256844	0.251100	0.251100	0.861942	0.879545
21	0.C50403	0.047639	-0.006961	-0.007973	0.033327	0.031472	0.250507	0.244902	0.244902	0.819945	0.788946
22	0.C49223	0.048650	-0.009176	-0.004594	0.030561	0.028401	0.237646	0.23604	0.23604	0.746396	0.746396
23	0.048467	0.048861	-0.010233	-0.010887	0.027724	0.025751	0.234920	0.227488	0.227488	0.693172	0.693172
24	2	4.371373	2.494265	1.357719	0.809501	0.474687	0.326589	0.765809	0.514916	1.999995	2.348202
3	2.022432	1.355507	0.728596	0.499342	0.326187	0.243934	0.395076	0.143118	0.221695	1.927392	1.927392
4	1.147133	0.839800	0.456955	0.337413	0.241886	0.193028	0.315445	0.298714	0.020220	1.920220	1.920220
5	0.728C75	0.564126	0.311304	0.240534	0.191262	0.152023	0.295559	0.286416	1.715375	1.715375	1.715375
6	0.497C49	0.400946	0.222952	0.177634	0.157473	0.134495	0.291070	0.283528	1.774177	1.616761	1.616761
7	0.357586	0.297424	0.164872	0.134128	0.133303	0.116391	0.290514	0.281373	1.641394	1.526462	1.526462
8	0.267908	0.228382	0.124535	0.107572	0.115140	0.102126	0.296500	0.283174	1.585881	1.444158	1.444158
9	0.207516	0.180572	0.095292	0.079364	0.100981	0.090680	0.290014	0.282503	1.477700	1.369317	1.369317
10	0.165394	0.146489	0.073418	0.061477	0.089622	0.081283	0.288817	0.291452	1.396447	1.300999	1.300999
11	0.135205	0.121632	0.056639	0.047494	0.080296	0.073421	0.286914	0.279696	0.279696	1.313280	1.238352
12	0.113101	0.103174	0.043575	0.036389	0.072492	0.066735	0.284405	0.277159	0.277159	1.190677	1.190677
13	0.C96642	0.C89271	0.033054	0.027439	0.065855	0.060972	0.281377	0.274551	0.274551	1.127088	1.127088
14	0.C84221	0.078681	0.024623	0.020162	0.060132	0.055943	0.277921	0.271332	0.271332	1.130171	1.130171
15	0.C74752	0.070546	0.017745	0.01136	0.055137	0.051507	0.274107	0.267763	0.267763	1.030447	1.030447
16	0.067480	0.064261	0.012081	0.009152	0.050726	0.047553	0.26990	0.263896	0.263896	1.029765	1.046347
17	0.061866	0.059390	0.007382	0.004990	0.046793	0.043996	0.256005	0.259731	0.259731	0.984142	0.984142
18	0.057525	0.055611	0.003460	0.001497	0.043249	0.040764	0.260971	0.255311	0.255311	0.940998	0.940998
19	0.054171	0.052687	0.000171	-0.00146	0.040024	0.037800	0.256089	0.250621	0.250621	0.865894	0.865894
20	0.051591	0.050441	-0.002595	-0.003930	0.037059	0.035051	0.250940	0.245632	0.245632	0.859677	0.859677
21	0.045628	0.046719	-0.004923	-0.006077	0.034297	0.032466	0.245470	0.240275	0.240275	0.820690	0.791207
22	0.048164	0.047479	-0.006880	-0.007732	0.031682	0.029187	0.239572	0.234409	0.234409	0.791900	0.751742
23	0.C47114	0.046596	-0.004513	-0.009264	0.029142	0.027526	0.233006	0.227683	0.227683	0.742112	0.714303
24	0.046435	0.046083	-0.008833	-0.009845	-0.010445	0.026524	0.024705	0.225070	0.216199	0.216199	0.666459
25	2	4.485528	2.563561	1.378732	0.823689	0.494901	0.329783	0.786085	0.521362	2.274010	1.942874
3	2.C85306	1.399146	0.742872	0.510152	0.326481	0.244185	0.395186	0.339676	2.159445	1.872879	1.872879

Table D.I (continued)

x	\tilde{A}	\tilde{A}^0	\tilde{B}	\tilde{B}^0	\tilde{C}	\tilde{C}^0	\tilde{Q}	\tilde{Q}^0	$\tilde{Q} \cdot 90$	$\tilde{Q} \cdot 99$	$\tilde{Q} \cdot 999$
4	1.187380	0.969873	0.467613	0.346170	0.242223	0.193319	0.309531	0.299854	2.079130	1.775911	
5	0.756029	0.585987	0.320084	0.248003	0.191628	0.159346	0.285451	0.274745	1.856284	1.676272	
6	0.517448	0.417488	0.230330	0.194000	0.157663	0.135035	0.280236	0.273088	1.738946	1.582048	
7	0.372954	0.310074	0.171257	0.139731	0.13712	0.116763	0.279313	0.272489	1.676878	1.495380	
8	0.279733	0.238258	0.130130	0.107755	0.115569	0.102527	0.279318	0.272456	1.528084	1.416337	
9	0.216735	0.189350	0.100282	0.083881	0.101427	0.091095	0.279032	0.272141	1.446440	1.346306	
10	0.172636	0.152637	0.077918	0.065585	0.090085	0.081718	0.278152	0.271298	1.362091	1.275495	
11	0.14C907	0.126486	0.067732	0.051266	0.080777	0.073875	0.276632	0.269864	1.291497	1.141118	
12	0.117577	0.106481	0.047255	0.039867	0.072991	0.067211	0.274533	0.267915	1.227409	1.162461	
13	0.100124	0.092218	0.036509	0.030662	0.066374	0.061469	0.271038	0.265506	1.158805	1.110893	
14	0.C866887	0.780913	0.027821	0.021441	0.060673	0.056454	0.269927	0.262703	1.11846	1.062962	
15	0.C76734	0.672174	0.020717	0.016914	0.055701	0.052053	0.265571	0.259563	1.064835	1.017889	
16	0.C68889	0.65378	0.016852	0.011770	0.051317	0.048128	0.261921	0.256132	1.019160	0.975543	
17	0.062786	0.60066	0.009971	0.007443	0.047413	0.044603	0.259117	0.252441	0.974379	0.935645	
18	0.058023	0.555904	0.005883	0.003799	0.043905	0.041410	0.253985	0.248512	0.932981	0.897240	
19	0.C54300	0.52645	0.002441	0.000715	0.040722	0.038491	0.249538	0.244350	0.893581	0.860586	
20	0.051397	0.50101	-0.000668	-0.001901	0.037808	0.035799	0.244966	0.239946	0.855761	0.825136	
21	0.049145	0.48130	-0.002932	-0.004124	0.035113	0.033288	0.240157	0.235270	0.819158	0.790583	
22	0.047417	0.46624	-0.005020	-0.006013	0.032989	0.030917	0.235046	0.230256	0.793231	0.750195	
23	0.046117	0.45502	-0.006756	-0.007612	0.030189	0.028634	0.229541	0.224769	0.747395	0.721472	
24	0.045179	0.44708	-0.006269	-0.008954	0.027847	0.026357	0.223413	0.219483	0.710527	0.684817	
25	0.044554	0.44243	-0.009486	-0.010037	0.025624	0.023740	0.215997	0.209638	0.669832	0.638952	

**Table D.III - Factors for Calculating Cramér-Rao Efficiencies of BLU Estimates of a Scale Parameter
and $100(1-R)$ Percent Points of the Extreme-Value Distribution, $R = e^{-1}$, .90, .99,
When $\frac{n-r}{n}$ of the Size n Ordered Sample is Censored From Above, $2 \leq n \leq 25$, $2 \leq r \leq n$**

n	r	A	A^0	B	B^0	C	C^0	$Q_{.90}$	Q^0	$Q_{.99}$	Q^0	$Q_{.99}$
2	2	0.659547	0.554332	0.064322	-0.128511	0.711857	0.3033764	3.975007	2.677764	15.131652	8.168960	
3	2	0.516039	0.514796	0.469246	0.076874	0.818365	0.399419	2.352912	2.191574	13.975769	8.269781	
3	3	0.402664	0.369555	-0.026772	-0.085674	0.344712	0.202642	2.200028	1.781363	7.925148	5.415973	
4	2	1.334C19	0.627559	0.772030	0.233942	0.847022	0.429045	2.250049	1.747402	12.579493	7.514420	
4	3	0.433157	0.333677	0.118027	0.009162	0.392233	0.254987	1.888275	1.582802	7.647457	5.613279	
4	4	0.291459	0.277166	-0.034670	-0.064256	0.225283	0.151982	1.590458	1.36022	5.379916	4.0114481	
5	2	1.789172	0.786604	1.011559	0.357105	0.895046	0.444948	1.769062	1.432654	11.422914	6.516842	
5	3	0.529395	0.362392	0.235374	0.089321	0.416816	0.274556	1.580857	1.350778	7.144279	5.310606	
5	4	0.291814	0.250523	0.031571	-0.09858	0.253791	0.185638	1.403454	1.234970	5.397521	4.269577	
5	5	0.231395	0.221733	-0.031991	-0.051404	0.166647	0.121585	1.229305	1.06818	4.070604	3.267586	
6	2	2.244005	0.960564	1.208225	C.457758	0.913293	0.454968	1.431167	1.204346	10.454506	6.376805	
6	3	0.652941	0.418373	0.331249	C.155951	0.632116	0.285030	1.341378	1.164235	6.711123	5.016280	
6	4	0.323719	C.257198	0.102022	0.038437	0.269716	0.199709	1.230427	1.095762	5.092651	4.129891	
6	5	0.223607	0.201827	0.010533	-C.016232	0.186107	0.145295	1.118673	1.010952	4.064971	3.476370	
6	6	0.191174	0.184777	-C.031373	-0.042937	0.131960	0.101321	1.007642	0.890681	3.272775	2.722987	
7	2	2.685691	1.137462	1.374610	C.542615	0.926126	0.461881	1.18981	1.034311	9.636969	5.919293	
7	3	0.787954	0.487326	0.416705	C.212661	0.442612	0.293479	1.153933	1.017435	6.320432	4.745446	
7	4	0.372647	0.280941	0.156958	C.080311	0.280158	0.208454	1.044985	0.975126	4.857122	3.915322	
7	5	0.235293	0.201634	0.050448	0.015963	0.197566	0.155984	1.00744	0.919716	3.951929	3.315607	
7	6	0.187701	0.169495	-0.001471	-0.018348	0.146271	0.119066	0.930151	0.854945	3.221719	2.917493	
7	7	0.162978	0.158381	-0.028603	-0.036717	0.109096	0.086847	0.844142	0.763441	2.734710	2.313989	
8	2	3.1C9991	1.312232	1.518578	0.615948	0.735646	0.4666946	1.013527	0.905150	8.938174	5.527468	
8	3	0.927027	0.562496	0.489217	C.261937	0.450277	0.293170	1.005371	0.997081	5.954377	4.496169	
8	4	0.430722	0.313780	0.205090	C.116971	0.287595	0.214523	0.964092	0.873701	4.629738	3.777210	
8	5	0.256047	0.212271	0.045913	0.044711	0.205169	0.1622912	0.911306	0.836048	3.91329	3.248352	
8	6	0.186582	0.166839	0.029555	0.004421	0.155033	0.127490	0.354874	0.791401	3.228495	2.871647	
8	7	0.155C9A	0.146327	-0.007184	-0.018688	0.120152	0.107665	C.795897	0.740220	2.763772	2.469674	
8	8	0.141983	0.138583	-0.026083	-0.032128	0.092916	0.075991	0.729914	0.668011	2.349191	2.042724	
9	2	3.515995	1.482672	1.645332	0.680191	0.942981	0.477518	0.986242	0.805688	9.333413	5.137875	

Table D.II (continued)

n	r	A	A^0	B	B^0	C	C^0	Q^0	Q^0	Q^0	Q^0
3	1	0.066436	0.640376	0.553268	0.305172	0.456126	0.303317	0.396716	0.802998	5.678459	4.251204
4	1	0.493734	0.351987	0.247785	0.149453	0.293180	0.219710	0.863227	0.788441	4.419130	3.611526
5	0	0.287481	0.229540	0.117661	0.070418	0.211085	0.167868	0.826837	0.762713	3.671914	3.133791
6	0	0.158C22	0.171599	0.050839	0.025625	0.161172	0.131140	0.785409	0.730578	3.140912	2.753261
7	0	0.155618	0.142877	0.012844	-0.01443	0.127127	0.107533	0.741601	0.693917	2.727624	2.431702
8	0	0.135059	0.128850	-0.003992	-0.019312	0.101763	0.097105	0.695372	0.652181	2.380427	2.140585
9	0	0.125823	0.123185	-0.021881	-0.028558	0.080876	0.067547	0.642873	0.593788	2.056979	1.815174
10	2	3.504149	1.647977	1.759472	0.737731	0.948830	0.477976	0.794751	0.729229	7.804222	4.820260
11	3	1.204241	0.719043	0.610517	0.343860	0.460738	0.305552	0.789717	0.723943	5.317162	4.624779
12	4	0.559271	0.393302	0.286C78	C.178553	0.297537	0.227474	0.778479	0.716327	4.223549	3.45H421
13	5	0.321045	C.251024	0.1462759	0.093577	0.215474	0.171618	0.753965	0.699961	3.535141	3.021768
14	6	0.214365	C.181196	0.073442	0.046640	0.165771	0.137278	0.723311	0.675399	3.046613	2.675302
15	7	0.161525	0.144726	0.031277	0.014493	0.132126	0.11245	0.689857	0.647968	2.669720	2.394734
16	8	0.134061	0.125262	0.005260	-0.004929	0.107479	0.092819	0.654667	0.617695	2.350763	2.134789
17	9	0.119776	0.115168	-0.011359	-C.017641	0.088144	0.076774	0.617274	0.583010	2.089530	1.900645
18	10	0.112573	0.110866	-0.021976	-0.025702	0.060793	0.057153	0.574340	0.534409	1.829746	1.631792
19	11	2	4.275424	1.907564	1.860590	0.789216	0.953583	0.476353	0.730491	0.667836	7.336566
20	12	2	4.630570	1.761762	1.953610	0.836245	0.957528	0.478470	0.687758	0.620733	4.624926
21	13	3	1.339428	0.797401	0.662244	0.378774	0.466470	0.309156	0.709911	0.654256	5.075415
22	14	4	0.625897	0.436355	0.320751	0.204873	0.301033	0.225233	0.706758	0.654886	4.045166
23	15	5	0.357166	0.275232	0.177238	0.114600	0.218957	0.174566	0.49C873	0.443381	3.405968
24	16	6	0.233577	0.194064	0.094075	0.062036	0.169364	0.140469	0.668254	0.526211	2.952429
25	17	7	0.171105	C.157195	0.049232	0.229145	0.135937	0.115763	0.642743	0.605264	2.603978
26	8	0.137035	0.125594	0.019467	0.007531	0.111652	0.096820	0.614837	0.581781	2.320632	2.046A5
27	9	9	0.118C95	0.111705	0.006638	-0.006940	0.292934	0.081546	0.585594	0.555594	2.078A23
28	10	10	0.1C7697	0.104152	-0.011959	-0.016853	0.077670	0.059484	0.554854	0.526962	1.861324
29	11	11	0.1C25C9	0.107788	-0.020327	-C.023366	0.0664174	0.055266	0.518982	0.485826	1.709516
30	12	12	4.630570	1.761762	1.953610	0.836245	0.957528	0.478470	0.687758	0.620733	4.645265
31	13	13	1.471483	0.874822	0.7C9395	0.410565	0.467553	0.111297	0.646442	0.603434	4.818895
32	14	14	0.692724	0.480282	0.352403	0.228879	0.303903	0.227484	0.645664	0.602171	3.891525
33	15	15	0.394671	0.101204	0.196C08	0.133H21	0.221794	0.176050	0.635655	0.595013	3.294974
34	16	16	0.255797	0.29186	0.113218	0.077981	0.172258	0.141015	0.619475	0.582467	2.951218
35	17	17	0.183261	0.156271	0.063872	0.042672	0.138960	0.119517	0.599505	0.566357	2.536204
36	18	18	0.142823	0.126699	0.032668	0.019218	0.114881	0.09955	0.577570	0.547891	2.277312
37	19	19	0.119429	0.111224	0.011922	0.03121	0.096486	0.084993	0.554380	0.527601	2.051474
38	20	20	0.105737	0.100913	-0.002280	-0.008146	0.072648	0.037011	0.505476	0.485673	1.713195
39	21	21	0.097890	0.095083	-0.012136	-0.016065	0.069373	0.061829	0.490501	0.477577	1.551276
40	22	22	0.093862	0.092399	-0.016894	-0.021419	0.058150	0.050661	0.471337	0.445341	1.498182
41	23	23	4.571948	2.110639	2.038996	0.879375	0.960854	0.480120	0.660883	0.584208	6.545579
42	24	24	1.600C181	0.95C942	0.752696	0.439734	0.470142	0.317089	0.593368	0.557343	4.624098
43	25	25	0.759199	0.524529	0.381500	0.250929	0.306303	0.229357	0.593330	0.553665	3.731066

Table D.II (continued)

n	r	A	A^0	B	B^0	C	C^0	Q^0	Q^0	Q^0	Q^0	Q^0	
5	0.433161	C.32A297	0.217895	0.151579	0.224151	0.178919	0.587874	0.552472	3.172015	2.720550	3.06616	3.06616	
6	0.279108	0.225878	0.132502	0.092691	0.174643	0.145099	0.576174	0.543508	2.774142	2.443400	3.186621	3.186621	
7	0.197252	0.164090	0.078356	0.056197	0.141424	0.120743	0.560786	0.531125	2.469782	2.215152	2.632743	2.632743	
8	0.150658	0.113830	0.044950	0.030050	0.117473	0.102261	0.543253	0.516449	2.223001	2.071449	2.696714	2.696714	
9	0.122664	0.112916	0.022495	0.012578	0.099266	0.087643	0.524419	0.501644	2.016611	1.851144	2.696708	2.696708	
10	0.106122	0.100000	0.006897	0.000146	0.084820	0.075554	0.504625	0.492468	1.037555	1.037555	1.676950	1.676950	
11	0.C95852	0.092093	-0.004165	-0.004165	0.072905	0.065454	0.453802	0.463261	1.676497	1.598335	1.420261	1.420261	
12	0.C85757	0.087481	-0.012073	-0.011929	0.062645	0.056334	0.461341	0.441692	1.526497	1.526497	1.373560	1.373560	
13	0.086493	0.085282	-0.017639	-0.019771	0.053152	0.046766	0.435055	0.411064	1.256763	1.256763			
14	2	5.259468	2.254447	2.117889	0.919194	0.963698	0.491586	0.644772	0.552225	6.207424	3.06616	3.06616	
	3	1.725456	1.025563	0.792714	0.466672	0.472348	0.314610	0.549704	0.519430	4.427745	3.186621	3.186621	
	4	0.824573	0.569731	0.408412	0.271304	0.308338	0.230941	0.548291	0.517165	3.792325	2.95642	2.95642	
	5	0.472356	0.356073	0.239164	0.167878	0.226141	0.185275	0.545653	0.514950	3.066621	2.632743	2.632743	
	6	0.303415	0.243663	0.146721	0.106330	0.176645	0.146840	0.537619	0.505717	2.691585	2.172723	2.172723	
	7	0.212558	C.179303	0.091624	0.066840	0.143475	0.122584	0.525964	0.499258	2.403887	2.159406	2.159406	
	8	0.16007	0.140471	0.056409	0.040155	0.119608	0.104227	0.511184	0.487561	2.172107	1.976614	1.976614	
	9	0.128145	0.116235	0.032403	0.021466	0.101522	0.097677	0.496441	0.474306	1.574376	1.614525	1.614525	
	10	0.108258	0.100817	0.015556	0.007981	0.087249	0.077992	0.48089	0.459858	1.611454	1.677814	1.677814	
	11	0.095676	0.090961	0.003442	-0.001882	0.075597	0.069104	0.462969	0.444318	1.661538	1.549463	1.549463	
	12	0.087744	0.084747	-0.005397	-0.009174	0.065737	0.059523	0.444936	0.427473	1.526480	1.428746	1.428746	
	13	0.C82495	0.CA1014	-0.011974	-0.014554	0.057084	0.051723	0.425420	0.408454	1.420118	1.399469	1.399469	
	14	0.C80228	0.079190	-0.015355	-0.015355	0.048941	0.043421	0.42490	0.381721	1.260706	1.165974	1.165974	
	15	2	5.614554	2.343457	2.191194	0.956168	0.966156	0.482851	0.645331	0.532229	5.900794	3.06616	3.06616
	3	1.847337	1.095885	0.829902	0.491687	0.474250	0.315918	0.513862	0.485496	4.247768	3.260166	3.260166	
	4	0.886928	0.612647	0.433635	0.290245	0.310088	0.232297	0.509387	0.482723	3.453989	2.858014	2.858014	
	5	0.511450	0.384226	0.257028	0.183103	0.227844	0.181987	0.504672	0.481739	2.969709	2.550722	2.550722	
	6	0.328367	C.2622C1	0.161836	0.119035	0.178350	0.149314	0.503174	0.477551	2.613557	2.305614	2.305614	
	7	0.228809	0.191501	0.104198	0.077707	0.145212	0.124136	0.494316	0.470404	2.341208	2.103465	2.103465	
	8	0.170484	0.148248	0.067132	0.049611	0.121402	0.105868	0.483137	0.461094	2.121875	1.932153	1.932153	
	9	0.134577	0.120797	0.041706	0.029774	0.103398	0.091519	0.470490	0.457259	1.939902	1.782535	1.782535	
	10	0.111735	0.102959	0.023721	0.015375	0.089237	0.07984	0.456882	0.438155	1.781870	1.651956	1.651956	
	11	0.056917	0.091226	0.016064	0.004713	0.077731	0.070184	0.442565	0.425435	1.643707	1.533052	1.533052	
	12	0.C83506	0.001011	-0.003286	-0.0068107	0.061879	0.042759	0.416663	0.411663	1.519172	1.423192	1.423192	
	13	0.08C958	C.078517	-0.006202	-0.009325	0.059817	0.054554	0.411794	0.396755	1.403830	1.318746	1.318746	
	14	0.C77025	0.075450	-0.013865	0.052413	0.047800	0.0394655	0.379918	0.29865	1.29865	1.214524	1.214524	
	15	0.074809	0.073911	-0.015557	-0.017135	0.045343	0.040528	0.374452	0.356273	1.177461	1.09195	1.09195	
	16	2	5.910144	2.527944	2.259641	0.990671	0.966302	0.481953	0.52007	5.619375	3.654580	3.654580	
	3	1.665907	1.169967	0.864627	0.515032	0.475906	0.317054	0.455154	0.455154	3.140421	3.140421	3.140421	
	4	0.953632	0.656116	0.456809	0.307924	0.311608	0.213473	0.475685	0.452575	3.344904	2.761774	2.761774	
	5	0.550447	0.412539	0.274662	0.197328	0.183206	0.183206	0.475573	0.452202	2.876183	2.473959	2.473959	
	6	0.352111	0.281248	0.175980	0.130916	0.179820	0.149585	0.472311	0.449540	2.539892	2.242184	2.242184	

Table D.II (continued)

n	r	A	A ⁰	B	B ⁰	C	C ⁰	Q	Q ⁰	Q ^{0.99}	Q ^{0.90}	Q ^{0.90}	Q ^{0.99}	Q ^{0.99}	
7	0.245731	0.204422	0.116181	0.087886	0.146703	0.125467	0.4655762	0.444227	2.291275	2.050797	1.988605	1.988605	1.988605	1.988605	
8	0.181809	0.156897	0.077199	0.058485	0.122932	0.167261	0.4556901	0.435951	2.072956	2.072956	1.78154	1.78154	1.78154	1.78154	
9	0.141972	0.125321	0.050460	0.037609	0.104985	0.092992	0.44522	0.427941	1.890343	1.890343	1.62476	1.62476	1.62476	1.62476	
10	0.116255	0.106135	0.031430	0.022355	0.090902	0.081456	0.43169	0.418024	1.757700	1.757700	1.512745	1.512745	1.512745	1.512745	
11	0.099263	0.092583	0.010970	0.079500	0.071981	0.07228	0.43052	0.420487	1.620487	1.620487	1.410820	1.410820	1.410820	1.410820	
12	0.087888	0.08149	0.007124	0.062340	0.070017	0.061755	0.410399	0.395700	1.501992	1.501992	1.3509	1.3509	1.3509	1.3509	
13	0.080254	0.077244	-0.000733	-0.004266	0.061930	0.056655	0.376174	0.363477	1.397514	1.397514	1.224237	1.224237	1.224237	1.224237	
14	0.075187	0.073163	-0.006722	-0.009344	0.054849	0.050331	0.383207	0.370110	1.297718	1.297718	1.207720	1.207720	1.207720	1.207720	
15	0.071943	0.070603	-0.011284	-0.013224	0.048425	0.044423	0.368014	0.355085	1.200720	1.200720	1.132114	1.132114	1.132114	1.132114	
16	0.070277	0.069292	-0.014635	-0.016064	0.042235	0.037995	0.350057	0.334006	1.098947	1.098947	1.021120	1.021120	1.021120	1.021120	
17	2	6.211586	2.658180	2.323825	1.023009	0.970192	0.484922	0.65367	0.509604	5.361800	5.361800	3.507796	3.507796	3.507796	3.507796
3	2.081279	1.239711	0.897189	0.536912	0.477363	0.318051	0.460707	0.438673	3.928523	3.928523	3.030365	3.030365	3.030365	3.030365	
4	1.016308	0.699035	0.474777	0.324499	0.312941	0.234502	0.446433	0.426104	3.214064	3.214064	2.675926	2.675926	2.675926	2.675926	
5	0.589197	0.440859	0.291211	0.210673	0.203609	0.184270	0.446371	0.425648	2.799969	2.799969	2.402014	2.402014	2.402014	2.402014	
6	0.372664	0.306621	0.189265	0.142075	0.161102	0.150685	0.444563	0.424286	2.470145	2.470145	2.182253	2.182253	2.182253	2.182253	
7	0.263129	0.217870	0.127260	0.097454	0.147997	0.125610	0.439848	0.420425	2.224130	2.224130	2.000500	2.000500	2.000500	2.000500	
8	0.193770	0.166190	0.086678	0.066840	0.124253	0.108461	0.412893	0.414625	2.025680	2.025680	1.846427	1.846427	1.846427	1.846427	
9	0.150110	0.132595	0.059718	0.044999	0.106348	0.09252	0.424196	0.417373	1.860151	1.860151	1.713096	1.713096	1.713096	1.713096	
10	0.121594	0.110128	0.048718	0.028956	0.092320	0.082788	0.414359	0.399054	1.719002	1.719002	1.595629	1.595629	1.595629	1.595629	
11	0.102484	0.094088	0.024004	0.016906	0.080991	0.073302	0.404599	0.389931	1.595420	1.595420	1.490440	1.490440	1.490440	1.490440	
12	0.089462	0.084242	0.012947	0.007703	0.071603	0.065278	0.393798	0.381043	1.495515	1.495515	1.394752	1.394752	1.394752	1.394752	
13	0.080515	0.076929	0.005459	0.005059	0.063644	0.058349	0.369277	0.369771	1.395935	1.395935	1.306269	1.306269	1.306269	1.306269	
14	0.074272	0.071898	-0.002000	-0.004951	0.056747	0.052237	0.370750	0.358725	1.291618	1.291618	1.222869	1.222869	1.222869	1.222869	
15	0.070212	0.066510	-0.007047	-0.009278	0.050624	0.046704	0.358296	0.346781	1.206116	1.206116	1.142163	1.142163	1.142163	1.142163	
16	0.067478	0.066346	-0.012611	-0.012610	0.045010	0.041485	0.344720	0.332280	1.120714	1.120714	1.060437	1.060437	1.060437	1.060437	
17	0.065908	0.065216	-0.013904	-0.015119	0.039524	0.035760	0.328641	0.314358	1.030207	1.030207	0.961054	0.961054	0.961054	0.961054	
18	2	6.494167	2.7864419	1.053435	0.971669	0.4855780	0.565076	0.4855780	0.4855780	0.4855780	3.124511	3.124511	3.124511	3.124511	
3	2.193580	0.927837	0.557497	0.478653	0.318933	0.416177	0.413822	0.413822	3.786148	3.786148	2.593947	2.593947	2.593947	2.593947	
4	1.017617	0.741336	0.499374	0.340195	0.314119	0.315409	0.412012	0.402404	3.036015	3.036015	2.364659	2.364659	2.364659	2.364659	
5	0.627596	0.469074	0.306798	0.223236	0.211747	0.185206	0.420381	0.402262	2.709063	2.709063	2.125602	2.125602	2.125602	2.125602	
6	0.404489	0.320188	0.201785	0.152586	0.182230	0.151656	0.419549	0.401469	2.046643	2.046643	1.697399	1.697399	1.697399	1.697399	
7	0.260845	0.231659	0.137710	0.106476	0.149132	0.127614	0.416277	0.398730	2.169714	2.169714	1.952562	1.952562	1.952562	1.952562	
8	0.206205	0.175993	0.095629	0.074726	0.125408	0.109505	0.410688	0.394220	1.980191	1.980191	1.805766	1.805766	1.805766	1.805766	
9	0.156626	0.139458	0.066527	0.051997	0.107533	0.095343	0.403965	0.384220	1.678760	1.678760	1.622290	1.622290	1.622290	1.622290	
10	0.127581	0.114770	0.045623	0.035209	0.093545	0.083934	0.395976	0.361356	1.697399	1.697399	1.566990	1.566990	1.566990	1.566990	
11	0.106605	0.097730	0.031070	0.022544	0.082269	0.074513	0.387243	0.373614	1.569762	1.569762	1.467178	1.467178	1.467178	1.467178	
12	0.091777	0.085799	0.018493	0.012812	0.072949	0.065570	0.377967	0.355254	1.465329	1.465329	1.376630	1.376630	1.376630	1.376630	
13	0.081352	0.077382	0.009522	0.005235	0.065077	0.059743	0.356157	0.346259	1.371077	1.371077	1.293457	1.293457	1.293457	1.293457	
14	0.074369	0.071438	0.002543	0.001722	0.058297	0.053766	0.358148	0.346668	1.284616	1.284616	1.215951	1.215951	1.215951	1.215951	
15	0.069361	0.061727	-0.002930	-0.005431	0.052340	0.048432	0.347584	0.336984	1.203676	1.203676	1.162123	1.162123	1.162123	1.162123	
16	0.065875	0.064425	-0.007237	-0.009156	0.046988	0.043552	0.336398	0.326190	1.126779	1.126779	1.070292	1.070292	1.070292	1.070292	
17	0.0633577	0.062575	-0.010613	-0.012081	0.042029	0.038908	0.324113	0.313684	1.050676	1.050676	0.997063	0.997063	0.997063	0.997063	

Table D.II (continued)

n	r	A	A^0	B	B^0	C	C^0	θ_{eff}	q^0	q^0	q^0	q^0	q^0
18	0	0.62208	0.061592	-0.013200	-0.014279	0.037136	0.033774	0.303689	0.296894	0.969538	0.907662		
19	2	6.768016	2.906904	2.441302	1.082159	0.973368	0.485546	0.709650	0.500314	4.975119	3.246692		
	3	2.302943	1.374393	0.956781	0.576928	0.479803	0.319719	0.426525	0.396896	3.653575	2.832170		
	4	1.138147	C.782978	0.518870	C.154821	0.315168	0.236216	0.399914	0.382257	3.013789	2.917176		
	5	0.665572	0.497104	0.321524	C.235101	0.232758	0.185037	0.397194	0.381097	2.612929	2.270501		
	6	0.430438	0.339847	0.213620	0.162518	0.183230	0.152512	0.396943	0.380742	2.342509	2.072005		
	7	0.258765	0.245791	0.147536	0.115008	0.150136	0.123499	0.394796	0.378208	2.117916	1.906897		
	8	0.218990	0.186178	0.104105	0.1282192	0.126425	0.110423	0.397681	0.375454	1.936533	1.766695		
	9	0.167589	0.146789	0.071930	0.058609	0.108573	0.096299	0.385079	0.370668	1.765360	1.645169		
	10	0.134084	0.119932	0.052177	0.041144	0.094617	0.084932	0.378402	0.364859	1.656258	1.538662		
	11	0.110891	C.101214	0.036033	C.027904	0.083379	0.075561	0.370961	0.359276	1.541796	1.443461		
	12	0.054694	0.087954	0.023779	0.017693	0.074108	0.067677	0.362967	0.351094	1.446155	1.377403		
	13	0.083220	0.078461	0.014314	0.009578	0.066300	0.060923	0.354550	0.343423	1.454523	1.278223		
	14	0.075025	0.071432	0.006904	C.003342	0.059600	0.055739	0.345775	0.335316	1.27719	1.205585		
	15	0.069159	0.066725	0.001045	-0.011711	0.053749	0.049828	0.336648	0.326766	1.196494	1.136905		
	16	0.064582	C.063235	-0.001615	-0.005759	0.048548	0.051229	0.327120	0.317693	1.125594	1.071204		
	17	0.062058	0.059212	-0.007331	-0.008999	0.043827	0.0469791	0.317000	0.307884	1.056949	1.006799		
	18	0.060090	0.059218	-0.010278	-0.011572	0.039413	0.036628	0.315942	0.296787	0.989678	0.940789		
	19	0.058901	0.058351	-0.012563	-0.013527	0.035022	0.031996	0.292800	0.281268	0.915596	0.859891		
20	2	7.033320	3.025855	2.495356	1.109360	0.974715	0.487233	0.738449	0.503442	4.701608	3.129932		
	3	2.405504	1.439417	0.984196	0.595327	0.480836	0.320423	0.414764	0.346778	3.529763	2.428118		
	4	1.197301	0.821338	0.537337	0.368765	0.316109	0.236938	0.379713	0.364114	2.942937	2.445125		
	5	0.703077	0.524993	0.3355478	0.246339	0.231662	0.186778	0.376481	0.362660	2.561194	2.211987		
	6	0.455986	0.355521	0.224839	0.171930	0.184127	0.153276	0.376466	0.361922	2.283674	2.021240		
	7	0.216802	0.260641	0.156972	C.123099	0.151049	0.129286	0.375148	0.350756	2.058661	1.863398		
	8	0.212030	0.196651	0.112149	0.09276	0.127329	0.111237	0.372092	0.358143	1.894488	1.722920		
	9	0.177498	0.154469	0.08999	0.064999	0.109494	0.071142	0.347601	0.354317	1.749654	1.613039		
	10	0.149917	0.125512	0.053411	0.046788	0.095561	0.095809	0.362040	0.349480	1.625802	1.510884		
	11	0.115834	0.105157	0.041618	0.033010	0.084354	0.076478	0.353703	0.343892	1.517901	1.419825		
	12	0.098103	0.090598	0.028423	0.022330	0.075121	0.068339	0.344801	0.327694	1.427574	1.327651		
	13	0.085409	0.080555	0.018896	0.013928	0.067353	0.061019	0.341471	0.321038	1.364747	1.262633		
	14	0.076224	0.072363	0.011086	0.007241	0.060716	0.050124	0.311605	0.323984	1.259068	1.193367		
	15	0.063542	0.066735	0.004833	0.001872	0.054940	0.050996	0.325834	0.316560	1.197312	1.126556		
	16	0.064679	0.062431	-0.000108	-0.002464	0.049837	0.046410	0.317549	0.308748	1.170296	1.067394		
	17	0.061165	0.059670	-0.004122	-0.005978	0.045254	0.047236	0.308488	0.300462	1.056722	1.008435		
	18	0.058671	0.057584	-0.007357	-0.008821	0.041056	0.038352	0.299698	0.291505	0.995162	0.950323		
	19	0.056570	0.056193	-0.009957	-0.011101	0.037098	0.034598	0.289432	0.281367	0.933587	0.890475		
	20	0.055929	0.055433	-0.011984	-0.012851	0.033133	0.030396	0.277655	0.267204	0.867323	0.816896		
21	2	7.290623	3.141483	2.546703	1.135190	0.975932	0.487854	0.770861	0.502858	4.517269	3.021049		
	3	2.513392	1.502965	1.010235	0.612796	0.481769	0.321058	0.405344	0.370817	3.413220	2.65991		
	4	1.255295	0.864207	0.554878	0.382006	0.316957	0.237588	0.363052	0.348084	2.857488	2.377335		

Table D.II (continued)

Table D.III (continued)

n	r	A	A ⁰	B	B ⁰	C	C ⁰	2.90	2.90	2.99	2.99	3.0	3.0	
6	0	0.531383	0.418128	0.255351	0.197513	0.186306	0.155139	0.375597	0.114820	2.124510	1.893893	1.744687	1.914110	
7	0	0.371001	0.303345	0.182493	0.145107	0.153208	0.131200	0.325518	0.314674	1.914674	1.779425	1.625843	1.779425	
8	0	0.271994	0.229125	0.134069	0.108570	0.129574	0.113206	0.324514	0.313771	1.779425	1.650964	1.522713	1.650964	
9	0	0.207380	0.179003	0.102151	0.082055	0.111719	0.099173	0.122391	0.311923	0.311923	1.539526	1.631959	1.539526	
10	0	0.163446	0.140222	0.075449	0.062209	0.097831	0.087909	0.319299	0.309221	1.539526	1.443295	1.351116	1.443295	
11	0	0.132629	0.118380	0.056912	0.046989	0.086680	0.078455	0.315445	0.305817	1.443295	1.358792	1.278325	1.358792	
12	0	0.110488	0.100696	0.047668	0.035087	0.075117	0.070905	0.311007	0.301851	1.278325	1.292246	1.212161	1.292246	
13	0	0.094282	0.071339	0.031514	0.025631	0.069840	0.054307	0.306124	0.297439	1.212161	1.213444	1.151470	1.213444	
14	0	0.082250	0.076969	0.022644	0.018021	0.063300	0.058609	0.300899	0.292668	1.213444	1.205055	1.095277	1.205055	
15	0	0.073222	0.069277	0.015501	0.011831	0.057650	0.051626	0.295402	0.287599	1.095277	1.095277	1.042777	1.042777	
16	0	0.066398	0.063427	0.009691	0.006753	0.052703	0.049216	0.286977	0.282277	1.042777	1.042777	0.92509	0.92509	
17	0	0.061219	0.058968	0.0058968	0.004927	0.002559	0.048321	0.283745	0.276771	0.92509	0.916	0.993385	0.993385	
18	0	0.057287	0.055576	0.0055976	0.004927	0.004921	0.044391	0.27745	0.270841	0.987499	0.987499	0.946416	0.946416	
19	0	0.054314	0.052011	0.0051917	0.004927	0.004826	0.033424	0.271230	0.2664776	0.939031	0.939031	0.901240	0.901240	
20	0	0.052088	0.051097	0.004961	0.003229	0.037546	0.035342	0.264557	0.259309	0.892260	0.892260	0.857127	0.857127	
21	0	0.050454	0.049704	0.0049704	0.007261	0.006232	0.034476	0.032495	0.251212	0.946267	0.946267	0.813076	0.813076	
22	0	0.049302	0.049145	0.0049045	0.009879	0.031524	0.029656	0.249454	0.243380	0.799614	0.799614	0.767183	0.767183	
23	0	0.048575	0.048203	0.010525	0.011175	0.028514	0.026432	0.240364	0.232352	0.748807	0.748807	0.710344	0.710344	
24	2	0.019406	3.47C256	2.688884	1.205671	0.978970	0.499399	0.322635	0.395127	0.522246	2.734091	2.015612	2.463387	
25	3	2.010263	1.685296	1.081302	0.660447	0.484091	0.322635	0.322635	0.346672	3.105981	3.105981	2.463387	2.463387	
26	4	1.422564	C.980880	0.602753	0.418122	0.319163	0.239200	0.325516	0.310367	2.628856	2.195920	2.463387	2.463387	
27	5	0.47903	0.3842980	0.384295	0.286136	0.236494	0.189093	0.313100	0.313100	2.311026	2.001923	2.001923	2.001923	
28	6	0.556647	0.437411	0.264623	0.205283	0.186906	0.155449	0.311670	0.301717	2.076624	1.842489	1.706644	1.706644	
29	7	0.380957	0.317784	0.190253	0.151795	0.153805	0.131722	0.311569	0.301656	1.893297	1.706644	1.594202	1.594202	
30	8	0.285435	0.240141	0.140739	0.114439	0.130123	0.113742	0.310966	0.301087	1.744167	1.694769	1.494769	1.494769	
31	9	0.217616	0.187499	0.105996	0.087279	0.112324	0.099723	0.309182	0.299693	1.619350	1.619350	1.494769	1.494769	
32	10	0.171314	0.150602	0.080646	0.0646911	0.098445	0.088175	0.308888	0.297506	1.512574	1.477258	1.329273	1.329273	
33	11	0.138657	0.124067	0.061584	0.051258	0.097306	0.079218	0.303652	0.294644	1.419621	1.329273	1.259070	1.259070	
34	12	0.115142	0.104593	0.046906	0.038990	0.078158	0.071508	0.298335	0.291234	1.337520	1.266410	1.195277	1.195277	
35	13	0.097611	0.090773	0.035384	0.029220	0.070498	0.064131	0.295577	0.287383	1.264402	1.264402	1.136808	1.136808	
36	14	0.084866	0.075716	0.026198	0.021336	0.063980	0.051259	0.290959	0.283178	1.197735	1.197735	1.0897843	1.0897843	
37	15	0.075086	0.070757	0.018780	0.014904	0.058354	0.054104	0.286074	0.278683	1.137151	1.08783	0.856392	0.856392	
38	16	0.067633	0.064369	0.012727	C.009609	0.053437	0.049727	0.280965	0.273940	1.081340	1.081340	0.848099	0.848099	
39	17	0.061924	0.059416	0.007745	0.005220	0.047990	0.046020	0.275664	0.268977	1.029473	1.029473	0.816156	0.816156	
40	18	0.057538	0.055613	0.001617	0.001560	0.045204	0.042497	0.270180	0.263890	0.980842	0.980842	0.940547	0.940547	
41	19	0.054171	0.052689	0.000178	-0.001503	0.041693	0.039285	0.264508	0.258399	0.934812	0.934812	0.897843	0.897843	
42	20	0.051598	0.050457	-0.002695	-0.004073	0.038485	0.036324	0.258619	0.252738	0.90783	0.90783	0.856392	0.856392	
43	21	0.049653	0.048776	-0.005098	-0.006229	0.035515	0.033555	0.25450	0.245740	0.848099	0.848099	0.816156	0.816156	
44	22	0.048212	0.047542	-0.007105	-0.008033	0.032719	0.03114	0.245483	0.240250	0.805956	0.805956	0.775618	0.775618	
45	23	0.047188	0.046684	-0.003768	-0.009526	0.030916	0.026105	0.239660	0.232897	0.767048	0.767048	0.733291	0.733291	
46	24	0.046535	0.046194	-0.010114	-0.010109	0.027247	0.027330	0.230037	0.222670	0.716169	0.716169	0.680747	0.680747	
47	25	2	8.249172	3.574557	2.729640	1.227157	0.979819	0.489831	0.925937	0.531826	3.870176	2.649639	2.3014748	2.3014748
48	3	2.904672	1.743482	1.102970	0.674959	0.484738	0.3221074	0.395285	0.341725	0.341725	2.370267	2.370267		

Table D.II (continued)

x	A	A^0	B	B^0	C	C^0	Q^0	Q^0	Q^0	Q^0	Q^0	Q^0	Q^0	Q^0	Q^0	Q^0	Q^0	Q^0	Q^0
4	1.476105	1.0118425	0.429129	0.3196469	0.295012	0.237055	0.199551	0.101136	0.291292	0.2560606	0.309644	0.161991	0.141991	0.141991	0.141991	0.141991	0.141991	0.141991	
5	0.682770	0.459151	0.395961	0.273506	0.212726	0.187455	0.156116	0.293768	0.280702	0.256217	0.256217	0.156100	0.156100	0.156100	0.156100	0.156100	0.156100	0.156100	
6	0.582445	0.456530	0.332180	0.197690	0.158204	0.154351	0.132200	0.298715	0.289626	0.289626	0.289626	0.1561848	0.1561848	0.1561848	0.1561848	0.1561848	0.1561848	0.1561848	
7	0.406810	0.251196	0.147134	0.120364	0.130670	0.114231	0.298399	0.289399	0.289399	0.289399	0.289399	0.103531	0.103531	0.103531	0.103531	0.103531	0.103531	0.103531	
8	0.258879	0.227927	0.196091	0.111602	0.092288	0.012876	0.100224	0.297256	0.286270	0.286270	0.286270	0.1467903	0.1467903	0.1467903	0.1467903	0.1467903	0.1467903	0.1467903	
9	0.227927	0.179306	0.157321	0.085632	0.071421	0.099004	0.068960	0.295271	0.286531	0.286531	0.286531	0.138366	0.138366	0.138366	0.138366	0.138366	0.138366	0.138366	
10	0.144919	0.129324	0.066069	0.055156	0.087875	0.079768	0.292572	0.284139	0.284139	0.284139	0.284139	0.080111	0.080111	0.080111	0.080111	0.080111	0.080111	0.080111	
11	0.119986	0.108685	0.050976	0.042740	0.078738	0.072053	0.289300	0.281215	0.281215	0.281215	0.281215	0.240215	0.240215	0.240215	0.240215	0.240215	0.240215	0.240215	
12	0.101552	0.093220	0.039104	0.032670	0.071093	0.045495	0.285580	0.277657	0.277657	0.277657	0.277657	0.178613	0.178613	0.178613	0.178613	0.178613	0.178613	0.178613	
13	0.087711	0.081480	0.029618	0.024526	0.064592	0.059843	0.28510	0.274149	0.274149	0.274149	0.274149	0.121291	0.121291	0.121291	0.121291	0.121291	0.121291	0.121291	
14	0.077191	0.072478	0.021939	0.017964	0.058986	0.054911	0.277164	0.270156	0.270156	0.270156	0.270156	1.070121	1.070121	1.070121	1.070121	1.070121	1.070121	1.070121	
15	0.069122	0.065524	0.015455	0.012365	0.054093	0.050561	0.272595	0.265922	0.265922	0.265922	0.265922	1.021208	1.021208	1.021208	1.021208	1.021208	1.021208	1.021208	
16	0.062891	0.060124	0.010467	0.077791	0.049773	0.046985	0.267839	0.261480	0.261480	0.261480	0.261480	0.976170	0.976170	0.976170	0.976170	0.976170	0.976170	0.976170	
17	0.058859	0.055919	0.006153	0.003963	0.045921	0.03198	0.262916	0.256847	0.256847	0.256847	0.256847	0.913599	0.913599	0.913599	0.913599	0.913599	0.913599	0.913599	
18	0.054307	0.052645	0.002545	0.002545	0.042451	0.042451	0.257832	0.252247	0.252247	0.252247	0.252247	0.82630	0.82630	0.82630	0.82630	0.82630	0.82630	0.82630	
19	0.051398	0.050105	0.001972	0.001972	0.039293	0.037128	0.252572	0.246994	0.246994	0.246994	0.246994	0.847367	0.847367	0.847367	0.847367	0.847367	0.847367	0.847367	
20	0.049151	0.048148	0.001038	0.001038	0.036191	0.034355	0.247117	0.241711	0.241711	0.241711	0.241711	0.847188	0.847188	0.847188	0.847188	0.847188	0.847188	0.847188	
21	0.047443	0.046661	0.000519	0.000519	0.033687	0.031903	0.241393	0.236152	0.236152	0.236152	0.236152	0.776870	0.776870	0.776870	0.776870	0.776870	0.776870	0.776870	
22	0.046165	0.045542	0.00067	0.00067	0.0297837	0.0297837	0.235269	0.230144	0.230144	0.230144	0.230144	0.74272	0.74272	0.74272	0.74272	0.74272	0.74272	0.74272	
23	0.045249	0.044646	0.0010281	0.0010281	0.026087	0.026087	0.220562	0.213764	0.213764	0.213764	0.213764	0.729654	0.729654	0.729654	0.729654	0.729654	0.729654	0.729654	
24	0.044646	0.043347	0.0009733	0.0009733	0.024317	0.024317	0.213764	0.213764	0.213764	0.213764	0.213764	0.653317	0.653317	0.653317	0.653317	0.653317	0.653317	0.653317	

Table D.III - Cramér-Rao Efficiencies of BLI Estimates of 10 Percent Points of the Extreme-Value Distribution, Where $\frac{n-r}{n}$ of the Size n Ordered Sample is Censored From Above, $2 \leq n \leq 18$,
 $2 \leq r \leq n$

r/n	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18
2	.835																
3	.892	.862															
4	.912	.905	.883														
5	.925	.918	.918	.898													
6	.932	.928	.927	.928	.910												
7	.933	.936	.934	.936	.936	.919											
8	.929	.942	.940	.941	.943	.943	.927										
9	.920	.947	.945	.945	.947	.948	.948	.948									
10	.907	.950	.949	.949	.950	.952	.952	.953	.952								
11	.891	.952	.953	.952	.953	.953	.954	.954	.956	.957							
12	.872	.952	.955	.955	.956	.957	.958	.958	.959	.960	.961						
13		.951	.959	.958	.958	.959	.960	.960	.960	.961	.962	.963					
14	.852	.948	.961	.961	.960	.961	.962	.962	.963	.964	.965	.965					
15	.812	.944	.962	.963	.962	.963	.963	.963	.964	.965	.966	.966	.967				
16	.792	.939	.963	.965	.964	.964	.965	.965	.966	.967	.968	.968	.969				
17	.773	.932	.963	.967	.966	.966	.966	.967	.968	.969	.970	.970	.971	.971			
18	.755	.925	.963	.968	.968	.967	.968	.968	.969	.970	.971	.971	.972	.972	.972		

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13. ABSTRACT		
<p>This report gives results concerning estimation of location and scale parameters. Most of the work pertains to the first extreme-value distribution of smallest values, the distribution of the natural logarithms of failure times having the two-parameter Weibull distribution. Experimental designs are derived, under the assumption that log failure times are polynomial functions of the reciprocal of stress level and have the extreme-value distribution, for over-stress life tests. These designs yield least-squares curves with minimum variance at a specified (nominal) stress level below the levels at which the life test is conducted. An estimate of the extreme-value location parameter μ associated with the nominal stress level and the relationship between μ and stress level can be obtained from the least-squares curve. Other extreme-value results apply to a life test conducted at a single fixed stress level.</p>		

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